

# Encapsulation of functional solvents for improved thermal stability in CO<sub>2</sub> capture applications

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## Abstract

Herein we address the efficiency of CO<sub>2</sub> sorption of ionic liquids (IL) with hydrogen bond donors (e.g., glycols) added as viscosity modifiers and the impact of encapsulating them to limit sorbent evaporation. Ethylene glycol, propylene glycol, 1,3-propanediol, and diethylene glycol were added to three different ILs: 1-ethyl-3-methylimidazolium 2-cyanopyrrolide ([EMIM][2-CNpyr]), 1-ethyl-3-methylimidazolium tetrafluoroborate ([EMIM][BF<sub>4</sub>]), and 1-butyl-3-methylimidazolium tetrafluoroborate ([BMIM][BF<sub>4</sub>]). Incorporation of the glycols decreased viscosity on average 51% compared to bulk IL. After encapsulation of the liquid mixtures using a soft template approach, thermogravimetric analysis revealed reductions in volatility of 36 and 40 % on average compared to the unencapsulated liquid mixtures, based on isotherms at 25 and 55 °C, respectively. The encapsulated mixtures of [EMIM][2-CNpyr]:1,3-propanediol and [EMIM][2-CNpyr]:diethylene glycol exhibited the lowest volatility (0.0019 and 0.0002 mmol/h at 25 °C, respectively) and were further evaluated as CO<sub>2</sub> absorption/desorption materials. Based on capacity determined from breakthrough measurements, [EMIM][2-CNpyr]:1,3-propanediol had lower transport limited absorption rate for CO<sub>2</sub> sorption compared to [EMIM][2-CNpyr]:diethylene glycol with 0.08 and 0.03 mol CO<sub>2</sub>/kg sorbent, respectively; however, [EMIM][2-CNpyr]:diethylene glycol capsules exhibited higher absorptions capacity at ~500 ppm CO<sub>2</sub> (0.66 compared to 0.47 mol CO<sub>2</sub>/kg sorbent for [EMIM][2-CNpyr]:1,3-propanediol). These results show that multiple glycols can be used to reduce IL viscosity while increasing physisorption sites for CO<sub>2</sub> sorption and encapsulation can be utilized to mitigate evaporation of volatile viscosity modifiers.

## Introduction

As atmospheric CO<sub>2</sub> concentrations continue to rise, alternative approaches for negative emissions technologies (NET), such as carbon capture, must be implemented in complement to decarbonization efforts to avoid the average global surface temperature from rising greater than 2 °C by the mid-21<sup>st</sup> century.<sup>1</sup> One NET approach is direct air capture (DAC), which utilizes chemical reactions and/or physical interactions to sequester CO<sub>2</sub> from the atmosphere. DAC is more energy intensive compared to point source CO<sub>2</sub> capture due to the lower concentration of CO<sub>2</sub> in the atmosphere (~420 ppm versus > 1,000 ppm).<sup>2</sup> To date, DAC approaches have focused on liquid solvents<sup>3</sup> (e.g., aqueous amines), solid sorbents<sup>4</sup> (e.g., metal organic frameworks, MOFs), and pressure driven approaches<sup>5</sup> (e.g., membranes). Current technologies in industrial DAC applications are hindered by low CO<sub>2</sub> sorption rates and capacity, high energy demands for sorbent regeneration, and poor scalability.<sup>6</sup>

Solvent-based chemical DAC technologies typically require strong bases due to the low concentration of CO<sub>2</sub> in the atmosphere. For example, aqueous solutions of NaOH and KOH are common in DAC applications, in addition to amines and amine-functionalized molecules (e.g., amino acids).<sup>3,6</sup> Strong bases typically chemisorb CO<sub>2</sub>, for example with a hydroxide anion reacting to form bicarbonate and carbonate anions. Although this can be favorable for the capture of CO<sub>2</sub>, desorption is highly endothermic; for example, temperatures of ~ 900 °C are required for CaCO<sub>3</sub>. Aqueous amines are the main solvent for point-source carbon capture (i.e., flue gas), but are not suitable for DAC because the volatile amines evaporate into the environment when large volumes of airflow are passed over the sorbent. Alternatives to aqueous bases and amines, such as amino acids and ionic liquids (ILs), have decreased regeneration temperatures, typically 70-120 °C.<sup>3,7</sup> Further, ILs have negligible volatility, chemical and thermal stability, and tunability making them attractive candidates for DAC.<sup>7</sup> Conventional ILs, such as 1-butyl-3-methylimidazolium hexafluorophosphate [BMIM][PF<sub>6</sub>], primarily rely on physisorption of CO<sub>2</sub> into free molar volume.<sup>8,9</sup> By tailoring the functional moieties, task specific ILs (TSILs) can absorb CO<sub>2</sub> via chemisorption, as well as physisorption,<sup>10</sup> offering a promising alternative to other DAC solvents. For example, the Brenneke group developed the TSIL 1-ethyl-3-methylimidazolium 2-cyanopyrrolide ([EMIM][2-CNpyr]),<sup>11</sup> which the Gurkan group demonstrated its DAC abilities.<sup>12,13</sup> The Gurkan group determined two reaction routes are possible for [EMIM][2-CNpyr] DAC: the anion reversibly reacts with CO<sub>2</sub> to form carbamate, or the cation reacts to form imidazolium-carboxylate.<sup>14</sup> Notably, many TSILs are not economically viable for broad implementation in DAC operations compared to current solvents (e.g., aqueous amines, KOH, etc.) due to higher synthesis costs.<sup>15,16</sup>

Applications of ILs and TSILs are limited by high viscosity, primarily during the absorption of CO<sub>2</sub>,<sup>17</sup> which can slow CO<sub>2</sub> absorption rate,<sup>15</sup> thereby making the processing of large volumes of air for CO<sub>2</sub> removal a challenge. TSILs for DAC is further limited as solvent pumping costs increase as viscosity increases. One approach to improve CO<sub>2</sub> absorption rates is mixing TSILs with additives to reduce viscosity.<sup>18,19</sup> These solvent systems can also reduce the quantity of IL required and supply additional CO<sub>2</sub> binding motifs to enhance sorption rate and capacity. For instance, Camper et al. showed that mixing imidazolium-based ILs (e.g., [HMIM][Tf<sub>2</sub>N]) with amines (e.g., monoethanolamine) improved CO<sub>2</sub> absorption by at least 20 times compared to neat IL due to an increase in chemisorption capacity.<sup>20</sup> Meanwhile, Nookuea et al. demonstrated that adding a hydrogen bond donor (e.g., monoethanolamine) can reduce the overall viscosity of the mixture.<sup>21</sup> The molecular interactions between ILs and other additives have been studied, suggesting that van der Waals interactions (e.g., hydrogen bonding) reduce the evaporation of the

additive as well as improve CO<sub>2</sub> sorption.<sup>19,22</sup> For example, Lee et al. demonstrated that a mixture of [EMIM][2-CNpyr] and ethylene glycol had improved absorption rate of CO<sub>2</sub> which was attributed to reduced viscosity compared to the bulk IL.<sup>19</sup> The authors also determined that EG aided in CO<sub>2</sub> sorption by protonating the anion and forming a complex with CO<sub>2</sub>. Importantly, the higher loading of EG (i.e., IL:EG at 1:3) resulted in noticeable evaporative loss, while lower compositions resulted in thermal stability attributed to Coulombic interactions.

Implementation of ILs for DAC is not limited to traditional solvent-based approaches (i.e., bulk liquids), and in complement can be used in various composite structures such as membranes (e.g., polymer-IL, supported IL membranes, and cross-linked gels),<sup>23–25</sup> IL-impregnation in porous structures (e.g., silica),<sup>26–29</sup> and microencapsulation.<sup>14,30–35</sup> Of these composite structures, encapsulation is perhaps the most scalable and most flexible to different compositions. Three main approaches can be used to encapsulate ILs: microfluidics,<sup>36</sup> hard template approach,<sup>37</sup> or soft template approach, of which the soft template approach is the most common. Here, a shell is grown around a droplet of the desired core, typically relying on an emulsion with liquid droplets stabilized by surfactants. The encapsulation of different types of ILs have been studied for post-combustion capture of CO<sub>2</sub> and for DAC. For example, Bernard et al. encapsulated imidazolium based fluorinated ILs from an emulsion, which leads to less uniformity in size distribution.<sup>38</sup> The Pentzer Group has meticulously worked at encapsulating a variety of ILs utilizing the soft template approach stabilized with modified graphene oxide<sup>39–41</sup> with a wide range of applications such as toxin removal,<sup>42–44</sup> CO<sub>2</sub> capture,<sup>14,45,46</sup> protecting phase change materials,<sup>47</sup> and utilizing dynamic chemistry for payload release.<sup>48–50</sup> The Gurkan group has done significant work with developing different deep eutectic solvents, such a choline-based eutectic solvents for CO<sub>2</sub> sorption,<sup>51</sup> and researching the kinetics and intermolecular interactions of the TSILs for CO<sub>2</sub> sorption.<sup>13,52</sup> In collaboration between the two groups, the versatility of the encapsulation techniques enable the applicability of more volatile additives for CO<sub>2</sub> sorbents by having the shell act as a barrier to the solvent while being CO<sub>2</sub> permeable. Currently, there are very limited studies on the role different glycols have for CO<sub>2</sub> sorption and modifying IL viscosity,<sup>53–55</sup> while limited studies have been done on quantifying how well encapsulation can reduce evaporation of volatile compounds (e.g., glycols).<sup>56</sup>

Herein, we demonstrate that glycol-based hydrogen bond donor (HBD) additives can be used to decrease the viscosity of ILs by ~51 % and that the volatility of the glycols can be reduced by 36 and 40% at temperature of 25 and 55 °C, respectively, compared to pure glycols. Further reductions in volatility can be achieved by encapsulating these liquid mixtures with a reduction of 40 and 43% at 25 and 55 °C, respectively, compared to pure glycols. We further demonstrate that encapsulation enhances CO<sub>2</sub> sorption rates of the IL:glycol mixtures, with [EMIM][2-CNpyr]:DEG having the fastest uptake rate compared to [EMIM][2-CNpyr]:1,3-P. The use of DEG and 1,3-P as viscosity modifiers increased the CO<sub>2</sub> capacity by a factor of 3 and 4, respectively. Ethylene glycol (EG), propylene glycol (PG), 1,3-propanediol (1,3-P), and diethylene glycol (DEG) are used as the HBDs and both ILs ([EMIM][BF<sub>4</sub>], and [BMIM][BF<sub>4</sub>]) and TSIL ([EMIM][2-CNpyr]). This study demonstrates that encapsulating the mixtures using a soft-template microencapsulation approach, the core volatility loss was further minimized with the least volatile samples ([EMIM][2-CNpyr]:1,3-P and [EMIM][2-CNpyr]:DEG) studied for CO<sub>2</sub> sorption applications. With the use of viscosity modifiers and encapsulation, more expensive viscous reactive chemicals (e.g., TSILs) can be more widely utilized in a variety of industries such as wastewater treatment, pharmaceuticals, and consumer goods.

## Methods

**Materials:** The IL 1-ethyl-3-methylimidazolium 2-cyanopyrrolide ([EMIM][2-CNpyr]) with a purity of >95 % was synthesized as previously reported.<sup>14</sup> 1-Ethyl-3-methylimidazolium tetrafluoroborate ([EMIM][BF<sub>4</sub>]) (>98 %) and 1-butyl-3-methylimidazolium tetrafluoroborate ([BMIM][BF<sub>4</sub>]) (>98 %) were purchased from Iolitec and were dried at 80 °C under reduced pressure for 72 h; [EMIM][2-CNpyr] was dried under reduced pressure at 70 °C for 72 h to avoid thermal decomposition. All other materials were used as received. Graphite flakes, propylamine, potassium permanganate, 4,4'-diaminodiphenylmethane (DAPM), hexamethylene diisocyanate (HDI), diethylene glycol (DEG), 1,3-propanediol (1,3-P), and sulfuric acid (95-98%) were purchased from Sigma-Aldrich. Hexanes, hydrogen peroxide (35 wt% in water), and toluene were purchased from Fisher Scientific. Additionally, n-octane (Oakwood Chemical), ethylene glycol (EG, from Acros Organics), propylene glycol (PG, from TCI), and *N,N*-dimethylformamide (DMF, from Alfa Aesar) were all purchased and used as received. Nitrogen gas (Ultra High Purity) and carbon dioxide gas (Bone Dry) were purchased from Airgas.

**Instrumentation:** Mixture composition and capsule core loading were characterized by nuclear magnetic resonance (NMR) spectroscopy in DMSO-d<sub>6</sub> using a Bruker Avance NEO 400 MHz NMR spectrometer. Centrifugation was conducted using a ThermoScientific Sorvall ST 8 centrifuge. Bath ultrasonication was done with a Fisherbrand CPX3800 5.7 L Ultrasonic Bath. Emulsification was done using a BioSpec hand-held homogenizer model 985370. The capsule morphology was analyzed using scanning electron microscopy (Tescan Vega SEM) at a voltage of 10-20 kV; prior to characterization, the sample was sputter-coated with 10 nm of Au (Cressington 108 Sputter Coater). Fourier transform infrared (FTIR) spectroscopy was performed on a JASCO FT/IR-4600 using a diamond coated ZnSe crystal in ATR mode. Thermogravimetric analysis (TGA) was performed on a TA instruments TGA 5500 equipped with a TA Instruments Blending Gas Delivery Module under N<sub>2</sub> and bone-dry CO<sub>2</sub>. Viscosity measurements were performed using an Anton Paar MCR-302 rotational rheometer with an Anton Paar 25 mm 0.5 degree cone CP25-0.5 top plate and an Anton Paar 24.986 mm parallel plate. The density of the mixtures was collected using an Anton Paar vibrating U-tube density meter (DMA 4500M) with an accuracy of 0.00005 g/cm<sup>3</sup>.

**IL:glycol Mixture Preparation and Characterization:** Mixtures of IL and glycols were prepared with molar ratios of 1:2, and confirmed by <sup>1</sup>H NMR spectroscopy using DMSO-d<sub>6</sub> as the solvent.

**Synthesis of Graphene Oxide (GO):** GO nanosheets were synthesized using a modified Hummer's method, as previously reported.<sup>57</sup> Briefly, graphite flakes (3 g) were dispersed in concentrated H<sub>2</sub>SO<sub>4</sub> (400 mL) at room temperature. KMnO<sub>4</sub> (3 g) was slowly added, and after complete addition the mixture was stirred at room temperature for 24 h; this was repeated 3 times for a total addition of 12 g of KMnO<sub>4</sub>. Then, after stirring a total of 72 h, the reaction was quenched by adding the solution into three Erlenmeyer flasks each containing ~750 mL of ice water. Dropwise addition of H<sub>2</sub>O<sub>2</sub> to the stirred solution was continued until the color turned from pink to brown, indicating excess KMnO<sub>4</sub> was consumed. The yellow-brown GO was isolated by centrifugation and subsequent washing of the pellet with isopropanol, each time discarding the supernatant and repeating until the supernatant was neutral by a Litmus test. The GO was then dried overnight under reduced pressure at room temperature, thereafter, blended to a fine powder. The powder was stored in a refrigerator, sealed with parafilm.

**Synthesis of Alkylated GO (C<sub>18</sub>-GO):** C<sub>18</sub>-GO was synthesized following a method previously reported.<sup>39</sup> GO (100 mg) was dispersed in DMF (40 mL) via sonication until no visible aggregates were observed. Meanwhile, octadecylamine (900 mg) was dissolved in DMF (60 mL) by gently heating to 60 °C in a 250 mL round bottom flask (rbf). The GO solution was added to the rbf and the resulting mixture stirred at 55 °C for ~5 minutes. The sample was then centrifuged, and supernatant discarded. The pellet was suspended in toluene (40 mL) via sonication. In a separate rbf, octadecylamine (2.7 g) was dissolved in toluene (60 mL) while stirring at 60 °C. Once the octadecylamine was dissolved, the GO dispersion was added, and the mixture stirred at 55 °C overnight. Thereafter, a dark brown precipitate was isolated via centrifugation, washed with octane (2 x 25 mL, discarding the supernatant each time) and dried under reduced pressure at ambient temperature. When ready to use, ~100 mg of C<sub>18</sub>-GO was dispersed in 1:1 v/v mixture of octane (25 mL) and heavy mineral oil (25 mL), resulting in a C<sub>18</sub>-GO concentration of 2 mg/mL.

**Synthesis and Characterization of Microcapsules:** Based a previously reported method,<sup>40</sup> capsules were synthesized by interfacial polymerization in an emulsion (i.e., a soft template approach). As an example, take the preparation of capsules with a core of pure EG. First, DAPM (0.66 mmol, 130.8 mg) was dissolved in 0.5 mL EG in a 20 mL scintillation vial via sonication. Then, C<sub>18</sub>-GO in octane/mineral oil (2.5 mL of a 2 mg/mL solution) was added to the EG/DAPM solution and emulsified by 3 cycles of shear mixing (20 s on, 15 s off), which produced an emulsion with droplets of EG/DAPM in a continuous phase of octane and mineral oil. The prepared emulsion was diluted with octane (1 mL). In a separate vial, HDI (0.86 mmol, 137.8 μL) was mixed with octane (1.25 mL) and this solution was added dropwise to the emulsion with swirling the vial by hand. The system was left unagitated at ambient temperature for 72 h, then the capsules were isolated via gravity filtration and washed with hexanes (~100 mL) then dispersed in hexanes (100 mL). Residual isocyanate groups were quenched by adding propylamine (2 mL) to the dispersion and allowing the system to rest for 1-2 h. Finally, the capsules were isolated via gravity filtration and washed with hexanes until pH of effluent is about neutral to verify propylamine removal (~300 mL hexanes). The capsules were air dried for an hour. A similar procedure was used for all capsules, with the discontinuous phase being ILs, glycols, or IL/glycol mixtures. The amount of monomer was consistent across all the samples, excluding the [EMIM][2-CNpyr] capsules for which a second additional HDI was used (0.43 mmol), with a total loading of 1.29 mmol HDI.

The loading of the core liquid in the capsules was determined by extraction of the core using DMSO-d<sub>6</sub> and mesitylene standard, and characterization by <sup>1</sup>H NMR, as previously reported.<sup>39</sup> Capsules (~20 mg) were weighed in a glass vial and then a 0.038 M mesitylene in DMSO-d<sub>6</sub> solution (1 mL) was added. The sample was sonicated for ~3 min to extract the core liquid and then passed through a PTFE syringe filter to separate the solid capsule shell. Relative integration of the <sup>1</sup>H NMR signals due to mesitylene and the IL, glycol, or IL and glycol was used to determine the wt% of the core in the capsule (Figure S1). Capsule sizing was done using ImageJ and SEM images with 100-500 capsules per sample.

### **Evaporation Rate Measurements:**

Evaporation rate studies were determined using thermogravimetric analysis (TGA) under an inert N<sub>2</sub> environment. As an example, bulk EG (20 μL) was spread on a tared, flame-cleaned high temperature platinum TGA pan. A 1 h isotherm under N<sub>2</sub> (flow rate of 25 mL/min) was conducted at 25 °C, monitoring the mass. The sample pan was cleaned and a fresh sample of EG (20 μL) was

added and a 1 h isotherm under N<sub>2</sub> (flow rate of 25 mL/min) at 55 °C was collected. A similar procedure was used on all unencapsulated pure glycols, pure ILs, and IL/glycol mixtures. Samples containing 1,3-P and DEG were pretreatment at 55 °C under N<sub>2</sub> (flow rate of 25 mL/min) for 5 min to desorb any volatiles resulting in a stable mass loss at 25 °C.

The evaporation rates of the encapsulated liquids were determined using the method described above. To compare capsules to bulk samples, the molar quantities of the liquids were held constant by using the core wt% loading of the capsules. For example, 20 μL of bulk EG has 0.358 mmol of EG and the capsules of EG had a measured core loading of 60 ± 3 wt% EG. Therefore, the amount of EG capsules used was 37 mg, using:

$$X \text{ mg of capsules} = \frac{(\text{mmol of bulk liquid})(\text{molar mass of liquid})}{\text{core loading wt\%}} \quad (1)$$

The thermal stability of the encapsulated and unencapsulated samples were determined using TGA with heating ramped from ambient temperature to 500 °C by 10 °C/min under N<sub>2</sub> (25 mL/min) (Figure S2).

**CO<sub>2</sub> Sorption Studies.** The IL:glycol mixtures with the lowest evaporation rates (i.e., [EMIM][2-CNpyr]:1,3-P and [EMIM][2-CNpyr]:DEG) were evaluated for CO<sub>2</sub> sorption utilizing both thermogravimetric and breakthrough techniques.

Thermogravimetric CO<sub>2</sub> sorption studies were conducted using TGA with flowrates of both CO<sub>2</sub> and N<sub>2</sub> at 25 mL/min. On a clean platinum TGA pan, ~10 mg of capsules was loaded. The capsules were pretreated to remove any absorbed gases and moisture at 55 °C under N<sub>2</sub> (25 mL/min) until the mass of the sample exhibited a similar linear mass loss determined from the evaporation studies, as previously determined. Then, the sample was cooled from 55 °C to 25 °C at a rate of 10 °C/min and a baseline mass was established. Then, N<sub>2</sub> was switched to CO<sub>2</sub> (25 mL/min). The mass of the sample increased steadily until a plateau was reached; then, for desorption, CO<sub>2</sub> was replaced with N<sub>2</sub> (25 mL/min) and the temperature was increased to 55 °C (10 °C/min). Decrease in mass was observed and then stabilized at approximately the baseline established with the pretreatment. This CO<sub>2</sub> sorption-desorption cycle was completed 10 times for both capsule samples.

Breakthrough experiments were performed following a previously described procedure.<sup>14</sup> Briefly, capsules (0.25 ± 0.01 g) were lightly packed into a 0.305” inner diameter column, with care taken not to break the capsules. A mixture of 500 ± 5 ppm CO<sub>2</sub> in N<sub>2</sub> (Airgas custom mixture) was fed to the column at 20 standard cm<sup>3</sup>/min (sccm) utilizing a mass flow controller (Brooks i5850, 0-200 sccm) and the effluent gas was analyzed by an IR gas sensor. A bypass was used to calibrate the infrared gas analyzer (SBA-5, PP Systems, Inc.) and the gas feed composition was measured. After 1 minute, the feed gas was diverted to the sample column, and the effluent CO<sub>2</sub> concentration was measured over time. The experiment was stopped when the concentration of CO<sub>2</sub> in the effluent reached the feed concentration of 500 ± 5 ppm. Capacity analysis was performed by integrating the breakthrough curve and using the following equation:

$$z = \frac{\int_0^t (C_0 - C) dt * F}{W * \bar{V}_{STP}} \quad (2)$$

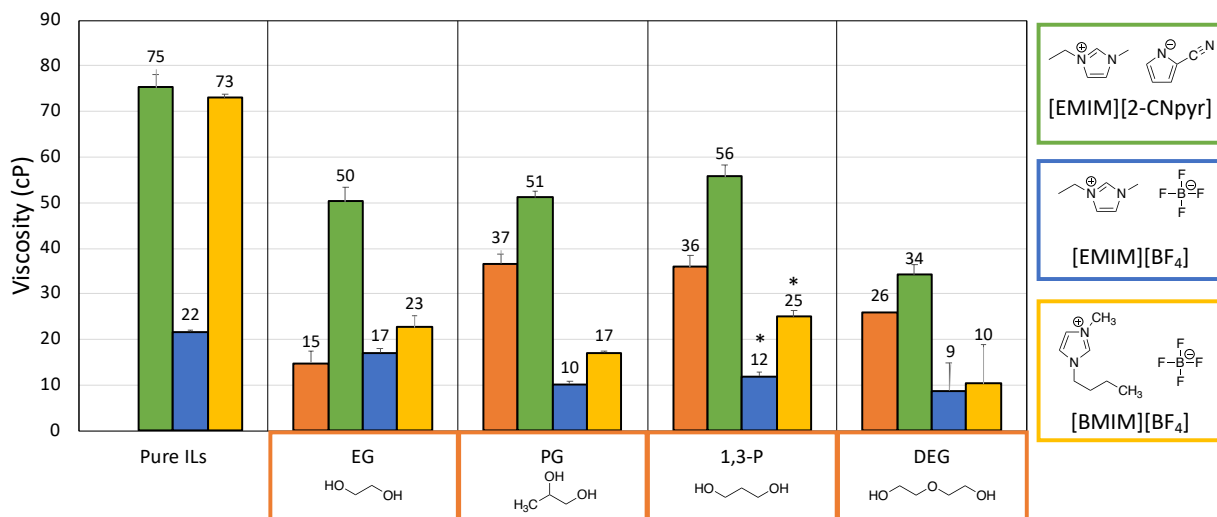
where  $z$  is the CO<sub>2</sub> loading (mmol CO<sub>2</sub> / g sorbent).  $C_0$  is the dimensionless feed CO<sub>2</sub> composition (concentration in ppm \* 10<sup>6</sup>),  $C$  is the dimensionless effluent CO<sub>2</sub> composition,  $t$  is time (min),  $F$

is the total mass flowrate of the feed gas (sccm),  $W$  is the weight of the sample (g), and  $\hat{V}_{STP}$  is the molar volume of CO<sub>2</sub> at STP (22.4 scc CO<sub>2</sub> / mmol CO<sub>2</sub>, assuming ideal gas law in dilute conditions). Breakthrough time ( $t_{BT}$ ) and pseudoequilibrium time ( $t_{PE}$ ) are defined as the time at which the effluent concentration reached 25 ppm CO<sub>2</sub> (5% of the feed concentration) and 490 ppm (97.5% of the feed concentration), respectively.

## Results and Discussion

**Materials Selection, Preparation, and Characterization.** Four different glycols were used as viscosity modifiers for three different ILs, each chosen for their commercial availability or ease of accessibility, giving twelve IL:glycol compositions, each prepared using a 1:2 molar ratio of IL to glycol, chosen based on prior studies.<sup>19,58</sup> Two generic ILs ([EMIM][BF<sub>4</sub>] and [BMIM][BF<sub>4</sub>]) and one TSIL ([EMIM][2-CNpyr]) were chosen. The generic [EMIM][BF<sub>4</sub>] and [BMIM][BF<sub>4</sub>] absorb CO<sub>2</sub> via physisorption into free volume and differ by the length of one alkyl chain on the imidazolium cation resulting in a difference in viscosities.<sup>25</sup> Recall, [EMIM][2-CNpyr] undergoes chemisorption by reaction of CO<sub>2</sub> via 4 possible routes, as stated earlier.<sup>14,19,59,60</sup> The four glycols were chosen as low-cost and non-corrosive viscosity modifiers with the ability to hydrogen bond through their hydroxyl groups: EG, PG, 1,3-P, and DEG. Thus, all mixtures were homogenous at room temperature, apart from [EMIM][BF<sub>4</sub>]:1,3-P and [BMIM][BF<sub>4</sub>]:1,3-P which phase separated at room temperature, but form a homogenous solution at 29 °C and 26 °C, respectively.

**Figure 1** shows the viscosity of the pure ILs, pure glycols, and their mixtures at 25 °C (with exception for [EMIM][BF<sub>4</sub>]:1,3-P and [BMIM][BF<sub>4</sub>]:1,3-P which were recorded at 40 °C). The viscosity of the pure ILs were:  $75.3 \pm 2.1$  for [EMIM][2-CNpyr],  $21.6 \pm 6.2$  for [EMIM][BF<sub>4</sub>], and  $73.0 \pm 8.5$  for [BMIM][BF<sub>4</sub>]. Despite having the same cation, [EMIM][2-CNpyr] and [EMIM][BF<sub>4</sub>] have significantly different viscosities. Interestingly, the viscosities of [EMIM][2-CNpyr] and [BMIM][BF<sub>4</sub>] were similar, yet [BMIM][BF<sub>4</sub>] had a more significant viscosity reduction with the addition of the glycol modifiers. All IL:glycol mixtures had decreased viscosity compared to the pure ILs, with [EMIM][BF<sub>4</sub>] and [BMIM][BF<sub>4</sub>] mixtures also having a lower viscosity than the pure glycols. In contrast, [EMIM][2-CNpyr] mixtures were more viscous compared to the corresponding pure glycols. The water content of the mixtures was measured to be between 1876 to 7629 ppm, with EG mixtures having the highest water content (7290 – 7629 ppm) with the other mixtures having a lower water content: PG (2114 – 2241 ppm), 1,3-P (2870 – 3860 ppm), and DEG (1876 – 2704 ppm). All water content data can be found in **Table S1**.



**Figure 1:** Viscosity of pure ILs and their mixtures for [EMIM][2-CNpyr] (green), [EMIM][BF<sub>4</sub>] (blue), [BMIM][BF<sub>4</sub>] (yellow), and pure glycols (orange). Data collected at 25 °C except samples marked with an “\*” which were taken at 40 °C.

To further examine the molecular interactions of the mixture, excess molar volume was calculated using eq 3:

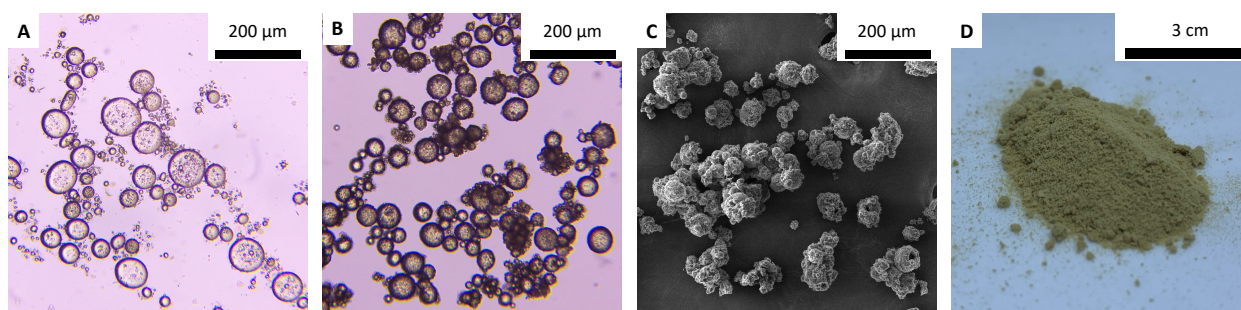
$$V_m^E = \frac{x_1 M_1 + x_2 M_2}{\rho_{mix}} - \frac{x_1 M_1}{\rho_1} - \frac{x_2 M_2}{\rho_2} \quad (3)$$

Where  $\rho$  is density,  $x$  is mole fraction, and  $M$  is molar mass. The excess molar volume had negative values for all [EMIM][2-CNpyr]-glycol mixtures, suggesting that hydrogen bond networks formed between the IL and the glycol, thereby resulting in a closer packing of the molecules and higher viscosity.<sup>61</sup> On the other hand, [EMIM][BF<sub>4</sub>]- and [BMIM][BF<sub>4</sub>]-glycol mixtures had positive excess molar volumes, indicating that the constituent species are not strongly interacting, resulting in lower viscosities. Although the analysis of the mixtures of [EMIM][BF<sub>4</sub>] and [BMIM][BF<sub>4</sub>] with 1,3-P used the densities at 40 °C, the excess molar volume is still very large and positive (3.9 and 2.1 mL/mol, respectively). These large positive values suggest poor molecular interactions, which is reasonable due to the mixture phase separating at 25 °C. The excess molar volume results have an indirect correlation with the mixture viscosities: as hydrogen bond networks form, molecules are more tightly packed resulting in higher viscosity.

Encapsulation of the pure ILs, pure glycols, and their mixtures was done using a soft-template approach. Briefly, the liquid for the core was shear mixed with an octane/mineral oil dispersion of C<sub>18</sub>-GO nanosheets (see experimental for details) to form a nanosheet-stabilized Pickering emulsion (**Figure 2A**). By pre-loading the droplet with 4,4'-diaminodiphenylmethane (DAPM) and adding hexamethylene diisocyanate (HDI) into the octane phase of the emulsion, A2+B2 step growth interfacial polymerization of the diamine and diisocyanate yielded a polyurea capsule shell around the droplet (**Figure 2B** and **2C**). The capsules were isolated by gravity filtration then residual isocyanate groups were quenched with propyl amine. The capsules were air dried for 1 h, yielding solid capsules in gram scale (**Figure 2D**); emulsion droplets were slightly smaller than the corresponding capsules, assumedly due to the polymer shell formation around the droplet (i.e., polymerization took place in the outer part of the droplet).



Images of all emulsions and capsules are shown in **Figure S3** and **Figure S4**, respectively, and illustrate spherical emulsion droplets and capsules tens of microns in diameter. The size distribution for each capsule system was evaluated utilizing SEM images and ImageJ analysis of 100-500 capsules per sample (**Table S1**). Overall, the average diameter sizes of the capsules with [EMIM][BF<sub>4</sub>] mixtures had the smallest average diameter ( $23 \pm 9 \mu\text{m}$ ), [BMIM][BF<sub>4</sub>] mixtures had an average of  $42 \pm 20 \mu\text{m}$ , and capsules of [EMIM][2-CNpyr] mixtures had the largest average diameter ( $52 \pm 15 \mu\text{m}$ ). The largest capsules were pure DEG and [EMIM][2-CNpyr]:DEG,  $70 \pm 29 \mu\text{m}$  and  $70 \pm 16 \mu\text{m}$ , respectively.



**Figure 2.** Images of the [EMIM][2-CNpyr]:1,3-P emulsion and capsules: A) Optical microscopy image of emulsion showing discrete IL:glycol droplets in a mineral oil/octane continuous phase, B) Optical microscopy image of capsules before isolation with visible polyurea shell formation, C) SEM image of isolated capsules, D) Photograph of isolated capsules post air-drying for 1 h.

The core loading wt% of the capsules was determined by extracting the core liquid using a deuterated solvent containing an internal standard and characterization of the liquid by <sup>1</sup>H NMR spectroscopy (a representative spectrum is shown in Figure S1). The spectra were analyzed by integrating signals from each constituent molecule present and comparing to the internal standard. The average core wt% across all samples was  $52 \pm 2 \text{ wt}\%$ . For example, capsules of [EMIM][BF<sub>4</sub>] and its mixtures had an average loading of  $62 \pm 1 \text{ wt}\%$  whereas capsules of [BMIM][BF<sub>4</sub>] and its mixtures had an average loading of  $60 \pm 1 \text{ wt}\%$ . However, capsules of [EMIM][2-CNpyr] and its mixtures had the lowest average loading of  $31 \pm 2 \text{ wt}\%$ , which may be due to the thicker shell (i.e., to prepare isolable capsules additional monomer was used). A negative correlation was observed between the core viscosity and loading. Capsules with higher viscosity cores resulted in a lower wt% of core material, for example, [EMIM][2-CNpyr] (viscosity of  $75.3 \pm 2.1 \text{ cP}$ ) had a core loading of  $25 \pm 1.8 \text{ wt}\%$ . Meanwhile, [EMIM][BF<sub>4</sub>]:EG (viscosity of  $10.3 \pm 0.7 \text{ cP}$ ) had a core loading of  $63 \pm 0.9 \text{ wt}\%$ .

**Volatility Measurements.** Volatility of the bulk and encapsulated liquids was examined by determining the evaporation rates using thermogravimetric analysis (TGA). First, isotherms under N<sub>2</sub>-feed were established for all systems at 25 °C and 55 °C, using a fresh sample for each. Notably, the pure ILs have no detectable evaporation rate at either temperature after initial minimal weight loss by desorption of, e.g., water vapor or gases, as previously documented (Figure S6).<sup>14,62</sup> The evaporation rates for the glycols and IL/glycol mixtures were established by taking the slope of the last 10 min of the 1 h isotherm, with the assumption that evaporation was due to loss of the glycol component. The evaporation rate expressed in mmol/h can be found in **Table 1** and graphically in **Figure 3**.

**Table 1:** Evaporation rates of bulk and encapsulated pure glycols and their mixtures at 25 and 55 °C, with the values at 55 °C in parenthesis.

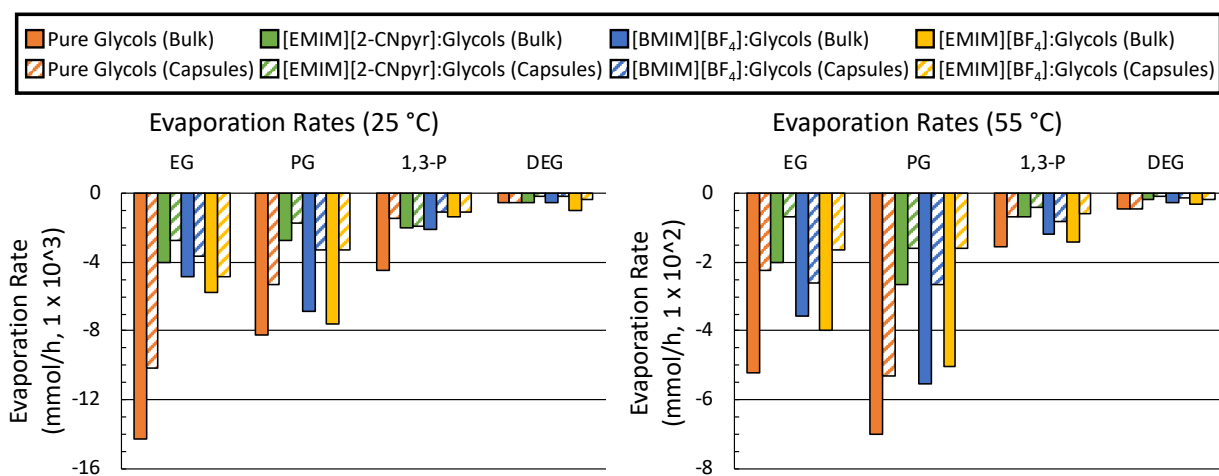
Evaporation Rates (mmol/h $1 \times 10^{-2}$ )								
25 °C (55 °C)	Pure Glycols		[EMIM] [2-CNpyr]		[BMIM][BF <sub>4</sub> ]		[EMIM][BF <sub>4</sub> ]	
	Bulk	Caps	Bulk	Caps	Bulk	Caps	Bulk	Caps
EG	1.43 (5.20)	1.01 (2.25)	0.40 (2.02)	0.28 (0.71)	0.48 (3.58)	0.37 (2.59)	0.58 (4.00)	0.49 (1.64)
PG	0.83 (6.99)	0.53 (5.28)	0.28 (2.38)	0.18 (1.61)	0.69 (5.53)	0.33 (2.64)	0.76 (5.01)	0.33 (1.61)
1,3-P	0.45 (1.57)	0.15 (0.68)	0.20 (0.69)	0.19 (0.41)	0.17 (1.21)	0.11 (0.84)	0.17 (1.40)	0.11 (0.60)
DEG	0.05 (0.46)	0.05 (0.46)	0.05 (0.19)	0.02 (0.08)	0.06 (0.29)	0.02 (0.12)	0.10 (0.34)	0.04 (0.14)

The evaporation rates of the bulk glycols and their mixtures with ILs at 25 °C had a trend dependent on the glycol, with the evaporation rate of EG > PG > 1,3-P > DEG, which correlates with previous reports of the bulk glycols.<sup>63–65</sup> Perhaps surprisingly, the evaporation rates of the IL/glycol mixtures were also dependent on the identity of the IL, with volatility trending as [EMIM][BF<sub>4</sub>] > [BMIM][BF<sub>4</sub>] > [EMIM][2-CNpyr]. In all cases, addition of the IL to the glycol decreased the volatility of the glycol, which can be attributed to favorable interactions between the components, e.g., ion-dipole and dipole-dipole interactions.<sup>66</sup> The evaporation rates of bulk [EMIM][BF<sub>4</sub>]- and [BMIM][BF<sub>4</sub>]-glycol mixtures were somewhat similar to each other (0.10 – 0.76 mmol/h and 0.06 – 0.69 mmol/h, respectively), whereas bulk [EMIM][2-CNpyr]-glycol mixtures had the highest viscosity hence presents more ionic interactions and therefore, these results are consistent with the above discussed results (0.05 – 0.40 mmol/h). Diffusion limitations of the glycol in the IL may contribute to lower evaporation rates in mixtures compared to the pure glycol, as diffusion of glycols to the surface is slowed by the hydrogen bonding network. Notably, both DEG and IL-DEG mixtures had similar evaporation rates at 25 °C (0.05 – 0.10 mmol/h). Now, examining the isotherm at 55 °C, the bulk material exhibited a similar trend that was seen at the 25 °C isotherm, however, PG has the overall highest evaporation rate: PG > EG > 1,3-P > DEG. In general, the mixture volatility was primarily dependent on the IL where [EMIM][BF<sub>4</sub>] (0.34 – 5.01 mmol/h) > [BMIM][BF<sub>4</sub>] (0.29 – 5.53 mmol/h) > [EMIM][2-CNpyr] (0.19 – 2.38 mmol/h), with the noticeable exception of [BMIM][BF<sub>4</sub>]:PG having a higher evaporation rate compared to the other IL:PG mixtures at 5.53 mmol/h.

The encapsulated glycols and their IL mixtures had a much lower evaporation rate compared to the bulk analog. At 25 °C the general evaporation rate trend was EG > PG > 1,3-P > DEG. Contrary to the bulk analog, the IL evaporation rate trend was different for the capsules. For the IL:EG mixtures, the evaporation rates were [EMIM][BF<sub>4</sub>] > [BMIM][BF<sub>4</sub>] > [EMIM][2-CNpyr]. However, IL:PG and IL:1,3-P had evaporation rates of [EMIM][BF<sub>4</sub>] = [BMIM][BF<sub>4</sub>] > [EMIM][2-CNpyr] and [EMIM][2-CNpyr] > [EMIM][BF<sub>4</sub>] = [BMIM][BF<sub>4</sub>], respectively. Lastly, IL:DEG had an evaporation rate trend of [EMIM][BF<sub>4</sub>] > [BMIM][BF<sub>4</sub>] = [EMIM][2-CNpyr]. To be clear, [EMIM][2-CNpyr]:glycol mixtures tend to have the lowest evaporation rates, however, [EMIM][2-CNpyr]:1,3-P had a higher evaporation rate compared to pure 1,3-P and the other IL:1,3-P mixtures. This is likely due to poor capsule formation which led to core leakage during

the handling of the capsules. Examining the 55 °C isotherm for the capsules, the pure encapsulated glycols had a general evaporation rate trend of PG > EG > 1,3-P > DEG. Interestingly, the encapsulated IL mixture evaporation rate trend was different at 55 °C compared to 25 °C where [BMIM][BF<sub>4</sub>] > [EMIM][BF<sub>4</sub>] > [EMIM][2-CNpyr]. The only exception was with IL:DEG with the trend being [EMIM][BF<sub>4</sub>] > [BMIM][BF<sub>4</sub>] > [EMIM][2-CNpyr].

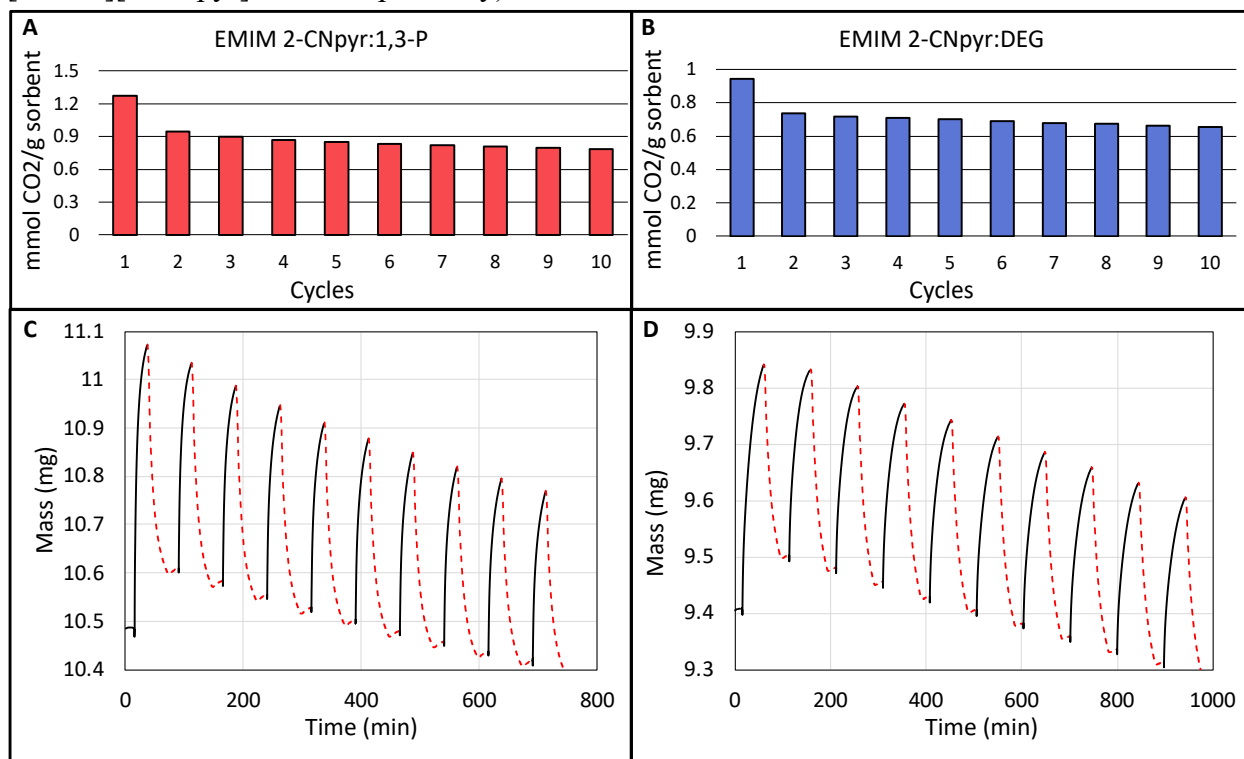
Comparing the overall bulk and encapsulated evaporation rates of the pure glycols to the IL:glycol mixtures, the mixtures exhibited a decrease in evaporation by an average of 36 and 40 % based on the isotherms at 25 and 55 °C, respectively. [EMIM][2-CNpyr]:glycol mixture evaporation rates decreased by 45 and 62 % compared to the pure glycol evaporation rates at 25 and 55 °C, respectively. The mixtures containing DEG had the largest evaporation decrease with encapsulation by 47 and 72 % at 25 and 55 °C, respectively. These results suggest that introducing a glycol as a viscosity modifier can reduce the viscosity of the IL while lowering the volatility of the glycol which can increase the working life of these encapsulated systems. Thus, capsules of [EMIM][2-CNpyr]:1,3-P and [EMIM][2-CNpyr]:DEG were selected for CO<sub>2</sub> sorption and thermal desorption studies because they had the lowest evaporation rates of all systems evaluated.



**Figure 3.** Evaporation rates of bulk liquids (solid) and encapsulated liquids (striped) at (A) 25 °C and (B) 55 °C all under a pure N<sub>2</sub> environment using TGA. The slope of the last 10 minutes of the isotherms was determined and converted to mmol/h. To enable comparison between a bulk and encapsulated sample, the molar quantity was held constant for each of the experiments.

**CO<sub>2</sub> Uptake Experiments.** CO<sub>2</sub> sorption for the encapsulated IL-glycols was performed at 25 °C with a pure CO<sub>2</sub>-gas stream and thermal desorption was performed at 55 °C under a N<sub>2</sub> gas stream, performing ten sorption-desorption cycles. The first cycle was used to condition the material and determine the sorption and desorption times. **Figure 4** shows the sorption/desorption cycles for [EMIM][2-CNpyr]:1,3-P and [EMIM][2-CNpyr]:DEG capsules. For both systems, a slight decrease in capacity is observed with each cycle (**Figure 4A, 4B**), this may be attributed to residual CO<sub>2</sub> that did not desorb completely out of the capsule core. Additionally, some evaporation of the core liquid likely occurred, which is supported by a decrease in the baseline mass with each cycle (**Figure 4C, 4D**); the average rate loss of sample mass was determined to be  $3.6 \times 10^{-4}$  and  $1.8 \times 10^{-4}$  mmol/h for [EMIM][2-CNpyr]:1,3-P and [EMIM][2-CNpyr]:DEG, respectively. This was lower than expected based on the evaporation rate of the capsules under a 1 h isotherm, as discussed above. After the first sorption-desorption cycle, the subsequent cycles had consistent

sample mass loss per cycle ( $0.024 \pm 0.002$  and  $0.024 \pm 0.003$  mg for [EMIM][2-CNpyr]:1,3-P and [EMIM][2-CNpyr]:DEG, respectively).



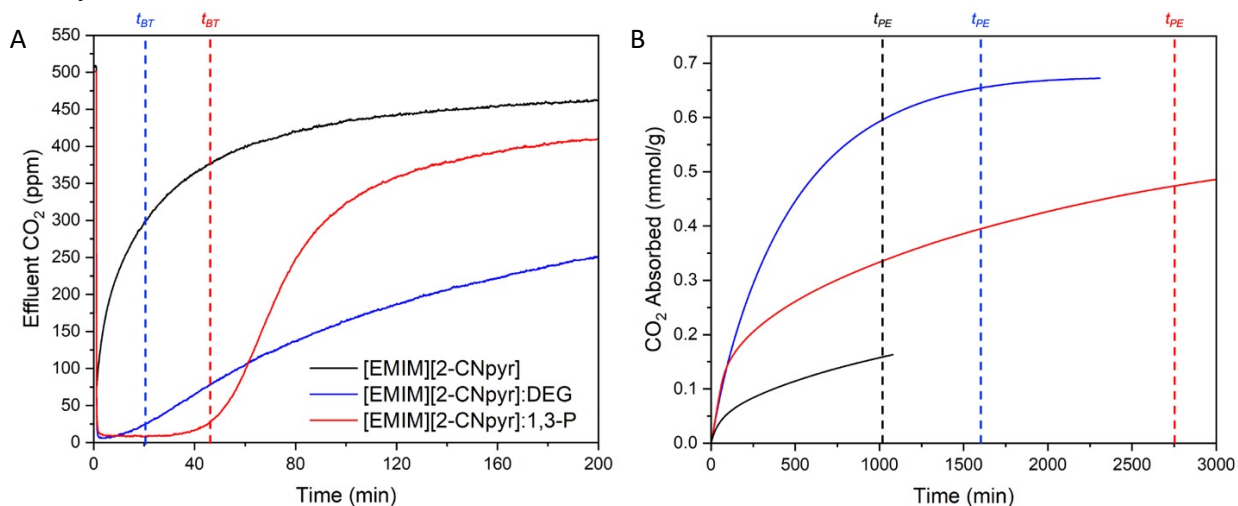
**Figure 4.** CO<sub>2</sub> sorption and desorption experiments conducted using TGA. [EMIM][2-CNpyr]:1,3-P results showed A) the CO<sub>2</sub> capacity per cycle (red bar graph) and C) the sorption/desorption curves based on mass where the absorption (solid black) is under a pure CO<sub>2</sub> environment at 25 °C and desorption (dashed red) is under a N<sub>2</sub> environment at 55 °C. [EMIM][2-CNpyr]:DEG results are outlined by B) the CO<sub>2</sub> capacity per cycle (blue bar graph) and D) the sorption/desorption curves based on mass with the same conditions as C.

**Breakthrough Experiments.** To access the sorbent performance of [EMIM][2-CNpyr], [EMIM][2-CNpyr]:DEG, and [EMIM][2-CNpyr]:1,3-P capsules and rate limitations (e.g., diffusion and reaction kinetics), breakthrough analyses were conducted. In a typical breakthrough experiment, capsules were packed in a column such that gas could be flowed through and the concentration of CO<sub>2</sub> coming out of the column measured. An ideal sorbent, i.e., one with no rate limitations, will present a step curve, where all CO<sub>2</sub> in the gas stream is absorbed until the sorbent reaches saturation, at which point the CO<sub>2</sub> concentration in the effluent will increase to the feed concentration. The breakthrough time ( $t_{BT}$ ) is determined when the effluent concentration reaches 5 % of the feed concentration (25 ppm CO<sub>2</sub>). Sorbents with greater mass transport limitations will present elongated S-curves, where elongation increases with greater kinetic barriers.

All three capsule types showed rate limitations such that by integrating the curves with respect to the feed concentration from 0 min to  $t_{BT}$  and  $t_{PE}$ , the breakthrough capacity and the pseudoequilibrium capacity, respectively, can be determined. The first 200 minutes of breakthrough curves for capsules of [EMIM][2-CNpyr], [EMIM][2-CNpyr]:DEG, and [EMIM][2-CNpyr]:1,3-P at 500 ppm CO<sub>2</sub> are presented in **Figure 5A**. The CO<sub>2</sub> loading over time is plotted in **Figure 5B**. Capsules containing only [EMIM][2-CNpyr] in the core were severely rate limited and did not absorb all CO<sub>2</sub> in the feed at the start of the experiment. This may be due to the low core loading ( $25 \pm 1.8$  wt%), however, this was comparable to the [EMIM][2-CNpyr]:1,3-P ( $28 \pm$

1.6 wt%) and [EMIM][2-CNpyr]:DEG (34 ± 3.6 wt%). Another possible cause for the limited breakthrough time could be column packing, as these capsules were highly aggregated and sticky compared to the [EMIM][2-CNpyr]:DEG and [EMIM][2-CNpyr]:1,3-P capsules, which made it very difficult to create a uniformly packed column without breaking the capsules. Aggregation also yields larger effective particles, significantly increasing diffusion distance and leading to greater rate limitations. The higher viscosity of the pure [EMIM][2-CNpyr] (75.3 ± 2.1 cP) compared to the glycol mixtures of [EMIM][2-CNpyr]:1,3-P (51.1 ± 2.1 cP) and [EMIM][2-CNpyr]:DEG (55.8 ± 2.4 cP) is also likely a significant factor impacting the sorption rate, especially in combination with capsule aggregation. The ratio of CO<sub>2</sub> to [EMIM][2-CNpyr] at full capacity is consistent with isotherm sorption values for bulk [EMIM][2-CNpyr] at 50 Pa (~500 ppm).<sup>14</sup> Capsules containing [EMIM][2-CNpyr]:1,3-P mixture had a  $t_{BT}$  of 44 minutes, indicating significantly reduced kinetic limitations compared the capsules of pure IL. These capsules were also a much finer powder which made uniform packing feasible. The pseudoequilibrium capacity was much higher as well, which is consistent with previous reports in a mixture of [EMIM][2-CNpyr] with EG, where the ratio of CO<sub>2</sub> to [EMIM][2-CNpyr] at lower partial pressures dramatically increases upon mixing with a hydrogen bond donor due to an additional “carbonate” binding route, where the hydroxyl is deprotonated by the highly basic IL anion as reported by Lee et al.<sup>19</sup>

Interestingly, the capsules containing [EMIM][2-CNpyr]:DEG in the core had a lower breakthrough time, 19 minutes, as well as a lower time to pseudoequilibrium, and yet displayed a much higher pseudoequilibrium capacity compared to the [EMIM][2-CNpyr]:1,3-P capsules. This is likely due to the [EMIM][2-CNpyr]:1,3-P capsules losing some 1,3-P over the extended sorption cycle, reducing the impact of the aforementioned carbonate formation and increasing the diffusion resistance for CO<sub>2</sub> by increasing viscosity. This is not observed to the same extent in the [EMIM][2-CNpyr]:DEG due to the higher boiling point of DEG, leading to greater overall CO<sub>2</sub> capacity of the mixture at low partial pressure, despite greater diffusion limitations. Both capsules were observed to be fine powders and were easily packed into the column, and thus the packing density was assumed to be similar.



**Figure 5.** Results of breakthrough experiments for capsules with [EMIM][2-CNpyr]-based cores. (A) First 200 minutes of breakthrough curves, with vertical dashed lines signifying the breakthrough time for each capsule. (B) CO<sub>2</sub> loading of the capsules calculated from the effluent CO<sub>2</sub> concentration using Eq. 2. Vertical dashed lines signify the pseudoequilibrium time.

By using the measured capsule composition, the ratio of CO<sub>2</sub> to [EMIM][2-CNpyr] could be determined, which represents the binding site saturation of the [EMIM][2-CNpyr] in the capsules. These values are presented in **Table 2**. Capsules of pure [EMIM][2-CNpyr] had a breakthrough CO<sub>2</sub> capacity of 0 due to significant kinetic barriers and packing limitations, in which the measured effluent CO<sub>2</sub> concentration never reached 25 ppm. In contrast, capsules of [EMIM][2-CNpyr]:1,3-P had the largest breakthrough CO<sub>2</sub> capacity (0.08 mol CO<sub>2</sub>/kg sorbent), despite having the longest pseudoequilibrium time (2756 min). [EMIM][2-CNpyr]:DEG capsules had a lower breakthrough CO<sub>2</sub> capacity of 0.03 mol CO<sub>2</sub>/kg sorbent with almost half the pseudoequilibrium time (1637 min) compared to [EMIM][2-CNpyr]:1,3-P capsules. Interestingly, [EMIM][2-CNpyr]:DEG had the highest pseudoequilibrium CO<sub>2</sub> capacity (0.66 mol CO<sub>2</sub>/kg sorbent), which suggests a higher binding site saturation ratio of 0.75. Although the core loading wt% is lower with capsules of pure [EMIM][2-CNpyr] compared to the capsules of the mixtures, pure [EMIM][2-CNpyr] capsules and [EMIM][2-CNpyr]:1,3-P capsules had similar core loading wt% (25 ± 1.8 and 28 ± 1.6 wt%, respectively), yet the pseudoequilibrium CO<sub>2</sub> capacity was much higher for [EMIM][2-CNpyr]:1,3-P.

**Table 2.** CO<sub>2</sub> absorption times and capacities under 500 ppm CO<sub>2</sub> in dry N<sub>2</sub>.

Capsule core	Breakthrough CO <sub>2</sub> capacity (mol CO <sub>2</sub> /kg sorbent)	Pseudoequilibrium time (min)	Pseudoequilibrium CO <sub>2</sub> capacity (mol CO <sub>2</sub> / kg sorbent)	Binding site saturation (CO <sub>2</sub> :IL)	Core loading wt%
[EMIM][2-CNpyr]	0	1027	0.16	0.13	25 ± 1.8
[EMIM][2-CNpyr]:1,3-P	0.08	2756	0.47	0.35	28 ± 1.6
[EMIM][2-CNpyr]:DEG	0.03	1637	0.66	0.75	34 ± 3.6

## Conclusions

The use of glycols as a viscosity modifier for IL-based mixtures for CO<sub>2</sub> sorption successfully decreased the viscosity and evaporation rates, however, there was a noticeable interaction between the glycol and a task-specific IL (TSILs) (i.e., [EMIM][2-CNpyr]). The decrease in evaporation is mainly attributed to the diffusion limitations of the glycols through the IL and molecular interactions (e.g., hydrogen bonding, etc.). To further decrease the evaporation rate of the mixtures, microencapsulation via a soft-templated approach was utilized. Encapsulated pure glycols and IL:glycol mixtures demonstrated the ability of the polyurea shell to act as a barrier while also increasing the working surface area of the sorbents. The two lowest evaporation rate mixtures were used for CO<sub>2</sub> sorption with [EMIM][2-CNpyr] were DEG and 1,3-P. It was found that the capsules of [EMIM][2-CNpyr]:DEG had the highest CO<sub>2</sub> capacity, albeit with a large kinetic barrier as determined by sorption/desorption cycles and breakthrough experiments. The use of ILs for sorption requirements can be utilized to a greater effect with the use of viscosity modifiers and encapsulation.

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## Abbreviations

DAC = direct air capture

IL = ionic liquid

TSIL = task specific ionic liquid

EG = ethylene glycol

1,3-P = 1,3-propanediol

PG = propylene glycol

DEG = diethylene glycol

[EMIM][2-CNpyr] = 1-ethyl-3-methylimidazolium 2-cyanopyrrolide

[BMIM][BF<sub>4</sub>] = 1-butyl-3-methylimidazolium tetrafluoroborate

[EMIM][BF<sub>4</sub>] = 1-Ethyl-3-methylimidazolium tetrafluoroborate

DAPM = 4,4'-diaminodiphenylmethane

HDI = hexamethylene diisocyanate

GO = graphene oxide

TGA = thermogravimetric analysis

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