

# Vinyl chloride synthesis via selective oxidative coupling of methyl chloride

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**Abstract:** Selective coupling of C<sub>1</sub> platform molecules to C<sub>2</sub> olefins is a cornerstone for establishing a sustainable chemical industry based on non-petroleum sources<sup>1-3</sup>. Vinyl chloride (C<sub>2</sub>H<sub>3</sub>Cl), one of top commodity petrochemicals, is commercially produced from coal- or oil-derived C<sub>2</sub> hydrocarbon (acetylene and ethylene) feedstocks with a high carbon footprint<sup>4-6</sup>. Here, we report a vinyl chloride synthesis via selective oxidative coupling of methyl chloride. This is enabled by a solid catalyst, featuring tungstate sub-nanoclusters embedded in a zirconia matrix, which effectively captures

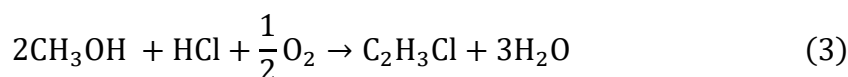
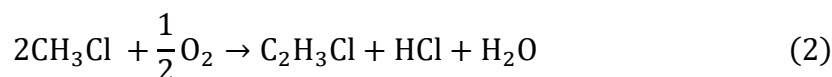
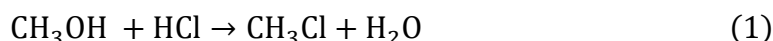
$\cdot\text{CH}_2\text{Cl}$  radicals homogeneously generated in  $\text{CH}_3\text{Cl}$  oxy-pyrolysis and selectively couples them into  $\text{C}_2\text{H}_3\text{Cl}$ . In-situ synchrotron-based vacuum ultraviolet photoionization mass spectrometry provides direct experimental evidence of the homogeneous-heterogeneous reaction mechanism. The process achieves methyl chloride conversion of 10 – 65% with a high vinyl chloride selectivity (60 – 75%) at a reaction temperature (600 – 750 °C), which is much lower than the traditional pyrolysis (> 850 °C). It also delivers a stable performance (at a vinyl chloride yield of *ca.* 30%) with no deactivation observed during a 50-hour test. Furthermore, combining with reaction of methanol and HCl to produce methyl chloride, we establish a methanol-to-vinyl chloride (MTV) route with the potential for significant reductions in climate change impact (24%) and cost (38%) compared to the state-of-the-art ethylene-based balanced process, allowing for the efficient utilization of cheaper and renewable  $\text{C}_1$  feedstocks.

## Main

Vinyl chloride ( $\text{C}_2\text{H}_3\text{Cl}$ ), the monomer of the third-most widely manufactured plastic, polyvinyl chloride, is produced commercially from fossil coal- or oil-derived  $\text{C}_2$  hydrocarbon feedstocks<sup>4-6</sup>. The direct hydrochlorination of coal-derived acetylene leads to vinyl chloride monomer (VCM) using toxic  $\text{HgCl}_2$  catalysts<sup>7-9</sup>. The ethylene-based balanced process (EBP) integrates the direct chlorination/oxychlorination of oil-derived ethylene and pyrolysis of ethylene dichloride (EDC) to produce VCM and has been widely adopted by VCM producers since the mid-1950s, accounting for nearly all capacities worldwide<sup>10-12</sup>. Although these industrial processes are suboptimal due to the use of relatively expensive and high carbon footprint feedstocks<sup>12,13</sup>, a new reaction route that can rival the existing ones in terms of cost and energy efficiencies is still underdeveloped. Very recently, it has been demonstrated that using natural gas-derived ethane as the feedstock, VCM could be made at a cheaper cost and with less  $\text{CO}_2$  emissions<sup>12,14</sup>. Yet, an economically competitive VCM production process based on the efficient utilization of cheaper and renewable  $\text{C}_1$  feedstocks that minimize environmental impact still represents a grand challenge.

C<sub>1</sub> platforms, such as methane, methanol, carbon monoxide, and carbon dioxide, play a crucial role in the current and future energy and chemical supply. Their significance is expected to grow further due to the increasing need to decarbonize chemicals and fuels in line with CO<sub>2</sub> capture and utilization to mitigate global warming<sup>2,15</sup>. The coupling of C<sub>1</sub> molecules to C<sub>2</sub> olefins presents a sustainable alternative to the petroleum-based chemical industry. One such example is the conversion of methanol to hydrocarbons<sup>16-20</sup>, which, when integrated with the renewable production of methanol from CO<sub>2</sub><sup>21</sup>, sets the foundation for a methanol economy<sup>22</sup>.

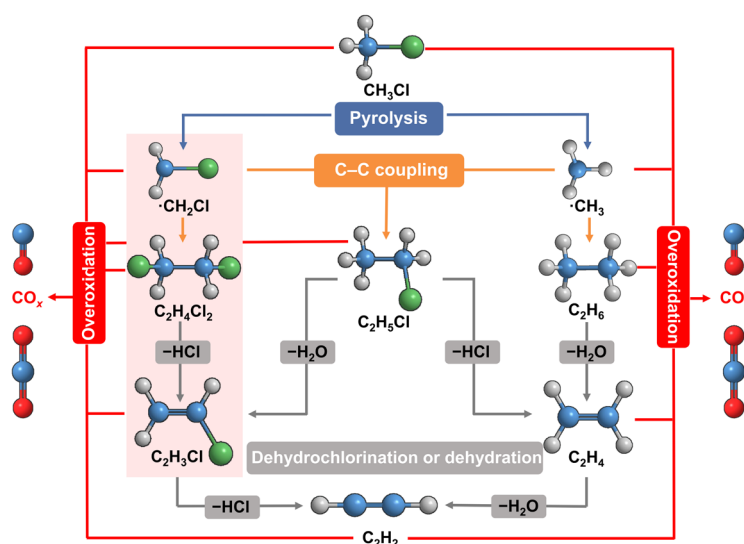
Herein, we report a methanol-based route for VCM production (MTV). The MTV process includes direct reaction of methanol and HCl to form methyl chloride (another important C<sub>1</sub> molecule<sup>23-26</sup>), followed by oxidative coupling of methyl chloride to make VCM (MCTV). The reactions for each component process are shown in **equation 1** and **2**, and the overall reaction is given by **equation 3**.



The hydrochlorination of methanol yields methyl chloride as the main product with small amounts of dimethyl ether as the only by-product. It is commercially carried out in both liquid-phase and gas-phase processes<sup>27</sup>. The second step (MCTV) is the key for MTV process and has not been established yet.

Direct coupling of CH<sub>3</sub>Cl into VCM is theoretically feasible via radical chain reactions (CH<sub>3</sub>Cl → ·CH<sub>2</sub>Cl → C<sub>2</sub>H<sub>4</sub>Cl<sub>2</sub> → C<sub>2</sub>H<sub>3</sub>Cl)<sup>28</sup>. However, there is no catalytic way to steer CH<sub>3</sub>Cl transformation at elevated temperature due to the highly reactive and short-lived nature of the radicals, the complex reaction networks, and uncontrollable gas-phase kinetics, especially in the presence of oxygen molecules (**Fig. 1**)<sup>28</sup>. Methyl chloride (oxy)pyrolysis is a high-temperature (> 850 °C) free radical chain process<sup>29,30</sup>, in which ·CH<sub>2</sub>Cl and ·CH<sub>3</sub> are two key C<sub>1</sub> intermediates. Methyl chloride readily couples to form acetylene, ethylene and some VCM in the gas

phase. However, the VCM yield in methyl chloride (oxy)pyrolysis is only 1 – 3% without replenishing chlorine in the pyrolysis system<sup>31,32</sup>. The loss of its chlorine component is due to facile VCM decomposition under the high-temperature condition<sup>30,33</sup>. Especially in the presence of oxygen, VCM is completely decomposed at temperature above 750 °C. In this work, we have discovered that high-concentration tungstate clusters embedded in a ZrO<sub>2</sub> matrix (NaWZr) can effectively capture  $\cdot\text{CH}_2\text{Cl}$  homogeneously generated in CH<sub>3</sub>Cl oxy-pyrolysis and selectively convert them into VCM. The proposed homogeneous-heterogeneous reaction mechanism is confirmed by in-situ synchrotron-based vacuum ultraviolet photoionization mass spectrometry (SVUV-PIMS). The oxidative coupling of methyl chloride into VCM achieves methyl chloride conversion of 10 – 60% with a high VCM selectivity (60 – 75%) at a reaction temperature (650 – 750 °C) much lower than traditional pyrolysis. The resulting VCM yield (8.9 – 39.7%) is massively propelled compared to that of the conventional pyrolysis (< 3%). Moreover, the utilization of renewable C<sub>1</sub> feedstocks (e.g., green methanol and biomethane) leads to superior environmental and economic performance, demonstrating the potential for a *ca.* 25% reduction in climate change impacts and *ca.* 40% reduction in costs.

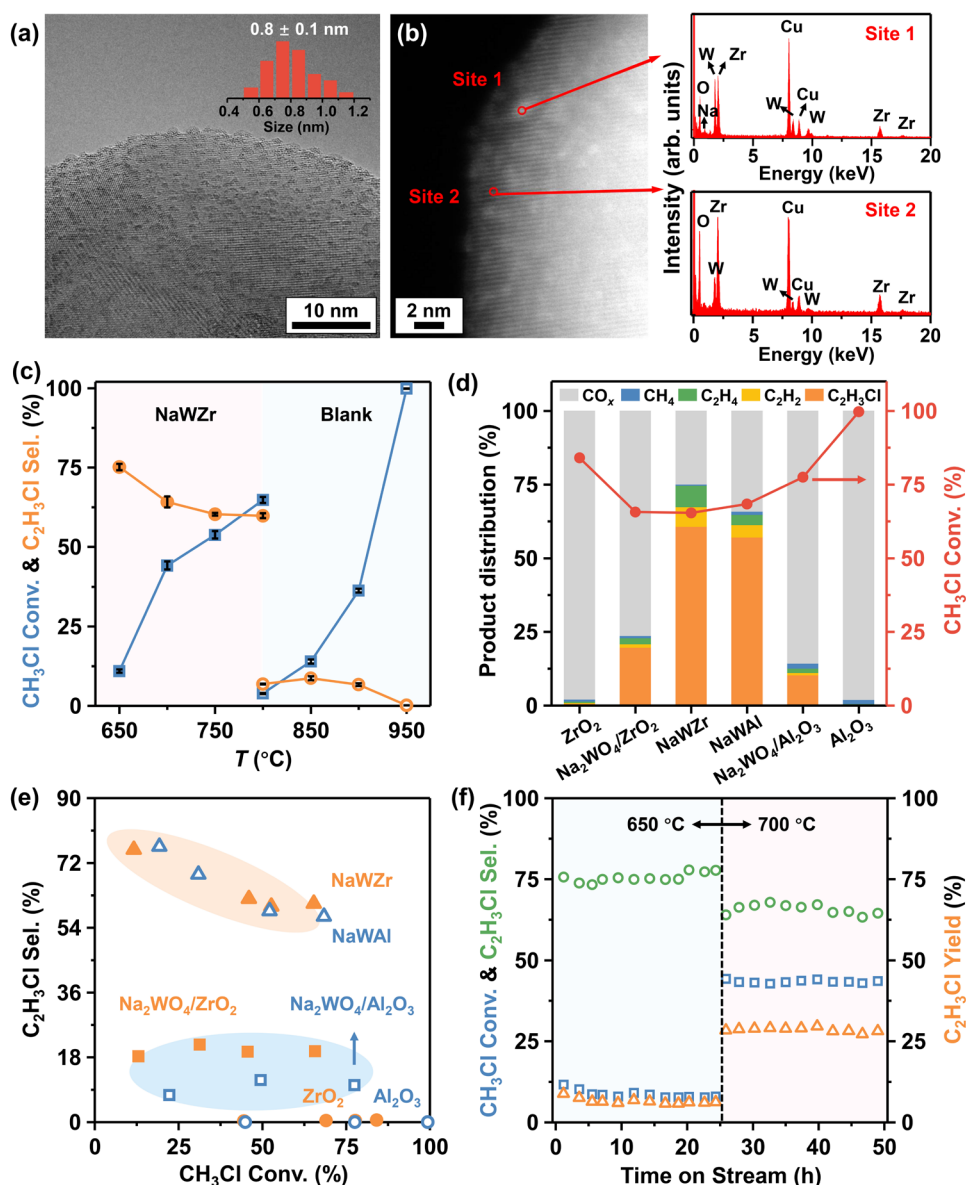


**Fig. 1 | A brief overview of the reaction networks of CH<sub>3</sub>Cl-to-C<sub>2</sub>H<sub>3</sub>Cl (MCTV) transformation.**

The NaWZr catalyst was prepared by our recently developed co-precipitation method using  $WCl_6$  and  $Zr(OC_4H_9)_4$  as precursors and NaOH as precipitating agent<sup>34</sup>. A W-to-Zr molar ratio of 1:3 was adopted to achieve a high concentration of sodium tungstate clusters within the  $ZrO_2$  matrix (see detailed methods in Supplementary Material). The final catalyst was calcined at 750 °C for 5 h before any characterization and catalytic tests. Aberration-corrected transmission electron microscopy confirms that W species are uniformly dispersed on the  $ZrO_2$  matrix as sodium tungstate clusters and the average particle size of tungstate clusters is ~0.8 nm (**Fig. 2a** and **Supplementary Fig. 1**). For comparison,  $Na_2WO_4/ZrO_2$  prepared by incipient-wetness impregnation shows a non-uniform distribution of W and Zr (**Supplementary Fig. 2**). Due to the high mass loading of impregnated  $Na_2WO_4$  (~35%), only part of them can disperse as nanoclusters on the surface of  $ZrO_2$  (**Supplementary Fig. 2**). The tungsten-rich/zirconium-poor regions in elemental mappings of  $Na_2WO_4/ZrO_2$  evidence that the excess  $Na_2WO_4$  aggregates into bulk crystals (**Supplementary Fig. 2**). Similar trends are also seen for NaWAl (**Supplementary Fig. 3**) and  $Na_2WO_4/Al_2O_3$ , demonstrating the co-precipitation method as a superior method to impregnation for obtaining a higher concentration of sodium tungstate clusters.

The oxidative coupling of  $CH_3Cl$  was conducted at atmospheric pressure under an optimized condition (**Fig. 2c**, **Supplementary Fig. 4** and **5**) of  $CH_3Cl:O_2:N_2 = 1:2:57$  and 650 – 750 °C that is much lower than traditional oxy-pyrolysis. There is no noticeable  $CH_3Cl$  conversion for the blank experiment at 750 °C, and the homogeneous reaction only attains limited  $CH_3Cl$  conversion (< 3.7%) and  $C_2H_3Cl$  selectivity (< 10%) even at 800 °C (**Fig. 2c** and **Supplementary Table 1**). Using  $ZrO_2$  and  $Al_2O_3$  as the catalysts significantly reduces the light-off temperature and improves  $CH_3Cl$  conversion but without  $C_2H_3Cl$  selectivity (< 1%) (**Fig. 2d** and **Supplementary Table 1**). Interestingly, once 35 wt.% of  $Na_2WO_4$  is deposited onto  $ZrO_2$  ( $Na_2WO_4/ZrO_2$ ), a boosted ~18%  $C_2H_3Cl$  selectivity is obtained over a wide range of  $CH_3Cl$  conversion (blue shaded area in **Fig. 2e**). This result suggests  $Na_2WO_4$  as the active component driving the pyrolysis of  $CH_3Cl$  to produce  $C_2H_3Cl$ . Moreover, when NaWZr and NaWAl with high concentrations of  $Na_2WO_4$  clusters are used as the

catalysts, the oxidative pyrolysis of CH<sub>3</sub>Cl eventually involves into a selective coupling of CH<sub>3</sub>Cl to C<sub>2</sub>H<sub>3</sub>Cl. As shown in the red shaded area in **Fig. 2e**, the C<sub>2</sub>H<sub>3</sub>Cl selectivity reaches 75.7% at CH<sub>3</sub>Cl conversion of 10 – 20% ( $T = 650\text{ }^{\circ}\text{C}$ ) and maintains ~60% at CH<sub>3</sub>Cl conversion of ~65% ( $T = 750\text{ }^{\circ}\text{C}$ ). Other minor products are CH<sub>4</sub> (0 – 3%), C<sub>2</sub>H<sub>4</sub> (6 – 9%), C<sub>2</sub>H<sub>2</sub> (0 – 7%), CO<sub>2</sub> (2 – 9%) and CO (8 – 25%). A single-pass C<sub>2</sub>H<sub>3</sub>Cl yield as high as ~39.7% is achieved over NaWZr at 750 °C. Further increasing the reaction temperature results in a decrease of C<sub>2</sub>H<sub>3</sub>Cl yield to 23.3% due to facile VCM decomposition at higher reaction temperature. The NaWZr catalyst delivers stable CH<sub>3</sub>Cl conversion and C<sub>2</sub>H<sub>3</sub>Cl selectivity during a 50-hour test (**Fig. 2f**). A stable 28% C<sub>2</sub>H<sub>3</sub>Cl yield is achieved at 700 °C. Aberration-corrected transmission electron microscopy analysis of the NaWZr catalyst after reaction confirms the structural stability of the sub-nanoclusters (**Supplementary Fig. 6**). Moreover, a C<sub>2</sub>H<sub>3</sub>Cl yield as high as 33% with a C<sub>2</sub>H<sub>3</sub>Cl selectivity of 53.9% can be achieved at 725 °C even without using N<sub>2</sub> as a dilution gas (**Supplementary Table 2**). The excellent C<sub>2</sub>H<sub>3</sub>Cl yield, low reaction temperature, and stable catalytic performance distinguishes MCTV with traditional pyrolysis process and showcase the great potential of MCTV for industrial-scale C<sub>2</sub>H<sub>3</sub>Cl production.



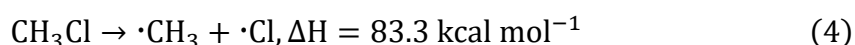
**Fig. 2 | Structural characterization and reaction performance.** (a) The aberration-corrected transmission electron microscopy images of NaWZr catalyst. (b) Representative energy dispersive spectroscopy (EDS) analysis of NaWZr catalyst. (c)  $\text{CH}_3\text{Cl}$  conversion and VCM selectivity as functions of reaction temperature in MCTV (NaWZr catalyst) and oxy-pyrolysis. The error bar was calculated based on three independent experiments. (d) The  $\text{CH}_3\text{Cl}$  conversion and product selectivity over various catalysts at  $750^\circ\text{C}$ . (e) The catalytic performances of various catalysts in MCTV. Detailed data are summarized in **Supplementary Table 1**. (f) Long-term stability tests over NaWZr catalyst at  $650^\circ\text{C}$  and  $700^\circ\text{C}$ . Reaction conditions: 150 mg catalyst,  $\text{CH}_3\text{Cl}:\text{O}_2:\text{N}_2 = 1:2:57$ , total gas flow rate =  $60 \text{ mL min}^{-1}$ .

We further investigate the compositional and structural influence of the tungstate catalyst in the CH<sub>3</sub>Cl-to-C<sub>2</sub>H<sub>3</sub>Cl conversion. Replacing the W element in NaWZr by Mo decreases the C<sub>2</sub>H<sub>3</sub>Cl selectivity from ~60% to ~1%, demonstrating that tungsten is the core component of the active sites (**Supplementary Fig. 7**). Using ammonium metatungstate as the tungsten precursor in co-precipitation produces WO<sub>3</sub> instead of Na<sub>2</sub>WO<sub>4</sub> (see X-ray diffraction patterns in **Supplementary Fig. 8**). The catalyst is denoted as WO<sub>3</sub>-ZrO<sub>2</sub> and shows much lower C<sub>2</sub>H<sub>3</sub>Cl selectivity than NaWZr at all the temperatures evaluated (**Supplementary Fig. 9**), suggesting that the active sites for MCTV are Na<sub>2</sub>WO<sub>4</sub> rather than WO<sub>3</sub>. Notably, when the Na element in NaWZr is replaced by K, C<sub>2</sub>H<sub>3</sub>Cl selectivity decreases from ~60% to 22% (**Supplementary Fig. 7**), demonstrating the critical role of Na. It is interesting to note that bulk Na<sub>2</sub>WO<sub>4</sub>, whether physically mixed with ZrO<sub>2</sub> or not, exhibits a limited C<sub>2</sub>H<sub>3</sub>Cl yield (< 4%) over the investigated temperature range (**Supplementary Fig. 10**). Correlating this result with the high-angle annular dark field scanning transmission electron microscopy (HAADF-STEM) micrographs (**Supplementary Fig. 2**) and catalytic performance (**Fig. 2d**) of Na<sub>2</sub>WO<sub>4</sub>/ZrO<sub>2</sub> leads to the conclusion that Na<sub>2</sub>WO<sub>4</sub> nanoclusters account for the C<sub>2</sub>H<sub>3</sub>Cl production. The higher concentration of Na<sub>2</sub>WO<sub>4</sub> clusters in NaWZr than Na<sub>2</sub>WO<sub>4</sub>/ZrO<sub>2</sub> may therefore be responsible for the 3 – 4 times higher C<sub>2</sub>H<sub>3</sub>Cl selectivity at the same degree of CH<sub>3</sub>Cl conversion (**Fig. 2e**). To further verify this hypothesis, we synthesized a series NaWZr catalysts with different concentrations of Na<sub>2</sub>WO<sub>4</sub> clusters and evaluated their catalytic performance in MCTV. According to our recent patent application<sup>34</sup>, the Na<sub>2</sub>WO<sub>4</sub> clusters concentration in NaWZr catalysts can be readily regulated by adjusting the W-to-Zr ratios and quantified by the number of tungstate clusters in 100 nm<sup>2</sup> of the ZrO<sub>2</sub> matrix in the high-resolution transmission electron microscopy (HRTEM) images. As shown in **Supplementary Fig. 11**, the volcano plots for the C<sub>2</sub>H<sub>3</sub>Cl selectivity and yield against the W-to-Zr ratio are similar to those for the concentration of tungstate nanoclusters. The maximum C<sub>2</sub>H<sub>3</sub>Cl selectivity and yield are achieved by NaWZr with W:Zr ratio of 3:9~4:9, which also shows the highest concentration of tungstate clusters. Notably, NaWAl using Al<sub>2</sub>O<sub>3</sub> as support to anchor tungstate clusters also achieves

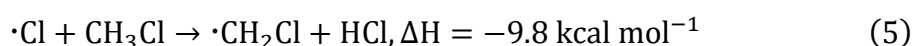


high-concentration Na<sub>2</sub>WO<sub>4</sub> clusters (**Supplementary Fig. 3**), and the catalytic performance of NaWAl is close to that of NaWZr (**Fig. 2** and **Supplementary Table 1**). These results exclude the support effect and hint at Na<sub>2</sub>WO<sub>4</sub> nanoclusters as the active sites for MCTV.

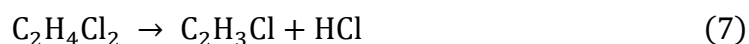
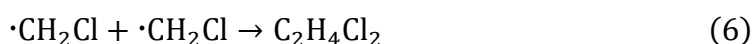
The oxidative pyrolysis of CH<sub>3</sub>Cl to VCM proceeds via radical chain reactions at high temperatures (**Fig. 1**)<sup>28</sup>. Due to the lower bond strength of CH<sub>3</sub>-Cl compared to CH<sub>2</sub>Cl-H, chain radical initiation usually occurs via the endothermic decomposition of CH<sub>3</sub>Cl into ·CH<sub>3</sub> and ·Cl (**equation 4**).



The subsequent exothermic H-abstraction reaction between ·Cl and CH<sub>3</sub>Cl (**equation 5**) dominates the conversion of CH<sub>3</sub>Cl, yielding ·CH<sub>2</sub>Cl as the primary C<sub>1</sub> radical intermediate<sup>29</sup>.



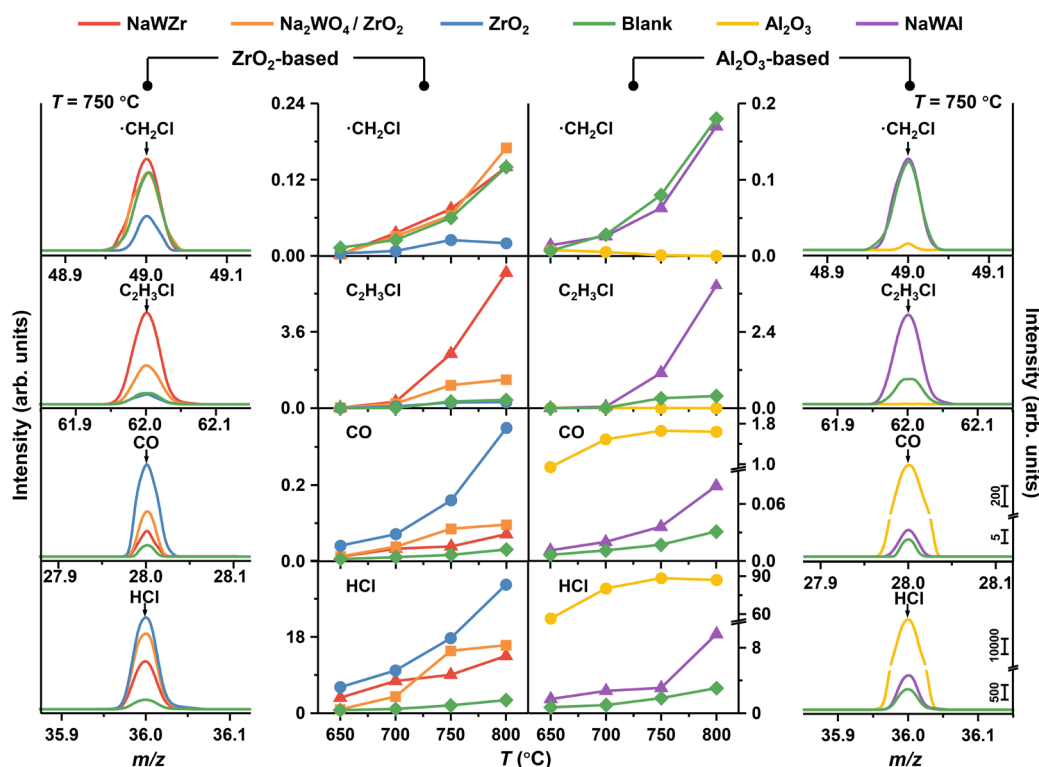
·CH<sub>2</sub>Cl can undergo coupling to form C<sub>2</sub>H<sub>4</sub>Cl<sub>2</sub> (**equation 6**), which readily decomposes into C<sub>2</sub>H<sub>3</sub>Cl and HCl (**equation 7**).



However, at elevated temperatures in the presence of oxygen, the irreversible overoxidation of reactive intermediates and products leads to a large amount of thermodynamically stable CO<sub>x</sub><sup>29</sup>, which restricts the C<sub>2</sub>H<sub>3</sub>Cl selectivity and yield in oxidative pyrolysis (**Fig. 1**). Introducing NaWZr into the reaction system significantly changes the kinetics of oxidative pyrolysis, evidenced by the different apparent reaction orders of CH<sub>3</sub>Cl (0.85 vs. 2.18, **Supplementary Fig. 12**) and reaction temperature. NaWZr achieves a CH<sub>3</sub>Cl conversion of 46% at a significantly lower temperature than the blank experiment (700 °C versus 920 °C). More importantly, in the presence of NaWZr, the reaction shifts from overoxidation to selective coupling into C<sub>2</sub>H<sub>3</sub>Cl at equivalent levels of CH<sub>3</sub>Cl conversion (**Supplementary Fig. 13**).

To illustrate how NaWZr changes the kinetics of the oxidative pyrolysis of CH<sub>3</sub>Cl, we investigated the impact of NaWZr on each elementary reaction of the CH<sub>3</sub>Cl-to-C<sub>2</sub>H<sub>3</sub>Cl conversion. As shown in **Supplementary Fig. 14**, the

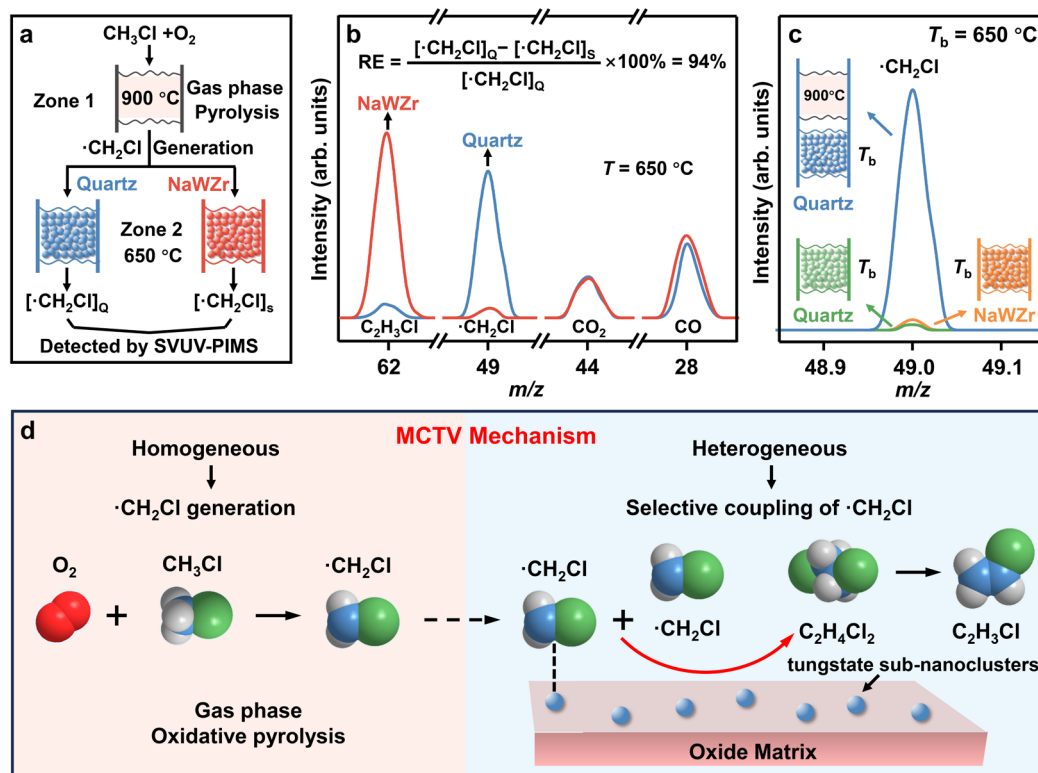
decomposition of  $C_2H_4Cl_2$  into  $C_2H_3Cl$  and  $HCl$  (**equation 7**) is a rapid reaction unaffected by the presence of NaWZr. Besides, the presence of  $CH_3Cl$  in gas phase significantly reduces the overoxidation of  $C_2H_3Cl$ , irrespective of the utilization of NaWZr as a catalyst (**Supplementary Fig. 15**). These findings exclude **equation 7** and the following conversion of  $C_2H_3Cl$  as the key steps influenced by NaWZr.



**Fig. 3 | Evolution of representative species during reaction.** The mass spectra of the representative species in the MCTV process were determined by in-situ SVUV-PIMS. Peak areas of the representative species were plotted as a function of temperature in the MCTV reaction over various catalysts. Reaction conditions: 150 mg catalyst, total pressure 0.1 bar,  $CH_3Cl:O_2 = 1:2$ , total gas flow rate =  $60 \text{ mL min}^{-1}$ .

The influence of NaWZr in radicals-involved elementary reactions was investigated by a validated in-situ synchrotron-based vacuum ultraviolet photoionization mass spectrometry (SVUV-PIMS)<sup>35</sup>. **Supplementary Fig. 16** displays all species detected at 750 °C and near ambient pressure (0.1 bar). Interestingly, the species identified during the blank experiment were also present over NaWZr,

indicating their similar reaction pathways. Specifically, methyl ( $\cdot\text{CH}_3$ ) and chloromethyl radicals ( $\cdot\text{CH}_2\text{Cl}$ ), represented by the signals at  $m/z = 15$  and  $49$ , are observed, suggesting that in both cases the reaction proceeds via radical reactions. No  $\text{C}_2\text{H}_4\text{Cl}_2$  and  $\text{C}_2\text{H}_5\text{Cl}$  signals were observed, likely due to their rapid decomposition into  $\text{C}_2\text{H}_3\text{Cl}$  and  $\text{C}_2\text{H}_4$  (**Supplementary Fig. 14** and **17**). To elucidate the reaction mechanism, we quantitatively analyzed the evolution of key radical intermediates and representative products ( $\cdot\text{CH}_2\text{Cl}$ ,  $\text{C}_2\text{H}_3\text{Cl}$ ,  $\text{CO}$ , and  $\text{HCl}$ ) during the  $\text{CH}_3\text{Cl}$ -to- $\text{C}_2\text{H}_3\text{Cl}$  conversion (**Fig. 3**). The most important finding is that  $\text{Na}_2\text{WO}_4/\text{ZrO}_2$ ,  $\text{NaWZr}$ , and  $\text{NaWAl}$  exhibit similar gas phase  $\cdot\text{CH}_2\text{Cl}$  signals but significantly higher  $\text{C}_2\text{H}_3\text{Cl}$  signals than the blank experiment over the investigated temperature range. According to the homogeneous reaction kinetics<sup>35</sup>, the similar  $\cdot\text{CH}_2\text{Cl}$  concentration at the same reaction conditions would result in a similar reaction outcome in the gas phase. The distinct  $\text{C}_2\text{H}_3\text{Cl}$  signal would therefore result from the heterogeneous  $\text{C}_2\text{H}_3\text{Cl}$  production over tungstate catalysts. Moreover, the  $\text{C}_2\text{H}_3\text{Cl}$  signals follow the same trend of  $\text{Na}_2\text{WO}_4$  clusters concentration, i.e.,  $\text{NaWZr} > \text{Na}_2\text{WO}_4/\text{ZrO}_2 \gg \text{ZrO}_2 \approx \text{blank}$ . This result corresponds well with the catalytic data shown in **Fig. 2e** and **Supplementary Table 1** and further suggests that the heterogeneous  $\text{C}_2\text{H}_3\text{Cl}$  production occurs over  $\text{Na}_2\text{WO}_4$  nanoclusters. The  $\text{HCl}$  signals at the same temperature follow an order of  $\text{ZrO}_2 > \text{Na}_2\text{WO}_4/\text{ZrO}_2 > \text{NaWZr} > \text{blank}$ , which is consistent with the trend of  $\text{CH}_3\text{Cl}$  conversion depicted in **Supplementary Table 1**. Given that  $\text{Na}_2\text{WO}_4$  itself is inert for  $\text{CH}_3\text{Cl}$  activation over the investigated temperature range, the primary function of the catalyst in  $\text{C}_2\text{H}_3\text{Cl}$  production is the coupling  $\cdot\text{CH}_2\text{Cl}$  to form  $\text{C}_2\text{H}_4\text{Cl}_2$  (**equation 6**), which readily decomposes into  $\text{C}_2\text{H}_3\text{Cl}$  and  $\text{HCl}$ .



**Fig. 4 | Mechanistic analysis.** (a, b) The reaction efficiencies (RE) of NaWZr towards  $\cdot\text{CH}_2\text{Cl}$  radicals generated by the oxidative pyrolysis of  $\text{CH}_3\text{Cl}$  in the gas phase at  $900\text{ }^\circ\text{C}$ .  $I_{\text{NaWZr}}/I_{\text{Q}}$  shows the intensity ratio of species detected over NaWZr and quartz. (c)  $\cdot\text{CH}_2\text{Cl}$  detected by in-situ SVUV-PIMS over NaWZr and quartz at  $650\text{ }^\circ\text{C}$ . Reaction conditions:  $150\text{ mg}$  catalyst,  $P = 2.67\text{ mbar}$ ,  $\text{CH}_3\text{Cl}:\text{O}_2 = 1:8$ , total gas flow rate =  $60\text{ mL min}^{-1}$ . (d) Schematic illustration of the homogeneous-heterogeneous reaction mechanism of MCTV process.

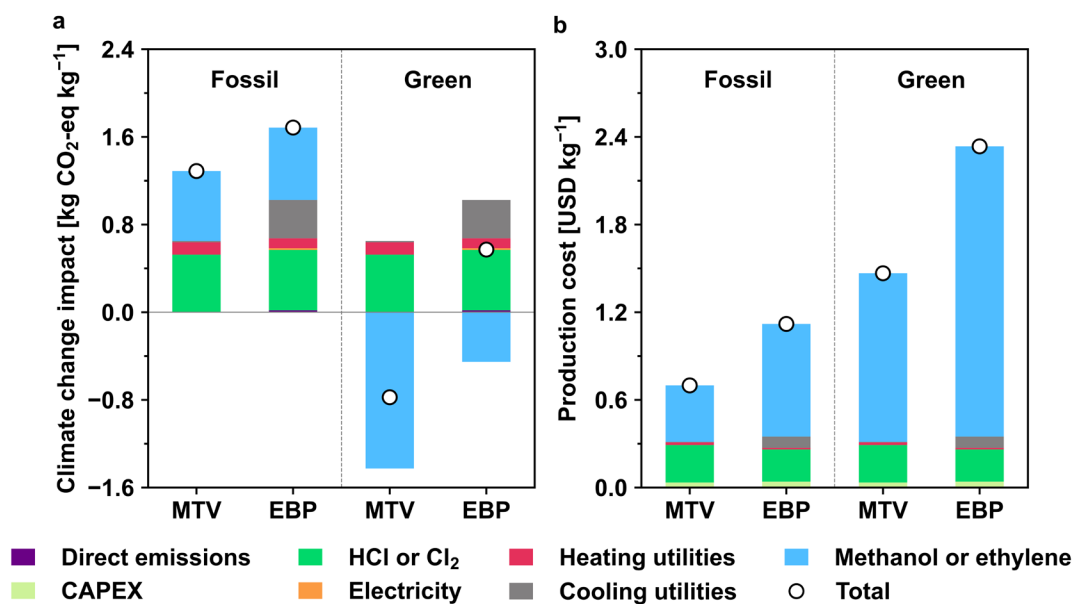
To directly elucidate the homogeneous-heterogeneous mechanism of MCTV reaction and investigate the critical role of NaWZr in controlling the transformation of  $\cdot\text{CH}_2\text{Cl}$ , we designed a two-temperature-zone reactor for the in-situ SVUV-PIMS study. In this reactor (**Fig. 4a**),  $\cdot\text{CH}_2\text{Cl}$  was homogeneously generated by oxy-pyrolysis of  $\text{CH}_3\text{Cl}$  at  $900\text{ }^\circ\text{C}$  (Zone 1) and then reacted with the downstream catalysts at  $650\text{ }^\circ\text{C}$  (Zone 2). Quartz, an inert material for  $\cdot\text{CH}_2\text{Cl}$  generation and transformation (**Supplementary Fig. 18**), was used as a control sample for NaWZr to offset the homogeneous transformation of  $\cdot\text{CH}_2\text{Cl}$  in Zone 2. Gas-phase  $\cdot\text{CH}_2\text{Cl}$  and its products

after reacting with NaWZr and quartz were monitored by SVUV-PIMS in the low-pressure mode (2.67 mbar) to improve the signal-to-noise ratio. The minimal production of  $\cdot\text{CH}_2\text{Cl}$  (**Fig. 4c**) and HCl (**Supplementary Fig. 18**) from quartz and NaWZr at 650 °C (Zone 2) as compared to the oxidative pyrolysis of  $\text{CH}_3\text{Cl}$  at 900 °C (Zone 1) excluded their role in  $\text{CH}_3\text{Cl}$  activation to generate  $\cdot\text{CH}_2\text{Cl}$  and confirmed that the two-zone reactor configuration successfully separated  $\cdot\text{CH}_2\text{Cl}$  transformation from  $\cdot\text{CH}_2\text{Cl}$  generation. Interestingly, once  $\cdot\text{CH}_2\text{Cl}$  homogeneously generated by  $\text{CH}_3\text{Cl}$  (oxy)pyrolysis passed through NaWZr, its gas-phase concentration significantly declined (**Fig. 4b**). Following the definition of reaction efficiency (RE) proposed by Lunsford *et al.*<sup>36</sup>, the RE of NaWZr towards  $\cdot\text{CH}_2\text{Cl}$  radicals was calculated to be 94%. These results unambiguously show that NaWZr can effectively capture  $\cdot\text{CH}_2\text{Cl}$  homogeneously generated by  $\text{CH}_3\text{Cl}$  oxy-pyrolysis and drive the following  $\cdot\text{CH}_2\text{Cl}$  transformation from the gas phase onto the catalyst surface. It is important to note that NaWZr produced 15 times higher  $\text{C}_2\text{H}_3\text{Cl}$  signal than quartz with only a slight increase of CO signal (6.7 %) (**Fig. 4b**). These results suggested that NaWZr is highly selective in capturing  $\cdot\text{CH}_2\text{Cl}$  and subsequently coupling them into  $\text{C}_2\text{H}_4\text{Cl}_2$  (**equation 6**), which readily decompose into  $\text{C}_2\text{H}_3\text{Cl}$  and HCl. These critical surface elementary steps eventually change the reaction kinetics and prompt  $\text{CH}_3\text{Cl}$  conversion at low reaction temperature.

The surface-confined  $\cdot\text{CH}_2\text{Cl}$  transformation over  $\text{Na}_2\text{WO}_4$  was also verified by the catalytic test over  $\text{Na}_2\text{WO}_4/\text{SiO}_2$ , which was prepared by incipient-wetness impregnation using quartz ( $\text{SiO}_2$ ) as the support. As mentioned above, both quartz and  $\text{Na}_2\text{WO}_4$  are inert for  $\text{CH}_3\text{Cl}$  activation. When  $\text{Na}_2\text{WO}_4/\text{SiO}_2$  was used as the catalyst,  $\cdot\text{CH}_2\text{Cl}$  was generated solely from the homogeneous oxy-pyrolysis of  $\text{CH}_3\text{Cl}$ . Interestingly,  $\text{Na}_2\text{WO}_4/\text{SiO}_2$  exhibited a remarkable  $\text{CH}_3\text{Cl}$  conversion and  $\text{C}_2\text{H}_3\text{Cl}$  selectivity at 700 °C (**Supplementary Fig. 19**). Meanwhile, all X-ray diffraction peaks of  $\text{Na}_2\text{WO}_4/\text{SiO}_2$  can be well attributed to  $\text{Na}_2\text{WO}_4 \cdot 2\text{H}_2\text{O}$  and  $\text{SiO}_2$ , excluding the phase transition of quartz and  $\text{Na}_2\text{WO}_4$ . These results confirmed that  $\text{Na}_2\text{WO}_4$  are the active component in manipulating  $\cdot\text{CH}_2\text{Cl}$  transformation. The significantly higher  $\text{CH}_3\text{Cl}$  conversion as compared to the oxidative pyrolysis of  $\text{CH}_3\text{Cl}$  in the empty reactor (49.1%

versus ~0%), on the other hand, suggested that the effective capture and transformation of  $\cdot\text{CH}_2\text{Cl}$  over  $\text{Na}_2\text{WO}_4$  can shift the chemical equilibrium of  $\text{CH}_3\text{Cl}$  oxy-pyrolysis towards  $\cdot\text{CH}_2\text{Cl}$  production. These findings further explained the significantly lower reaction temperature of NaWZr than the blank experiment for 46%  $\text{CH}_3\text{Cl}$  conversion (Supplementary Fig. 13).

In light of the aforementioned findings, the homogeneous-heterogeneous reaction mechanism of MCTV can be summarized as depicted in Fig. 4d. The reaction is initiated by a homogeneous  $\cdot\text{CH}_2\text{Cl}$  generation via oxy-pyrolysis, which is followed by a surface-confined  $\cdot\text{CH}_2\text{Cl}$  transformation to selectively produce  $\text{C}_2\text{H}_3\text{Cl}$ . This represents a significant advancement in controllable radical chemistry. Combined with commercial methyl chloride production via methanol and HCl reaction, we can establish an MTV process (methanol-to-VCM).



**Fig. 5 | Environmental and economic comparison of processes for VCM manufacture. (a)** Climate change impacts and **(b)** Production costs per kg of VCM via the MTV route (assuming full conversion and selectivity) are compared to the conventional EBP pathway. Results for both the fossil and green routes, depending on the hydrocarbon source, are shown. Bio-based hydrocarbon sources are discussed herein for the green routes, while other possible scenarios are displayed in Supplementary Fig. 22.

To further elucidate the practical significance of the MTV pathway on an industrial scale, we quantified its carbon footprint and production costs. Specifically, we compared the MTV process, assuming full conversion and selectivity (to gauge its full potential), with the conventional EBP route (ethylene-based balanced process for VCM synthesis). We considered two distinct scenarios for the MTV process, depending on the source of methanol: from natural gas reforming (fossil) and biomethane reforming (green). Similarly, for the EBP route, we explored two cases, distinguished by the source of ethylene: from steam reforming of hydrocarbons (fossil) and corn stover-based bioethanol dehydration (green). **Fig. 5a** displays the climate change impacts associated with the production of 1 kg of VCM. Notably, when comparing the fossil-based scenarios, we observed a substantial 24% reduction in carbon footprint. Furthermore, the switch to the green scenario, anticipated to be more applicable in the future, resulted in a significant 237% reduction in climate change impacts relative to the green ethylene analog. This substantial reduction in the future-oriented green scenario can be primarily attributed to the utilization of biomethane feedstock that results in negative net contributions to the overall impacts (on a cradle-to-gate basis) due to the biogenic nature of the carbon<sup>37</sup>. In addition to the reduction in the carbon footprint, both the current fossil-based and future green MTV scenarios demonstrated a 38% decrease in production costs relative to their ethylene-based counterparts (**Fig. 5b**). This reduction is predominantly due to the lower costs associated with C<sub>1</sub> feedstocks, specifically methanol (0.4 USD kg<sup>-1</sup> for fossil methanol), compared to ethylene (1.7 USD kg<sup>-1</sup> for fossil ethylene) used in the EBP route. Lastly, a sensitivity analysis on the MTV process revealed that the current selectivity is nearly at the target value of 69% needed to match the economic performance of the EBP pathway. Consequently, the MTV process represents a superior alternative in terms of both economic viability and environmental sustainability when compared to the state-of-the-art EBP route and will potentially play a pivotal role in establishing a more sustainable C<sub>1</sub> industry based on renewable carbon and less reliant on petroleum-derived sources.

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## Methods

### Catalyst preparation

*Synthesis of NaWZr.* NaWZr was synthesized by a co-precipitation method using  $\text{Zr}(\text{OC}_4\text{H}_9)_4$  and  $\text{WCl}_6$  as the precursors<sup>34</sup>. Typically, 9 mmol of  $\text{Zr}(\text{OC}_4\text{H}_9)_4$  and  $X$  mmol ( $X = 0 - 4$ ) of  $\text{WCl}_6$  were dissolved in 30 mL of ethanol to get a clear solution. Subsequently, a certain amount of NaOH aqueous solution (23 wt.%) was slowly added to the solution to generate precipitation. After stirring for 2 h, the mixture was transferred into a Petri dish (diameter 150 mm) to vapor the ethanol at 40 °C overnight. Afterward, the samples were aged at 85 °C for 6 h, followed by calcination at 750 °C for 5 h to get the final products. The W-to-Zr molar ratio of NaWZr is 3:9 if not elsewhere specified. NaWAl was synthesized by the same method with 9 mmol of  $\text{Al}(\text{OC}_4\text{H}_9)_3$  mixed with 3 mmol of  $\text{WCl}_6$  as the precursors. KWZr was synthesized by the same method with 9 mmol of  $\text{Zr}(\text{OC}_4\text{H}_9)_4$  mixed with 3 mmol of  $\text{WCl}_6$  as the precursors, then KOH aqueous solution (23 wt.%) was slowly added to the solution to generate precipitation. NaMoZr was synthesized by the same method with 9 mmol of  $\text{Zr}(\text{OC}_4\text{H}_9)_4$  mixed with 3 mmol of  $\text{MoCl}_5$  as the precursors.

*Synthesis of  $\text{WO}_3\text{-ZrO}_2$ .*  $\text{WO}_3\text{-ZrO}_2$  was synthesized by the same co-precipitation method with 9 mmol of  $\text{Zr}(\text{OC}_4\text{H}_9)_4$  mixed with 3 mmol of ammonium paratungstate.

*Synthesis of  $\text{Na}_2\text{WO}_4/\text{ZrO}_2$  catalyst.*  $\text{Na}_2\text{WO}_4/\text{ZrO}_2$  were prepared by an incipient-wetness impregnation method. 3 mmol of  $\text{Na}_2\text{WO}_4 \cdot 2\text{H}_2\text{O}$  was dissolved in 10 mL of deionized water. Then 9 mmol of  $\text{ZrO}_2$  was added into the clear solution. The mixture was stirred at 65 °C until dry, and then aged at 85 °C overnight. The acquired samples are denoted as  $\text{Na}_2\text{WO}_4/\text{ZrO}_2$  after calcination at 750 °C for 5 h.  $\text{Na}_2\text{WO}_4/\text{Al}_2\text{O}_3$  and  $\text{Na}_2\text{WO}_4/\text{SiO}_2$  were synthesized by the same method.

$\text{Na}_2\text{WO}_4$ ,  $\text{ZrO}_2$ ,  $\text{Al}_2\text{O}_3$ , and quartz sand ( $\text{SiO}_2$ ) were purchased from the Aladdin Reagent Co. Ltd.

### Catalyst characterization

High-angle annular dark field scanning transmission electron microscopy (HAADF-STEM) images and elemental mapping were acquired in an FEI Titan G2

80-200 ChemiSTEM microscope (200 kV) equipped with a spherical aberration corrector. High-resolution transmission electron microscopy (HRTEM) images were acquired in a spherical aberration (Cs)-corrected transmission electron microscope (FEI Titan G2 80-300) operating at an accelerating voltage of 300 kV. X-ray diffraction (XRD) patterns were recorded on a Rigaku Ultimate IV diffractometer using Cu K $\alpha$  radiation at the  $2\theta$  angle range from 5 to 80°.

### **Synchrotron-based VUV photoionization mass spectrometry (SVUV-PIMS)**

SVUV-PIMS study was carried out at the combustion beamline of the National Synchrotron Radiation Laboratory at Hefei, China. The quartz catalytic reactor was connected to the SVUV-PIMS system, where the catalyst bed was placed 60 mm away from the sampling nozzle (diameter 1.1 mm) of the mass spectrometer. All the catalysts (150 mg) were pelleted at 10 – 20 mesh before being loaded. CH<sub>3</sub>Cl, O<sub>2</sub>, and Ar in a ratio of 0.5:1:58.5 were cofed into the reactor with a total flow rate of 60 mL min<sup>-1</sup>. The in-situ experiment was carried out at 0.1 bar. The signals of  $\cdot$ CH<sub>3</sub>,  $\cdot$ CH<sub>2</sub>Cl, C<sub>2</sub>H<sub>3</sub>Cl, and C<sub>2</sub>H<sub>4</sub> were acquired at a photon energy of 10.7 eV, the signals of C<sub>2</sub>H<sub>2</sub>, C<sub>2</sub>H<sub>2</sub>Cl<sub>2</sub>, CH<sub>3</sub>Cl, and CH<sub>2</sub>Cl<sub>2</sub> were acquired at a photon energy of 11.8 eV, the signals of H<sub>2</sub>O, HCl, and CH<sub>4</sub> were acquired at a photon energy of 13 eV, and the signals of CO and CO<sub>2</sub> were collected with a photon energy of 14.6 – 14.8 eV.

### **Calculation of reaction efficiencies (RE) of NaWZr towards $\cdot$ CH<sub>2</sub>Cl radicals**

The secondary reactions of  $\cdot$ CH<sub>2</sub>Cl radicals over the catalysts could be quantified by reaction efficiencies (RE). CH<sub>3</sub>Cl, O<sub>2</sub>, and Ar in a ratio of 1.25:10:48.75 were cofed into a two-temperature-zone reactor with a total flow rate of 60 mL min<sup>-1</sup>.  $\cdot$ CH<sub>2</sub>Cl radicals were generated by the oxidative pyrolysis of CH<sub>3</sub>Cl in the gas phase at 900 °C (Zone 1), followed by reacting with 150 mg of down-stream catalysts (*e.g.*, NaWZr and quartz sand) at 650 °C (Zone 2). Gas-phase  $\cdot$ CH<sub>2</sub>Cl and its products after reacting with NaWZr and quartz were monitored by SVUV-PIMS in the low-pressure mode (2.67 mbar) to improve the signal-to-noise ratio.

RE is reported relative to quartz by using the equation:

$$RE = \frac{[\cdot\text{CH}_2\text{Cl}]_Q - [\cdot\text{CH}_2\text{Cl}]_S}{[\cdot\text{CH}_2\text{Cl}]_Q} \times 100\% \quad (8)$$

### Catalyst evaluation

*Methyl chloride to vinyl chloride (MCTV)*: The MCTV tests were conducted in a quartz fix-bed reactor tube with a length of 300 mm and an inner diameter of 9 mm under atmospheric pressure. The tube was placed in the heating furnace vertically and configured with a thermocouple in the inner tube to detect the temperature. In a typical reaction, 150 mg of NaWZr catalyst was loaded in the reactor. CH<sub>3</sub>Cl, O<sub>2</sub>, and N<sub>2</sub> in a ratio of 1:2:57 were cofed into the reactor. The total flow rate was 60 mL min<sup>-1</sup>. The products were analyzed by an online gas chromatography equipped with a flame ionization detector (FID) detector and a thermal conductivity detector (TCD) detector. CH<sub>3</sub>Cl, CH<sub>4</sub>, C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>2</sub>, C<sub>2</sub>H<sub>3</sub>Cl were quantified by FID, and CO, CO<sub>2</sub> were quantified by TCD.

The contents of all the carbon-containing products were quantified by a standard curve method. The CH<sub>3</sub>Cl conversion, products selectivity and yield were calculated using the following equations:

$$\text{CH}_3\text{Cl Conv.} = \frac{X_{\text{CH}_3\text{Cl},\text{inlet}} - X_{\text{CH}_3\text{Cl},\text{outlet}}}{X_{\text{CH}_3\text{Cl},\text{inlet}}} \times 100\% \quad (9)$$

$$\text{CH}_4 \text{ Sel.} = \frac{X_{\text{CH}_4,\text{outlet}}}{X_{\text{CH}_3\text{Cl},\text{inlet}} - X_{\text{CH}_3\text{Cl},\text{outlet}}} \times 100\% \quad (10)$$

$$\text{C}_2\text{H}_4 \text{ Sel.} = \frac{2 \times X_{\text{C}_2\text{H}_4,\text{outlet}}}{X_{\text{CH}_3\text{Cl},\text{inlet}} - X_{\text{CH}_3\text{Cl},\text{outlet}}} \times 100\% \quad (11)$$

$$\text{C}_2\text{H}_2 \text{ Sel.} = \frac{2 \times X_{\text{C}_2\text{H}_2,\text{outlet}}}{X_{\text{CH}_3\text{Cl},\text{inlet}} - X_{\text{CH}_3\text{Cl},\text{outlet}}} \times 100\% \quad (12)$$

$$\text{C}_2\text{H}_3\text{Cl Sel.} = \frac{2 \times X_{\text{C}_2\text{H}_3\text{Cl},\text{outlet}}}{X_{\text{CH}_3\text{Cl},\text{inlet}} - X_{\text{CH}_3\text{Cl},\text{outlet}}} \times 100\% \quad (13)$$

The C<sub>2</sub> products include C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>2</sub>, and C<sub>2</sub>H<sub>3</sub>Cl.

$$\text{C}_2 \text{ Sel.} = \frac{2 \times X_{\text{C}_2\text{H}_4,\text{outlet}} + 2 \times X_{\text{C}_2\text{H}_2,\text{outlet}} + 2 \times X_{\text{C}_2\text{H}_3\text{Cl},\text{outlet}}}{X_{\text{CH}_3\text{Cl},\text{inlet}} - X_{\text{CH}_3\text{Cl},\text{outlet}}} \times 100\% \quad (14)$$

$$\text{CO Sel.} = \frac{X_{\text{CO},\text{inlet}}}{X_{\text{CH}_3\text{Cl},\text{inlet}} - X_{\text{CH}_3\text{Cl},\text{outlet}}} \times 100\% \quad (15)$$

$$\text{CO}_2 \text{ Sel.} = \frac{X_{\text{CO}_2,\text{outlet}}}{X_{\text{CH}_3\text{Cl},\text{inlet}} - X_{\text{CH}_3\text{Cl},\text{outlet}}} \times 100\% \quad (16)$$

$$\text{C}_2\text{H}_3\text{Cl Yield} = \text{CH}_3\text{Cl Conv.} \times \text{C}_2\text{H}_3\text{Cl Sel.} \times 100\% \quad (17)$$

$$\text{C}_2 \text{ Yield} = \text{CH}_3\text{Cl Conv.} \times \text{C}_2 \text{ Sel.} \times 100\% \quad (18)$$

The carbon balance was calculated according to:

$$\text{Carbon balance} = \frac{X_{\text{CH}_3\text{Cl},\text{outlet}} + \sum x \times X_{\text{products},\text{outlet}}}{X_{\text{CH}_3\text{Cl},\text{inlet}}} \times 100\% \quad (19)$$

where  $x$  is the number of carbon atom in the products. (*i.e.*, CH<sub>3</sub>Cl, CH<sub>4</sub>, C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>2</sub>, C<sub>2</sub>H<sub>3</sub>Cl, CO, CO<sub>2</sub>). Generally, the carbon balance was higher than 98%.

*C<sub>2</sub>H<sub>4</sub>Cl<sub>2</sub> oxidation:* C<sub>2</sub>H<sub>4</sub>Cl<sub>2</sub> oxidation was conducted in the same reactor of MCTV. C<sub>2</sub>H<sub>4</sub>Cl<sub>2</sub> was pumped into the reactor at a flow rate of 0.5 mL h<sup>-1</sup> and vaporized on the reactor wall prior to the catalytic bed. C<sub>2</sub>H<sub>4</sub>Cl<sub>2</sub>, O<sub>2</sub>, and N<sub>2</sub> in a ratio of 1:2:31 were cofed into the reactor. The total flow rate was 80 mL min<sup>-1</sup>, and the mass of the catalyst was 150 mg. The C<sub>2</sub>H<sub>3</sub>Cl was quantified by a standard curve method. The C<sub>2</sub>H<sub>3</sub>Cl yield were calculated using the following equations:

$$\text{C}_2\text{H}_3\text{Cl Yield} = \frac{X_{\text{C}_2\text{H}_3\text{Cl},\text{outlet}}}{X_{\text{C}_2\text{H}_2\text{Cl}_2,\text{inlet}}} \times 100\% \quad (20)$$

*C<sub>2</sub>H<sub>5</sub>Cl oxidation:* C<sub>2</sub>H<sub>5</sub>Cl oxidation were conducted in the same reactor of MCTV. C<sub>2</sub>H<sub>5</sub>Cl, O<sub>2</sub>, and N<sub>2</sub> in a ratio of 1:2:57 were cofed into the reactor. The total flow rate was 60 mL min<sup>-1</sup>. 150 mg of NaWZr catalyst was loaded in the reactor. The products were analyzed by an online gas chromatography equipped with an FID detector and a TCD detector. CH<sub>4</sub>, C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>2</sub>, CH<sub>3</sub>Cl, C<sub>2</sub>H<sub>3</sub>Cl, C<sub>2</sub>H<sub>5</sub>Cl were quantified by FID, and CO, CO<sub>2</sub> were quantified by TCD. The contents of all the carbon-containing products were quantified by a standard curve method. The C<sub>2</sub>H<sub>5</sub>Cl conversion, products selectivity and yield were calculated using the following equations:

$$\text{C}_2\text{H}_5\text{Cl Conv.} = \frac{X_{\text{C}_2\text{H}_5\text{Cl},\text{inlet}} - X_{\text{C}_2\text{H}_5\text{Cl},\text{outlet}}}{X_{\text{C}_2\text{H}_5\text{Cl},\text{inlet}}} \times 100\% \quad (21)$$

$$\text{C}_2\text{H}_4 \text{ Sel.} = \frac{X_{\text{C}_2\text{H}_4,\text{outlet}}}{X_{\text{C}_2\text{H}_5\text{Cl},\text{inlet}} - X_{\text{C}_2\text{H}_5\text{Cl},\text{outlet}}} \times 100\% \quad (22)$$

$$\text{C}_2\text{H}_3\text{Cl Sel.} = \frac{X_{\text{C}_2\text{H}_3\text{Cl},\text{outlet}}}{X_{\text{C}_2\text{H}_5\text{Cl},\text{inlet}} - X_{\text{C}_2\text{H}_5\text{Cl},\text{outlet}}} \times 100\% \quad (23)$$

$$\text{C}_2\text{H}_4 \text{ Yield} = \text{C}_2\text{H}_5\text{Cl Conv.} \times \text{C}_2\text{H}_4 \text{ Sel.} \times 100\% \quad (24)$$

$$\text{C}_2\text{H}_3\text{Cl Yield} = \text{C}_2\text{H}_5\text{Cl Conv.} \times \text{C}_2\text{H}_3\text{Cl Sel.} \times 100\% \quad (25)$$

## Economic and environmental assessment

The process models (**Supplementary Fig. 20** based on full conversion and selectivity and **Supplementary Fig. 21** based on current conversion and selectivity) of

the MTV route were developed in Aspen Plus v12, using standard unit operations to simulate reactions, temperature and pressure changes, and separations. The results of the simulation, including mass and energy inputs and outputs as well as sizes of process units, were then utilized for conducting an economic and environmental assessment. **Supplementary Table 3** and **4** display the mass balance of the MTV plant at full and current conversion and selectivity, respectively. The economic assessment considers operational and capital expenditures (OPEX and CAPEX) for the reference year 2022. The CAPEX and OPEX terms were calculated as in Medrano-García *et al.*<sup>38</sup>, from where we retrieved the economic performance of the EBP route. Specifically, the CAPEX term was determined using correlations from Sinnott and Towler<sup>39</sup>, considering installation factors for each equipment unit and annualizing the total value using the annual capital charge ratio. **Supplementary Table 5** presents the prices of feedstock and utilities used in the OPEX estimation of both the MTV and EBP routes.

Next, the carbon footprint was quantified following an attributional life cycle assessment (LCA) in accordance with the ISO 14044/14040 standards<sup>40,41</sup>. The functional unit is 1 kg of VCM produced following a cradle-to-gate scope, including all activities from raw materials acquisition to the production of VCM at the plant. The cradle-to-gate scope is adopted because we assume that the end-use phase will be the same regardless of the synthesis route. The mass and energy flows of the EBP route were taken from Medrano-García *et al.*<sup>38</sup>, while those for the MTV route were obtained from the process model developed in this work. These data enable us to model the foreground system (chemical plant), while data for modeling the background system (all activities supplying inputs to the chemical plant) were primarily sourced from the Ecoinvent v3.8 database<sup>42</sup>. We consider the 100-year global warming potentials (GWPs) as implemented in the IPCC 2013 methodology<sup>43</sup>. The inventories used to calculate the carbon footprint for both the MTV and EBP routes are shown in **Supplementary Table 6**. The breakeven selectivity of the fossil MTV route relative to the state-of-the-art EBP pathway (*i.e.*, the minimum selectivity considering the current conversion of 65.4% that would make the MTV process economically competitive against the EBP analog) was obtained from a sensitivity analysis performed on the



Aspen simulation based on current conversion and selectivity (*i.e.*, the current experimental values reported in this article).

### **Data availability**

All the data supporting the findings of this study are available within the article and its Supplementary Information files or from the corresponding authors upon reasonable request.

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### **Author contributions**

†These authors contributed equally to this work. J.F. and S.Z. designed the study. Y.W., and S.Z. performed most of the experiments. Y.W., X.C., Y.Z., and J.L. synthesized the catalysts. Y.W., K.W., and Y.W. performed the structural characterization of catalysts. Y.W., Y.P., K.W., J.H., and C.L. performed the in-situ SVUV-PIMS study. A.N., G.G.-G. and J.P.-R. conceived, conducted, and analyzed the process simulations. Y.W., S.Z., A.N., G.G.-G., J.P.-R., and J.F. wrote the paper. The other authors performed some of the experiments and revised the paper.

**Competing interests:** JF and SZ are named in patent applications (application numbers: CN202111211376.3, PCT/CN2021/124519, and US18032338) relating to this work. The remaining authors declare no competing interests.

### **Additional information**

Supplementary Information accompanies this paper at <https://doi.org/10.1038/xxxx>.