New functional form to describe the temperature dependence of liquid phase reaction rates

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ABSTRACT

9 Chemical reactions in subcritical or near-critical solvents hold significant promise for numerous industrial and environmental applications. The Arrhenius equation is typically used to describe 11 the temperature dependence of reaction rates, yet it often falls short in capturing the behavior Liquid phase reaction rates near critical points of solvents. To address this limitation, we ¹³ Non-Arrhenius behavior **propose a** novel functional form that can correctly describe the temperature trends of liquid phase rate constants from room temperature up to the critical temperature of a solvent. The 15 Subcritical solvent 15 proposed scheme uses four kinetic parameters with physical implications, two accounting for the gas phase contribution and the other two accounting for the solvation effect on reactions. The 17
17 new functional form can accurately reproduce the anomalous temperature dependence of liquid phase rate constants in subcritical and near-critical regimes that the Arrhenius equation fails to capture. Furthermore, our preliminary finding suggests that the kinetic parameters associated with the solvation terms can be computed with ab initio approaches to estimate the temperature- dependent rate constants of liquid phase reactions based on their corresponding rate constants in gas phase. The proposed functional form provides an alternative approach to describe the non-Arrhenius behavior of diverse liquid phase reactions across a wide range of temperature.

²⁵ **1. Introduction**

 Chemical reactions in subcritical or near-critical solvents have been the subject of great interest in many industrial $_{27}$ and environmental applications [\[1,](#page-12-0) [2,](#page-12-1) [3,](#page-12-2) [4\]](#page-12-3). Kinetic rates and selectivity of various industrially relevant reactions, such as dehydration of alcohols, Diels-Alder, alkylation, and cyclization, can be enhanced in subcritical water or organic solvents [\[1,](#page-12-0) [5,](#page-12-4) [6,](#page-12-5) [7\]](#page-12-6). Waste plastics can be effectively decomposed and recycled by depolymerization reactions in subcritical water or alcohols [\[8,](#page-12-7) [9,](#page-12-8) [10,](#page-12-9) [11\]](#page-12-10). Subcritical fluids also serve as excellent reaction media for the conversion of biomass to fuels and other valuable chemicals [\[12,](#page-12-11) [13,](#page-12-12) [14\]](#page-12-13). In nuclear power plants, subcritical or supercritical water is used as a coolant for a reactor, and a knowledge of the kinetic mechanisms of water radiolysis is essential for designing a safe water-coolant reactor that can suppress the formation of oxidizing species and mitigate corrosion [\[15,](#page-12-14) [16,](#page-12-15) [17,](#page-12-16) [18\]](#page-12-17).

³⁵ Due to the high interest in the chemistry of subcritical systems, kinetic rates of many liquid phase reactions have been ³⁶ measured and investigated under subcritical conditions. They are typically measured at multiple temperatures under ³⁷ constant pressure and fitted to the Arrhenius equation, which can then be used to estimate rate constants at different ³⁸ temperatures. The Arrhenius equation [\[19\]](#page-12-18) is the most widely used functional form for describing the temperature (T) 39 dependence of a rate constant (k) and has a following form:

$$
k = A \exp\left(\frac{-E_a}{RT}\right) \tag{1}
$$

where A is the pre-exponential factor, E_a is the activation energy, and R is the universal gas constant. The Arrhenius α_1 equation assumes a linear relationship between ln k and $1/T$ and treats A and E_a as temperature-independent

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⁴² parameters. While most reactions show the linear dependence, many liquid phase reactions start to exhibit non- Arrhenius behavior as temperature approaches a critical point of a solvent [\[15,](#page-12-14) [16,](#page-12-15) [20,](#page-12-19) [21,](#page-12-20) [22,](#page-12-21) [18\]](#page-12-17). Near a critical point, the physicochemical properties of a solvent change dramatically with a slight variation of temperature, and as a result, rapid slowing-down or acceleration of rate constants are observed for many liquid phase reactions at elevated temperatures. A modified version of the Arrhenius equation is frequently used to describe more complex temperature dependence of a rate constant:

$$
k = AT^n \exp\left(\frac{-E_a}{RT}\right) \tag{2}
$$

48 where n is introduced as an additional empirical parameter. The modified equation can cover a wider temperature range ⁴⁹ than the conventional Arrhenius equation, but it still fails to capture the anomalous temperature dependence of liquid ⁵⁰ phase reactions in subcritical regions.

 \mathbf{I}_{51} In an alternative approach, the temperature dependence of a liquid phase rate constant (k_{liq}) is explained in terms of 52 gas phase and solvation contributions [\[23,](#page-12-22) [24,](#page-12-23) [25,](#page-12-24) [16,](#page-12-15) [26\]](#page-13-0):

$$
k_{\rm liq} = A \exp\left(-\frac{E_a + \Delta \Delta G_{\rm solv}^{\ddagger}}{RT}\right) \tag{3}
$$

⁵³ where $\Delta\Delta G_{\text{solv}}^{\ddagger}$ represents the solvation effect on the free energy of activation, and A and E_a are the gas phase kinetic parameters of the same reaction. The $\Delta \Delta G_{\text{solv}}^{\ddagger}$ term accounts for the difference between the solvation free energies of ϵ ₅₅ the reactants and transition state (TS). This approach assumes A and E_a to be constant and attempts to describe the ⁵⁶ non-Arrhenius behavior of k_{liq} in terms of the temperature dependence of $\Delta\Delta G_{solv}^{\ddagger}$. As temperature approaches the ⁵⁷ critical point of a solvent, the solvent's dielectric constant changes significantly, causing the $\Delta\Delta G_{\text{solv}}^{\ddagger}$ value to change 58 a lot for the reaction whose reactants and TS have different dipole moments. Marrone, Tester, and their co-workers 59 [\[23,](#page-12-22) [24\]](#page-12-23) adopted the Kirkwood theory [\[27\]](#page-13-1) to express $\Delta\Delta G_{\text{solv}}^{\ddagger}$ as a function of the dielectric constant of a solvent and ⁶⁰ the dipole moments and molecular radii of reactants and TS. While they were able to reproduce the experimental data μ of CH₂Cl₂ hydrolysis from room temperature up to the critical point of water, their method relies on several variables ⁶² that cannot be easily fitted to experimental data.

63 An alternative functional form that can describe the temperature dependence of k_{liq} with minimal empirical parameters ⁶⁴ is needed. Previously, we have developed a correlation to predict the solvation free energy of a species from around 65 250 K up to the critical temperature of a solvent with only two solvation properties [\[28\]](#page-13-2). The correlation was able to ⁶⁶ provide accurate predictions for a variety of solvent-solute pairs only based on the solvation free energy and solvation ⁶⁷ enthalpy at 298 K and the solvent's density. In this work, we apply the same correlation to estimate the solvation ⁶⁸ free energies of the reactants and TS of a reaction, hence estimating the $\Delta\Delta G_{\rm solv}^\ddag$ across a range of temperatures. Our ⁶⁹ proposed method only needs two parameters to express the temperature dependence of $\Delta\Delta G_{\rm solv}^{\ddagger}$, which can be easily τ ⁰ fitted to experimental data or potentially calculated using ab initio methods. The devised method can be combined with 71 the Arrhenius equation to accurately reproduce the experimental rate constants of diverse liquid phase reactions for a ⁷² wide range of temperature.

⁷³ **2. Method**

⁷⁴ **2.1. Derivation of the new functional form**

⁷⁵ The overview of our approach is illustrated in Figure [1.](#page-2-0) Our method uses the previously developed correlation [\[28\]](#page-13-2) to ⁷⁶ approximate the temperature dependence of $\Delta\Delta G_{\rm solv}^{\ddagger}$ and subsequently employs eq [3](#page-1-0) to express the liquid phase rate

- ⁷⁷ constant as a function of Arrhenius parameters and $\Delta\Delta G_{\text{solv}}^{\ddagger}$. Eq [3](#page-1-0) is derived based on the assumption that the same
- π ⁸ reaction occurs in both gas and liquid phases [\[25\]](#page-12-24), which allows the liquid phase rate constant to be expressed in terms

Figure 1: Overview of the method for estimating the temperature dependence of a liquid phase rate constant.

⁷⁹ of the corresponding gas phase rate constant (k_{gas}) and solvation correction [\[25\]](#page-12-24):

$$
k_{\rm liq} = k_{\rm gas} \exp\left(\frac{-\Delta\Delta G_{\rm solv}^{\ddagger}}{RT}\right) = A \exp\left(-\frac{E_a + \Delta\Delta G_{\rm solv}^{\ddagger}}{RT}\right) \tag{4}
$$

⁸⁰ In eq [4,](#page-2-1) it is also assumed that k_{gas} follows the Arrhenius form ($k_{\text{gas}} = A \exp\left(\frac{-E_a}{RT}\right)$) and the transmission coefficient ⁸¹ for quantum tunneling effects is similar between gas phase and liquid phase. The solvation correction term, $\Delta\Delta G_{\text{solv}}^{\ddagger}$ ⁸² is defined as the difference between the solvation free energy of the TS ($\Delta G_{\text{solv}}^{\text{TS}}$) and the solvation free energy of the $\text{frac}(\Delta G_{\text{solv}}^{\text{R}})$:

$$
\Delta \Delta G_{\text{solv}}^{\ddagger} = \Delta G_{\text{solv}}^{\text{TS}} - \Delta G_{\text{solv}}^{\text{R}_i} \tag{5}
$$

⁸⁴ Solvation free energy (ΔG_{solv}) is a change in Gibbs free energy associated with the transfer of a solute molecule from ⁸⁵ a gas phase to a solution phase. In our earlier work [\[28\]](#page-13-2), we combined two existing correlations [\[29,](#page-13-3) [30\]](#page-13-4), which were 86 developed based on thermodynamic relationships, and formulated a piecewise function that can predict the solvation 87 free energy of a solvent-solute pair for a broad range of temperature:

For
$$
T \leq 0.75T_{\rm c}
$$
:

$$
\Delta G_{\text{solv}}(T) = a + b(1 - T_{\text{r}})^{0.355} + c(T_{\text{r}})^{0.59} \exp\left(1 - T_{\text{r}}\right) + RT \ln\left(\frac{\rho_{\text{g}}(T)}{\rho_{\text{l}}(T)}\right) \tag{6}
$$

88

For $0.75T_c \leq T < T_c$:

$$
\Delta G_{\text{solv}}(T) = d \left(\frac{\rho_1(T)}{\rho_c} - 1 \right) + RT \ln \left(\frac{\rho_g(T)}{\rho_1(T)} \right) \tag{7}
$$

where T_c is the solvent's critical temperature, T_r is the reduced temperature ($T_r = \frac{1}{T}$ ⁸⁹ where T_c is the solvent's critical temperature, T_r is the reduced temperature ($T_r = \frac{T_c}{T_c}$), ρ_c is the solvent's critical density, ⁹⁰ and $\rho_g(T)$ and $\rho_l(T)$ are the solvent's gas-phase and liquid-phase saturation densities at temperature T, respectively.

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 91 The lower case letters, a, b, c, and d, represent the empirical parameters that are unique to each solvent-solute pair. We

 92 have previously demonstrated that the piecewise function (eq [6](#page-2-2) and [7\)](#page-2-3) can provide accurate Δ G_{solv} predictions up to

⁹³ the critical temperature of a solvent for various closed-shell compounds in solution [\[28\]](#page-13-2).

In this work, we assume that the piecewise function is applicable to any compounds, transition states, and particles 95 95 dissolved in a solvent. We plug eq [6](#page-2-2) and [7](#page-2-3) into eq 5 to get the following relationships:

For
$$
T \le 0.75T_c
$$
:
\n
$$
\Delta \Delta G_{\text{solv}}^{\ddagger}(T) = (a^{TS} - a^R) + (b^{TS} - b^R)(1 - T_r)^{0.355} + (c^{TS} - c^R)(T_r)^{0.59} \exp(1 - T_r)
$$
\n(8)

96

For $0.75T_c \leq T < T_c$:

$$
\Delta \Delta G_{\text{solv}}^{\ddagger}(T) = (d^{\text{TS}} - d^{\text{R}}) \left(\frac{\rho_1(T)}{\rho_c} - 1 \right)
$$
 (9)

⁹⁷ where a^{TS} , b^{TS} , c^{TS} , and d^{TS} represent the empirical parameters of the TS and a^R , b^R , c^R , and d^R represent the empirical ⁹⁸ parameters of the reactant. The equations can be simplified by lumping the two empirical parameters as follow:

For $T \leq 0.75T_c$:

$$
\Delta \Delta G_{\text{solv}}^{\ddagger}(T) = a + b(1 - T_{\text{r}})^{0.355} + c(T_{\text{r}})^{0.59} \exp\left(1 - T_{\text{r}}\right) \tag{10}
$$

99

For
$$
0.75T_c \leq T < T_c
$$
:

$$
\Delta \Delta G_{\text{solv}}^{\ddagger}(T) = d \left(\frac{\rho_1(T)}{\rho_c} - 1 \right)
$$
 (11)

100 where a, b, c , and d now represent the empirical parameters unique to each reaction-solvent pair. Eq [11](#page-3-0) ensures that $\Delta \Delta G_{\text{soly}}^{\ddagger}$ approaches a correct limit of zero as temperature approaches a critical point. More details on the critical limit 102 can be found in the dedicated work of Japas and Levelt Sengers [\[30\]](#page-13-4) and in our prior study [\[28\]](#page-13-2).

103 In order to solve for the four empirical parameters (a, b, c, d) , four equations are needed. We use the same approach ¹⁰⁴ as our earlier work [\[28\]](#page-13-2) and obtain two equations by forcing the piecewise function shown in eq [10](#page-3-1) and [11](#page-3-0) to match in ¹⁰⁵ value and gradient at the transition temperature:

At
$$
T = 0.75T_c
$$
:

106

$$
a + b(1 - T_r)^{0.355} + c(T_r)^{0.59} \exp(1 - T_r) = d\left(\frac{\rho_1(T)}{\rho_c} - 1\right)
$$
\n(12)

107

$$
-\frac{0.355b}{T_c}(1-T_r)^{-0.645} + \frac{c \exp(1-T_r)}{T_c} \left(0.59(T_r)^{-0.41} - (T_r)^{0.59}\right) = \frac{d}{\rho_c} \frac{d\rho_1}{dT}
$$
(13)

108 The $\Delta \Delta G_{\text{solv}}^{\ddagger}$ values or its gradients (enthalpy or entropy) at two temperatures are needed to obtain two additional 109 equations. Our two prior studies [\[31,](#page-13-5) [32\]](#page-13-6) demonstrated that the ab initio COSMO-RS method can provide reasonable **110** estimations of $\Delta\Delta G_{\text{solv}}^{\ddagger}$ and $\Delta\Delta H_{\text{solv}}^{\ddagger}$ at 298 K for various liquid phase reactions. Thus, we formulate two more ₁₁₁ equations based on the $\Delta \Delta G_{\text{solv}}^{\ddagger}$ and $\Delta \Delta H_{\text{solv}}^{\ddagger}$ values at 298 K:

 $At T = 298 K$:

112

$$
a + b(1 - T_{\rm r})^{0.355} + c(T_{\rm r})^{0.59} \exp(1 - T_{\rm r}) = \Delta \Delta G_{\rm solv}^{\ddagger} (298 \text{ K}) \tag{14}
$$

113

$$
-\frac{0.355b}{T_c}(1-T_r)^{-0.645} + \frac{c \exp(1-T_r)}{T_c} \left(0.59(T_r)^{-0.41} - (T_r)^{0.59}\right)
$$

=
$$
-\frac{\Delta \Delta H_{\text{solv}}^{\ddagger}(298 \text{ K}) - \Delta \Delta G_{\text{solv}}^{\ddagger}(298 \text{ K})}{298 \text{ K}} \quad (15)
$$

where the right-hand side of eq [15](#page-4-0) is equivalent to the temperature gradient of $\Delta\Delta G_{\rm solv}^{\ddagger}$ at 298 K:

$$
\frac{d\Delta\Delta G_{\text{solv}}^{\ddagger}}{dT}\Big|_{T=298\text{ K}} = -\Delta\Delta S_{\text{solv}}^{\ddagger}(298\text{ K}) = -\frac{\Delta\Delta H_{\text{solv}}^{\ddagger}(298\text{ K}) - \Delta\Delta G_{\text{solv}}^{\ddagger}(298\text{ K})}{298\text{ K}}
$$
(16)

115 With a set of four equations (eq [12](#page-3-2) - [15\)](#page-4-0) that are linear with respect to a , b , c , and d , we can solve for those four ¹¹⁶ parameters based on ΔΔ $G_{\text{solv}}^{\ddagger}$ (298 K), ΔΔ $H_{\text{solv}}^{\ddagger}$ (298 K), and the saturation densities ($\rho_1(T)$) and critical properties (T_c , φ_c) of a solvent. The densities and properties of many common solvents can be obtained using open-source models, ¹¹⁸ such as fluid thermodynamics packages CoolProp [\[33\]](#page-13-7) and Clapeyron.jl [\[34\]](#page-13-8), and a machine learning model developed ¹¹⁹ by Biswas et al.[\[35\]](#page-13-9) Since the solvent's properties are easily obtainable from the existing models, we can treat them as ¹²⁰ known values. Thus, only $\Delta \Delta G_{\text{solv}}^{\ddagger}$ (298 K) and $\Delta \Delta H_{\text{solv}}^{\ddagger}$ (298 K) are needed to solve for the four empirical parameters and hence obtain $\Delta \Delta G_{\text{solv}}^{\ddagger}$ at any temperature. The computed $\Delta \Delta G_{\text{solv}}^{\ddagger}(T)$ values can be subsequently combined with the gas phase kinetic parameters (A, E_a) as shown in [4](#page-2-1) to obtain a liquid phase rate constant.

¹²³ In summary, our proposed approach allows us to describe the temperature dependence of a liquid phase rate constant in terms of four kinetic parameters: (1) A, (2) E_a , (3) $\Delta \Delta G_{\text{solv}}^{\ddagger}$ (298 K), and (4) $\Delta \Delta H_{\text{solv}}^{\ddagger}$ (298 K). Here, A and E_a 124 account for the Arrhenius behavior while $\Delta \Delta G_{\text{solv}}^{\ddagger}$ (298 K) and $\Delta \Delta H_{\text{solv}}^{\ddagger}$ (298 K) account for the solvation effect that ¹²⁶ exhibits non-Arrhenius behavior.

 The method developed in our earlier study [\[28\]](#page-13-2) estimates the temperature-dependent solvation free energy at a solvent's saturation pressure, and thus $\Delta \Delta G_{\text{solv}}^{\ddagger}$ is also estimated along a solvent's saturation curve. This indicates that the gas phase rate constant (k_{gas}) in eq [4](#page-2-1) should correspond to the values at the saturation pressure for pressure-dependent reactions. Yet, our earlier work [\[28\]](#page-13-2) demonstrated that the method can provide reasonable predictions of solvation free energy at higher pressures as well as long as the temperature is not too close to the critical temperature of the solvent ($T < 0.8T_c$). Near a critical point, the pressure effect becomes more significant, and therefore our method is expected to have a higher error if the pressure deviates from the saturation pressure at elevated temperatures $(0.8T_c < T)$. Moreover, our method assumes the dilute limit, which may not be valid if a substantial amount of a reactant is dissolved or if the solvent is a reactant.

¹³⁶ **2.2. Method validation: fitting the four kinetic parameters**

137 The proposed method is tested by fitting the four kinetic parameters $(A, E_a, \Delta\Delta G_{\text{solv}}^{\ddagger}(298 \text{ K}), \Delta\Delta H_{\text{solv}}^{\ddagger}(298 \text{ K}))$ to the ¹³⁸ experimental data of liquid phase rate constants and calculating the rate constants with the fitted parameters. For each ¹³⁹ reaction, the four kinetic parameters are optimized by minimizing the following loss function:

$$
L = \sqrt{\frac{\sum_{i=1}^{N} \left(\log_{10}(k_{\text{liq,expt}}) - \log_{10}(k_{\text{liq,calc}}) \right)^2}{N}} + \lambda \left((\Delta \Delta G_{\text{solv}}^{\ddagger} (298 \text{ K}))^2 + (\Delta \Delta H_{\text{solv}}^{\ddagger} (298 \text{ K}))^2 \right)
$$
(17)

140

$$
k_{\text{liq,calc}} = f\left(A, E_a, \Delta\Delta G_{\text{solv}}^{\ddagger}(298 \text{ K}), \Delta\Delta H_{\text{solv}}^{\ddagger}(298 \text{ K})\right)
$$

where λ is a regularization term, $k_{liq,expt}$ is an experimental rate constant, and $k_{liq,calc}$ is a calculated rate constant 142 which is a function of the kinetic parameters to be optimized. The regularization term is added in eq [17](#page-4-1) to prevent the 143 solvation parameters ($\Delta \Delta G_{\text{solv}}^{\ddagger}$ (298 K), $\Delta \Delta H_{\text{solv}}^{\ddagger}$ (298 K)) from being overfitted to the experimental data. The optimal

value of λ is identified as 0.0001 when a kcal/mol unit is used for the solvation parameters in the loss function. Only 145 the solvation parameters are regularized as their values typically fall within ± 7 kcal/mol for most reactions and larger ¹⁴⁶ values are rare unless the polarity of the TS is significantly different from that of the reactants [\[32\]](#page-13-6). We also found that ¹⁴⁷ adding the regularization term for the solvation parameters provides more reasonable results for the optimized kinetic ¹⁴⁸ parameters.

The initial guesses of $\Delta\Delta G_{\text{solv}}^{\ddagger}$ (298 K) and $\Delta\Delta H_{\text{solv}}^{\ddagger}$ (298 K) are arbitrarily set to -1 kcal/mol and -1.5 kcal/mol, $_{150}$ respectively, while the initial guesses of the Arrhenius parameters, A and E_a , are determined based on the experimental $_{151}$ data. To find the best initial guesses for A and E_a , the ln k vs $1/T$ plot is first made using the experimental data, and a $\frac{1}{152}$ linear line is fitted only using the data points at a lower temperature region (around $T < 0.75T_c$) where the Arrhenius behavior is observed. Then the fitted linear line is vertically shifted to match the experimental $\ln k$ values near T_c . Finally, the initial guesses of A and E_a are made based on the y-intercept (y-intercept = ln A) and slope (slope = $-\frac{E_a}{R}$ ¹⁵⁴ Finally, the initial guesses of A and E_a are made based on the y-intercept (y-intercept = ln A) and slope (slope = $-\frac{E_a}{R}$) ¹⁵⁵ of the resulting linear line. The vertical shifting step is necessary when generating the linear line because as temperature approaches T_c , $\Delta \Delta G_{solv}^{\ddagger}$ approaches zero (see eq [11\)](#page-3-0) and k_{liq} consequently approaches $A \exp \left(\frac{-E_a}{RT_c} \right)$ ¹⁵⁶ approaches T_c , $\Delta \Delta G_{\text{solv}}^+$ approaches zero (see eq 11) and k_{liq} consequently approaches $A \exp\left(\frac{-E_a}{RT_c}\right)$ (see eq [4\)](#page-2-1). By 157 ensuring that the linear line passes through the experimental $\ln k$ values near T_c , we can generate good initial guesses ¹⁵⁸ that lead to a correct critical limit.

¹⁵⁹ The parameters are optimized with a constrained optimization function from the SciPy package [\[36\]](#page-13-10). The bounds of $\Delta \Delta G_{\text{solv}}^{\ddagger}$ (298 K) and $\Delta \Delta H_{\text{solv}}^{\ddagger}$ (298 K) are empirically set to (−6 kcal/mol, 4 kcal/mol) and (−10 kcal/mol, 8 kcal/mol), 161 respectively. For A and E_a , two different sets of bounds are used to obtain two sets of optimized parameters, and the 162 best set that gives the lowest residual error is selected as the final optimized values. The two sets of bounds used for A a_{init} are (log₁₀ $A_{\text{init}} - 1$, log₁₀ $A_{\text{init}} + 1$) and (log₁₀ $A_{\text{init}} - 2$, log₁₀ $A_{\text{init}} + 2$) where A_{init} is the initial guess determined from the steps described previously. The bounds used for E_a are $(-\frac{E_{a,\text{init}}}{1000F})$ $\frac{E_{a,\text{init}}}{1000R} - 12, -\frac{E_{a,\text{init}}}{1000R}$ $\frac{E_{a,\text{init}}}{1000R} + 12$) and $\left(-\frac{E_{a,\text{init}}}{1000R}\right)$ 164 the steps described previously. The bounds used for E_a are $(-\frac{2a,\text{init}}{1000R} - 12, -\frac{2a,\text{init}}{1000R} + 12)$ and $(-\frac{2a,\text{init}}{1000R} - 12, 0)$ where $E_{a,init}$ is the initial guess. Finally, k_{liq} are calculated based on the optimized kinetic parameters and compared with the ¹⁶⁶ experimental data.

¹⁶⁷ **2.3. Method validation: calculating the solvation kinetic parameters**

168 We additionally calculate k_{liq} using experimental k_{gas} data and the solvation parameters computed from ab initio methods to test whether our proposed method can yield accurate predictions without using any experimental k_{liq} $_{170}$ data. The solvation parameters, $\Delta \Delta G_{\text{solv}}^{\ddagger}$ (298 K) and $\Delta \Delta H_{\text{solv}}^{\ddagger}$ (298 K), are calculated based on the computational 171 approach described in Ref. [31;](#page-13-5) the geometries of reactants and TS are optimized at the ω B97XD/def2-TZVP level ¹⁷² of theory [\[37,](#page-13-11) [38\]](#page-13-12) using Gaussian16 [\[39\]](#page-13-13), followed by the single-point COSMO-RS [\[40,](#page-13-14) [41,](#page-13-15) [42\]](#page-13-16) calculations at the 173 BP-TZVPD-FINE level [\[43,](#page-13-17) [44,](#page-13-18) [45,](#page-13-19) [46\]](#page-13-20). The COSMO-RS calculations are performed using TURBOMOLE 7.5 [\[47,](#page-13-21) [48\]](#page-13-22) and COSMOtherm (release 2021) [\[49\]](#page-13-23). Temperature-dependent $\Delta\Delta G_{\text{solv}}^{\ddagger}$ values are then calculated using the computed ¹⁷⁵ $\Delta \Delta G_{\text{solv}}^{\ddagger}$ (298 K) and $\Delta \Delta H_{\text{solv}}^{\ddagger}$ (298 K) and combined with experimental k_{gas} data to obtain k_{liq} using eq [4.](#page-2-1)

¹⁷⁶ **3. Experimental data**

177 Experimental data of liquid phase rate constants are collected from literature to evaluate the method. The data collection is limited to the reactions that have experimental rate constants across a wide range of temperature and exhibit non- Arrhenius behavior at elevated temperature. A total of 14 reactions that occur in water are collected as listed in Table [1.](#page-6-0) Due to the scarcity of experimental data, we were unable to find the reaction data for solvents other than water.

81 As Table 1 indicates, many of these reactions are fast bimolecular reactions that are affected by diffusion rates. 182 Bimolecular liquid phase reactions with rate constants greater than around 3×10^9 M⁻¹s⁻¹ at 298 K are usually influenced by diffusion limitations [\[15\]](#page-12-14). While diffusion effects diminish as temperature increases, it can affect the reaction rates up to around 473 K for fast reactions. For diffusion-controlled reactions, experimentally measured or observed rate constants do not correspond to their intrinsic rate constants but are the function of both diffusion and intrinsic rate constants. Observed rate constants (k_{obs}) of bimolecular reactions can be estimated as:

$$
k_{\text{obs}} = \left(\frac{1}{k_{\text{diff}}} + \frac{1}{k_{\text{liq}}}\right)^{-1} \tag{18}
$$

where k_{diff} is the diffusion rate constant and k_{liq} is the intrinsic liquid phase rate constant.

188 The original data sources [\[15,](#page-12-14) [50,](#page-13-24) [21\]](#page-12-20) of Reactions 1 and 2 reported the estimated k_{liq} along with the k_{obs} . However, the majority of the studies only reported the k_{obs} , which are assumed to be diffusion-controlled to a certain extent. Since the true k_{liq} could not be determined for those reactions, we fitted our functional form to the experimental k_{obs} data ¹⁹¹ for the fitting method described in Section [2.2.](#page-4-2) We did not separately account for the diffusion effects in our method as it is challenging to make accurate estimations of k_{diff} for the reactions investigated in this study and diffusion effects ¹⁹³ become negligible near a critical temperature of a solvent. It is shown that our method can still accurately reproduce ¹⁹⁴ the experimental rate constants of the diffusion-limited reactions as further discussed in the results section.

¹⁹⁵ **4. Results and discussion**

¹⁹⁶ **4.1. Fitting the functional form**

¹⁹⁷ The results of the proposed functional form that are fitted to the experimental data are shown in Figure [2](#page-7-0) as blue solid lines ($k_{\text{liq, fitted}}$) for individual reactions. The results of the fitted Arrhenius equation ($k_{\text{Arrhenius, fitted}}$, orange dashed line) are also provided in the figure for comparison. The experimental data of intrinsic rate constants ($k_{\text{liq, expt}}$) and $_{200}$ observed rate constants ($k_{obs, \text{expt}}$) are represented in circular markers and diamond markers, respectively.

 Figure [2](#page-7-0) shows that our functional form outperforms the Arrhenius equation for all reactions. Our method can accurately reproduce the experimental rate constants for the entire temperature range up to the critical temperature of the solvent while the Arrhenius equation starts to deviate from the experimental data above around 400 K. The mean absolute error (MAE) and root-mean-square error (RMSE) of each method are summarized in Table [2.](#page-8-0) Three different errors 205 are computed by using (1) the entire range of temperature (All T), (2) temperature below 400 K (T \leq 400 K), and (3) ²⁰⁶ temperature above 400 K (400 K $\lt T$). It can be seen that our fitted functional form has a much lower error with a 207 MAE/RMSE of 0.07/0.09 in $\log_{10} k_{liq}$ for the entire T range compared to the Arrhenius equation that has a MAE/RMSE ²⁰⁸ of 0.25/0.35 in $\log_{10} k_{\text{liq}}$. Below 400 K, both the proposed functional form and the Arrhenius equation have similar fitting errors. However, at elevated temperatures above 400 K, the Arrhenius form cannot fit to the experimental data well and has a substantially higher error. Our proposed functional form, on the contrary, has a consistently low error for all temperature ranges.

²¹² From Figure [2,](#page-7-0) it can be seen that the reactions mostly exhibit the Arrhenius behavior at moderate temperatures and ²¹³ show a rapid decrease or increase in rate constants above approximately 450 K. The reactions have different shapes of ²¹⁴ curves for the $\log_{10} k$ vs 1000/T plots, and the results indicate that our method is able to replicate all of these different

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Figure 2: Comparison of the proposed functional form ($k_{liq, fitted}$, solid blue line) and the Arrhenius equation ($k_{Arrhenius, fitted}$, orange dashed line) fitted to the experimental rate constants. All reactions occur in water.

Comparison of the overall $\log_{10} k_{liq}$ errors for each fitted functional form. Each reaction is weighted equally.

 curvatures. The only exception is Reaction 4 for which our fitted function has a relatively higher error. Reaction 4 shows an unusual trend where the rate constants start to decrease at around 460 K and then rapidly increase near the critical temperature. Large deviations among the experimental data are also observed for Reaction 4 near the critical point as there is one data point that has a much lower value compared to other data points at around the critical temperature. Thus, it is possible that the relatively poor performance of our method on Reaction 4 is due to its high experimental uncertainty.

₂₂₁ The results also show that our method can accurately reproduce the observed rate constants of the reactions that are influenced by diffusion limits. It is likely that the diffusion rate only affects the degree of the curvature of the $\log_{10} k$ 223 vs 1000/T plot and does not dramatically change the general temperature dependence for the reaction. Since our ²²⁴ proposed functional form is able to fit to different shapes of curves, it is likely that it can also fit to the observed rate ²²⁵ constants of the diffusion-controlled reactions. To further validate our reasoning, we additionally fitted our functional $\frac{1}{226}$ form to both $k_{\text{liq, expt}}$ and $k_{\text{obs, expt}}$ data for Reactions 1 and 2, which had both types of data available. The results ₂₂₇ are presented in Figure [3.](#page-8-1) It can be seen that our method can correctly describe the temperature dependence of both ²²⁸ intrinsic and observed rate constants. As we expected, the two types of data differ only in the degree of curvature, ²²⁹ and their temperature trends are generally similar. Due to a lack of data, we are unable to perform the same analysis ²³⁰ for other reactions. Nonetheless, since our method shows good agreements with the experimental data for both the ²³¹ reactions with and without diffusion effects as indicated by Figure [2,](#page-7-0) we anticipate the results to be similar for other ²³² reactions.

Figure 3: Comparison of the proposed functional forms fitted to the intrinsic liquid phase rate constants (k_{lin} , blue) and observed rate constants $(k_{obs}, green)$.

²³³ The fitted empirical parameters of each reaction are provided in Table [3.](#page-9-0) The parameters have reasonable values for ²³⁴ all reactions as they were fitted using a constrained optimization method to obtain physically feasible solutions. The 235 magnitudes of the fitted A and E_a values are found to be similar between our functional form and the Arrhenius equation. As mentioned earlier, our method assumes that the A and E_a terms are relevant to the gas phase contributions ²³⁷ while $\Delta \Delta G_{\text{solv}}^{\ddagger}$ (298 K) and $\Delta \Delta H_{\text{solv}}^{\ddagger}$ (298 K) account for the solvation effects. However, the optimized parameters

Table 2

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Table 3

	Our functional form			Arrhenius eq		
Rxn	\boldsymbol{A}	E_a	$\Delta\Delta G_{\sf solv}^{\ddagger}$	$\Delta \Delta H^{\ddagger}$ solv	A	E_a
			(298 K)	(298 K)		
$\mathbf{1}$	$5.35e + 10$	2.51	-1.49	-0.62	$3.12e + 10$	0.64
2	$3.62e + 11$	2.60	-1.14	-0.37	$2.48e + 11$	1.19
3	$9.89e + 13$	3.30	1.59	-3.78	$1.74e + 13$	4.36
4	$6.78e + 09$	1.05	-0.66	-0.20	$1.01e + 10$	0.60
5	$4.16e + 10$	6.06	-1.89	0.71	$6.31e+10$	4.34
6	$1.39e + 13$	9.94	-2.17	0.49	6.11e+13	8.64
7	$1.16e + 13$	5.16	-0.90	0.15	$9.50e + 12$	4.11
8	$2.04e + 11$	5.51	-3.63	3.28	$9.34e + 12$	4.08
9	$6.46e + 10$	3.05	-1.89	1.48	1.31e+12	2.95
10	$4.33e+12$	9.18	-4.35	-1.21	$3.65e + 12$	4.73
11	$2.03e + 08$	4.03	1.54	-2.08	$2.72e + 07$	4.39
12	$5.77e+09$	4.26	1.80	-4.83	$1.12e + 09$	5.84
13	$8.24e + 11$	2.07	1.25	-1.45	$1.90e + 11$	2.59
14	$3.96e + 10$	4.12	-2.51	-1.62	$1.36e + 11$	2.60

Fitted kinetic parameters. E_a , $\Delta\Delta G_{\sf solv}^\ddag$ (298 K), and $\Delta\Delta H_{\sf solv}^\ddag$ (298 K) are in kcal/mol. A is in M $^{-1}$ s $^{-1}$ for a bimolecular reaction and in s−1 for a unimolecular reaction.

 are not guaranteed to correspond to the true values as they can have multiple solutions. Different initial guesses and constraints can yield different solutions, and it is difficult to determine which solution is closer to the true values. Our method also assumes that the gas phase rate constant follows the Arrhenius form, but some of the reactions are pressure-dependent in a gas phase and have non-Arrhenius behavior. Therefore, the fitted parameters should be treated as empirical parameters rather than the true kinetic parameters for the gas phase rate constants and solvation effects.

 $_{243}$ We additionally examined the contributions from the fitted gas phase parameters (A, E_a) and solvation parameters ²⁴⁴ (ΔΔ $G_{\text{solv}}^{\ddagger}$ (298 K), ΔΔ $H_{\text{solv}}^{\ddagger}$ (298 K)) separately for our method. The results are provided for six representative reactions in Figure [4.](#page-10-0) The liquid phase rate constants estimated using all four parameters are presented in blue solid lines ²⁴⁶ ($k_{\text{liq, fitted}}$), and the "gas phase" rate constants estimated using only A and E_a are presented in dotted red lines ($k_{\text{gas, fitted}}$). $_{247}$ The gas phase kinetic parameters of Reactions 1, 2, and 5 could be found in literature, and therefore the gas phase rate constants are also computed using the literature values for these reactions and provided in the figure as black dash-²⁴⁹ dotted lines ($k_{\text{gas, literature}}$) for comparison. The literature values are obtained using RMG Database [\[61\]](#page-14-10), which found multiple data for each reaction. The maximum and minimum rate constants estimated using different literature values are marked by the shaded area in the figure. Reactions 1 and 2 are identified as pressure-dependent, and their gas phase rate constants are computed at the saturation pressure of the solvent (sat. P) for all temperatures.

 Figure [4](#page-10-0) shows that the gas phase rate constants estimated using the fitted parameters deviate from the literature values for Reactions 1 and 2. This was expected as our method does not guarantee that the fitted parameters match the true values. Moreover, Reaction 1 has a non-linear temperature dependence in a gas phase that cannot be captured by the Arrhenius equation. On the contrary, the fitted gas phase rate constants show close agreement with the literature values for Reaction 5. Both Reactions 1 and 2 are pressure-dependent and assumed to be barrierless in a gas phase while Reaction 5 is independent of pressure and has a barrier height with a clearly defined transition state. It is hence possible that our approach can provide more accurate gas phase kinetic parameters for the reactions that have transition states and do not have pressure dependence. However, it is difficult to draw a solid conclusion as the comparison was ²⁶¹ made for only three reactions. More experimental data are needed for future studies to investigate whether the fitted parameters could yield reasonable estimates of gas phase rate constants. From Figure [4,](#page-10-0) it can be seen that the $k_{\text{gas, fitted}}$ v_{263} values approach the $k_{\text{liq, fitted}}$ limits as temperature approaches the critical point. This is because our functional form ²⁶⁴ forces the $\Delta \Delta G_{\text{solv}}^{\ddagger}(T)$ and k_{liq} to reach the limit of zero and k_{gas} , respectively, at the critical temperature. In fact, we can see that the literature gas phase rate constants of Reactions 1, 2, and 5 approach the same limit at around the critical point. The results seem to imply that our functional form approaches a correct limit. However, as mentioned

Figure 4: Comparison of the liquid phase rate constants estimated using all four parameters ($k_{liq, fitted}$, blue solid lines) and the gas phase rate constants estimated using only A and $E_{\scriptscriptstyle a}$ ($k_{\scriptscriptstyle\rm gas,\; fitted}$, red dotted line).

²⁶⁷ previously, the analysis was made only using three reactions, and more experimental data are required to further verify ²⁶⁸ whether our approach can provide correct limits at the critical point.

²⁶⁹ **4.2. Predicting the solvation parameters**

 270 New k_{liq} predictions are made based on the solvation parameters computed using the ab initio methods described in 271 Section [2.3.](#page-5-0) In this approach, the solvation energies and enthalpies of reactants and TS are calculated at 298 K and ²⁷² combined together to get the $\Delta \Delta G_{\text{solv}}^{\ddagger}$ (298 K) and $\Delta \Delta H_{\text{solv}}^{\ddagger}$ (298 K) of a reaction. Then we applied our method to ²⁷³ extrapolate $\Delta \Delta G_{\text{solv}}^{\ddagger}(T)$ from $\Delta \Delta G_{\text{solv}}^{\ddagger}(298 \text{ K})$ and $\Delta \Delta H_{\text{solv}}^{\ddagger}(298 \text{ K})$ and combined it with the literature k_{gas} data to k_{liq} predictions. The solvation parameters, however, could be only calculated for the reaction that has a TS and ²⁷⁵ has literature gas phase kinetic parameters. Only Reaction 5 matched this criteria, and thus the new predictions were ²⁷⁶ made for only one reaction.

 The results of the predicted k_{liq} are presented in Figure [5a](#page-11-0) along with the computed solvation parameters. We made additional predictions in Figure [5b](#page-11-0) by using the experimental solvation free energy and enthalpy data of the reactants 279 that are obtained from various sources $[62, 63, 64, 65, 66, 67]$ $[62, 63, 64, 65, 66, 67]$ $[62, 63, 64, 65, 66, 67]$ $[62, 63, 64, 65, 66, 67]$ $[62, 63, 64, 65, 66, 67]$ $[62, 63, 64, 65, 66, 67]$ $[62, 63, 64, 65, 66, 67]$ $[62, 63, 64, 65, 66, 67]$ $[62, 63, 64, 65, 66, 67]$ $[62, 63, 64, 65, 66, 67]$ $[62, 63, 64, 65, 66, 67]$. Note that both figures use the same solvation energy and enthalpy values for the TS that are computed from the ab initio approach, and they only differ in the solvation values used for the reactants. The results show that Figure [5b](#page-11-0) provides more accurate predictions of k_{liq} . Figure [5a](#page-11-0) has a higher error at elevated temperatures, yet it also provides acceptable predictions overall. Both plots have similar $\Delta \Delta G_{\text{solv}}^{\ddagger}$ (298 K) values, but their $\Delta \Delta H_{\text{solv}}^{\ddagger}$ (298 K) values differ by around 2 kcal/mol. Our prior study [\[68\]](#page-14-17) indicated that the COSMO-RS method, which is used to compute the solvation parameters, has a higher calculation error for solvation enthalpy compared to solvation free energy. Therefore, it is likely that the COSMO-RS method has relatively higher errors for the solvation enthalpies of the reactants, causing Figure [5a](#page-11-0) to underperform. Due to the paucity of ²⁸⁷ the experimental data, the exact calculation errors of $\Delta\Delta G_{\rm solv}^{\ddagger}(298 \text{ K})$ and $\Delta\Delta H_{\rm solv}^{\ddagger}(298 \text{ K})$ and of $k_{\rm liq}$ cannot be determined for this approach.

Figure 5: Result of the k_{liq} predictions from the calculated solvation kinetic parameters. (a) The ΔG_{sol} (298 K) and $\Delta H_{\rm solv}(298$ K) of both TS and reactants are calculated using ab initio methods. (b) Only the $\Delta G_{\rm solv}(298$ K) and $\Delta H_{\text{solv}}(298 \text{ K})$ of the TS is calulcated using ab intio method, and those of the reactants are obtained from literature.

 Overall, it is found that our method can achieve reliable predictions of temperature-dependent liquid phase rate constants for Reaction 5 based on the computed or experimental solvation parameters. This suggests that our proposed expression can serve not only as an empirical functional form but also as a predictive method. Nonetheless, the analysis was limited to only one reaction, and more thorough assessments should be made with more experimental data to determine whether our method can also provide accurate predictions for different reactions.

²⁹⁴ **5. Conclusions**

 We have developed a new functional form that can describe the temperature dependence of liquid phase rate constants for various reactions. The proposed method employs four kinetic parameters, two associated with the gas phase contributions and other two associated with the solvation corrections. These parameters can be fitted to experimental liquid phase rate constants to accurately reproduce the experimental data from room temperature up to the critical temperature of a solvent. The method was evaluated using 14 reactions, and the results reveal that our method showed superior performance at elevated temperatures compared to the Arrhenius equation. The four kinetic parameters have ³⁰¹ physical meanings and can be also calculated using ab initio methods instead of empirically fitting to the data. A 302 preliminary result implies that the solvation parameters can be computed using the quantum chemistry and COSMO-303 RS methods to make the k_{liq} predictions. Moving forward, future studies should look to collect more experimental data to further evaluate our proposed method and to test whether the kinetic parameters can be accurately calculated using ab initio approaches.

³⁰⁶ **CRediT authorship contribution statement**

³⁰⁷ **Yunsie Chung:** Conceptualization, Methodology, Data Curation, Validation, Visualization, Writing - Original Draft. ³⁰⁸ **William H. Green:** Supervision, Funding acquisition, Resources, Writing - Review & Editing.

³⁰⁹ **Declaration of competing interest**

³¹⁰ The authors declare that they have no known competing financial interests or personal relationships that could have 311 appeared to influence the work reported in this paper.

³¹² **Data availability**

³¹³ The experimental data collected from literature for method validation are provided as Supplementary data.

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