

Sol-gel processing of a covalent organic framework for the generation of hierarchically porous monolithic adsorbents

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ABSTRACT. Covalent organic frameworks (COFs) have emerged as a versatile materials platform for applications including chemical separations, water purification, chemical reaction engineering and energy storage. Their inherently low mechanical stability, however, frequently renders existing methods of pelletisation ineffective contributing to pore collapse, pore blockage or insufficient densification of crystallites. Here, we present a general process for the shaping and densifying of COFs into centimetre-scale porous monolithic pellets without the need for templates, additives or binders. This process minimises mechanical damage from shear-induced plastic deformation and further provides a network of interparticle mesopores that we exploit in accessing analyte capacities above those achievable from the intrinsic porosity of the COF framework. Using a lattice-gas model, we accurately capture the monolithic structure across the mesoporous range and tie pore architecture to performance characteristics in both gas storage and separation applications. Collectively, these findings represent a substantial step in the practical applicability of COFs and other mechanically weak porous materials.

1. Main

Porous materials capable of reducing both the cost and energy intensity of industrial chemical processes are critically needed in transitioning to a carbon-neutral energy cycle.^{1,2} Constructed from earth-abundant elements and affording a combination of chemo-structural diversity, ease of synthetic modification and relative chemical stability, covalent organic frameworks (COFs) have emerged as attractive alternatives to existing porous materials including activated carbons, zeolites and metal-organic frameworks (MOFs).³⁻⁵ However, a technological limit has been reached where traditional methods of adsorbent post-processing are poorly suited to COFs as a result of the low mechanical stability frequently exhibited by these materials.⁶⁻¹¹ To date, these mechanical characteristics have been shown to limit the pressures that can be used during pelletisation^{10,12} and the selection of fluids available for activation⁶⁻⁸ – deviations from which can result in sharp losses in capacity. While factors such as framework topology and linker length can be synthetically tuned to target more robust architectures¹³, the inverse approach has not been attempted – i.e., whereby a desired COF can be shaped into an industrially relevant form factor without compromising key performance metrics.

Here, we report a rapid and general process for the shaping of COFs into macroscopic pellets without the use of binders, templates or additives, and without any further processing steps needed for a final application. For an archetypical two-dimensional (2D) COF, TPB-DMTP-COF,¹⁴ we demonstrate control over the degree of aggregation of crystallites within pellets and systematically identify the presence of a lower limit in inter-crystallite pore size for a given activation solvent. We tie this limit to the onset of capillary-action induced, turbostratic disordering of crystallites and further confirm that mechanical damage can be avoided through the use of an ultra-low surface tension activation fluid. COF monoliths thus prepared exhibit identical low-pressure adsorption characteristics to those of the best-reported powder analogues and, additionally, benefit from a system of interparticle mesopores that push final adsorption capacities above levels expected for single crystals. We capture these structural characteristics in a lattice-gas model, which accurately reproduces experimentally-derived isotherms for COF monoliths *in silico*. The combination of intact crystallites and hierarchical mesopores in an industrially-suitable pellet endows COF monoliths with superior adsorption properties relative to powders, which we demonstrate for both pure component gas storage (CO₂ and CH₄) and mixed gas chemical separation (CO₂/N₂ and CO₂/CH₄) applications. Based on these findings, our work not only provides a path forward for the industrial applicability of COFs but a systematic framework through which COF microstructure and final adsorption properties can be tuned without altering the underlying COF chemistry.

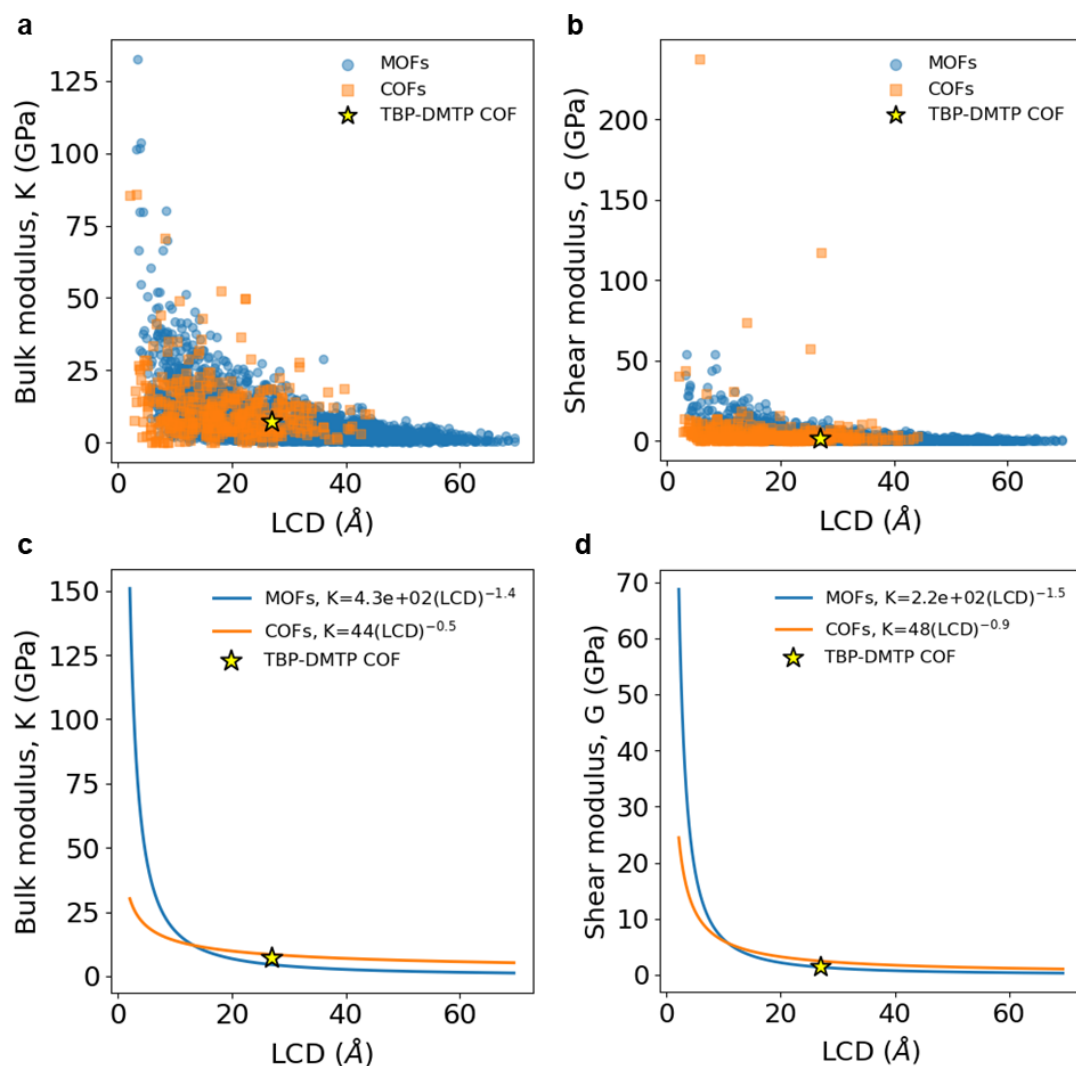
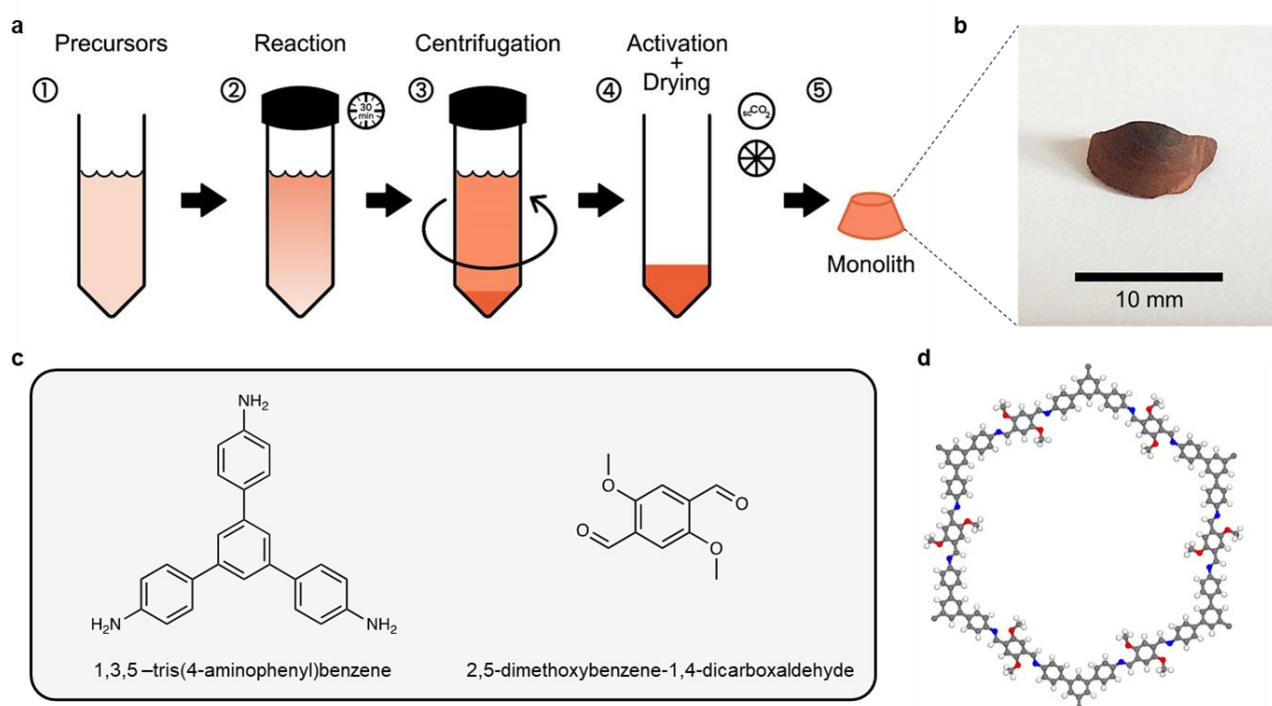


Figure 1 | Mechanical properties calculation. (a) Relationship between bulk modulus, K (GPa), and LCD (\AA) and (b) between shear modulus, G (GPa), and LCD (\AA) with MOFs in blue (circle), COFs in orange (square), and TPB-DMTP-COF in yellow (star). (c, d) Exponential fits to the data shown in figures (a) and (b), respectively, with MOFs in blue, COFs in orange, and TPB-DMTP COF in yellow (star).

2. High-throughput mechanical properties calculation

2D COFs are thought to be unstable to in-plane mechanical shear.⁹ To evaluate the mechanical properties of COFs across topologies and linkage chemistries, we first performed a high-throughput screen of all reported COFs as inventoried in the CURATED-COF database¹⁵ and compared their bulk moduli, shear moduli and elastic constants to those of MOFs¹³ (**Figure 1**). Within a largest cavity diameter (LCD) range of 15-40 \AA , the bulk and shear moduli of COFs were found to be similar to those of MOFs, with COFs exhibiting marginally higher bulk moduli and shear moduli on average. However, at lower LCD ranges characteristic of ultramicroporous ($< 7 \text{\AA}$) and microporous ($< 20 \text{\AA}$) materials, the bulk and shear moduli of COFs were found to be substantially lower than those of MOFs, suggesting an inherently greater tendency of COFs to mechanically deform even in the absence of larger ($> 15 \text{\AA}$) pores. To gain insights into the mechanical stability of these materials, we

84 then analysed the elastic constants of a representative COF subset, hexagonal 2D COFs, which
 85 currently account for 54% of 2D COFs and 45% of all COFs synthesised to date. Applying the
 86 stability criteria: $c_{11} > |c_{12}|$, $c_{33}(c_{11} + 2c_{12}) > 2(c_{13})^2$, $c_{11}c_{33} > (c_{13})^2$ and $c_{44} > 0$, a majority (64%) of
 87 hexagonal 2D COFs were found to be unstable, confirming weakness to mechanical shear as a
 88 predominating feature of these materials and possibly shedding light on the low degrees of
 89 crystallinity frequently exhibited by these materials. As conventional methods of powder pelletization
 90 routinely employ pressures in the range of 1-3 GPa, which are known to trigger losses in capacity
 91 within MOFs,¹⁶⁻²⁰ a revised approach for COF processing and pelletisation was sought.



92
 93 **Figure 2 | TPB-DMTP-COF monolith synthesis and structure.** (a) Processing workflow for TPB-DMTP-
 94 COF monolith formation. (b) TPB-DMTP-COF monolith. (c) Organic precursors used in the synthesis of the
 95 COF monolith. (d) Pore structure of TPB-DMTP-COF with C atoms in grey, N atoms in blue, O atoms in red,
 96 and H atoms in white.

97 98 3. Sol-gel synthesis of COFs

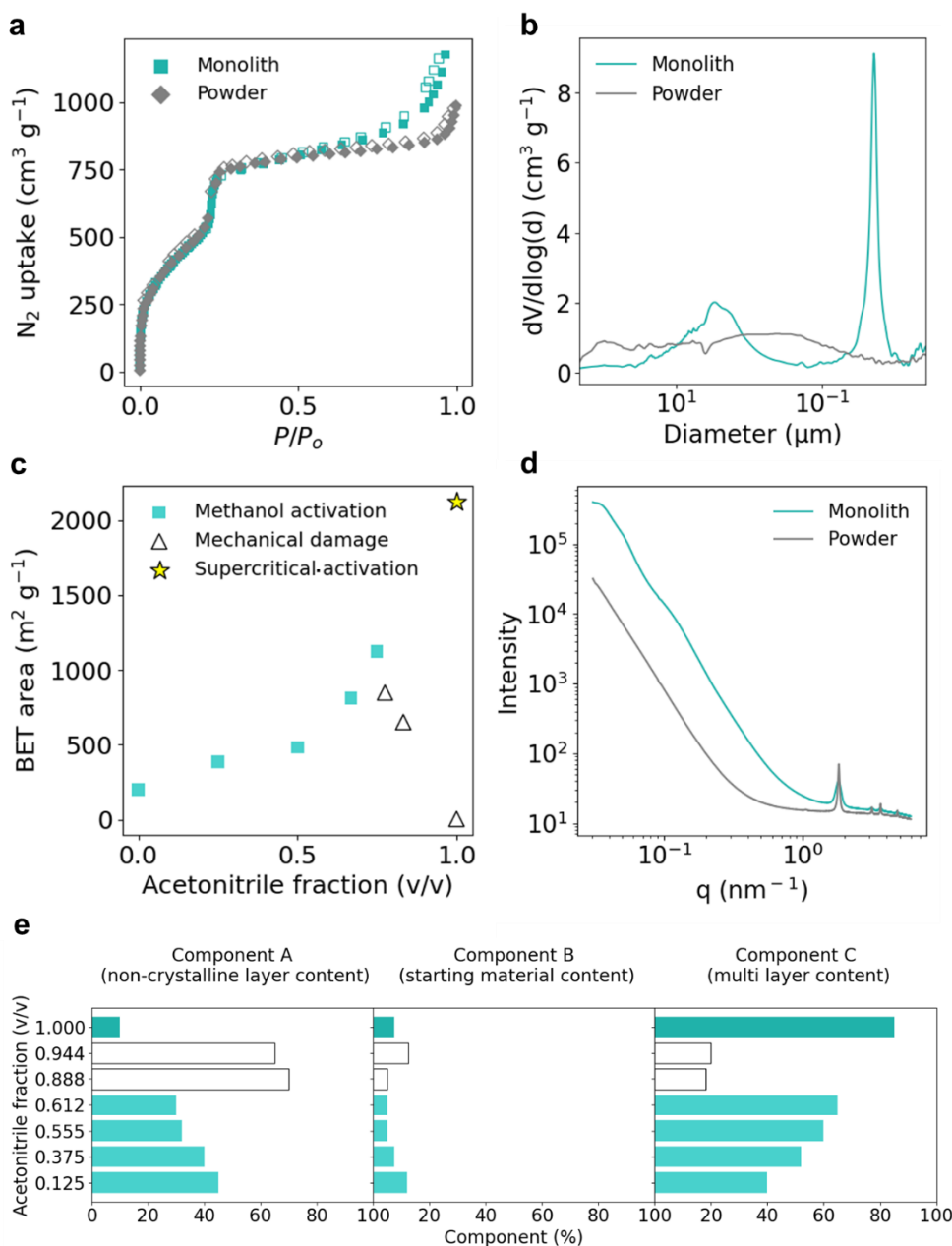
99 To permit ease of experimental benchmarking and analysis, TPB-DMTP-COF was identified as a
 100 representative 2D COF with an LCD of 25 Å and excellent known crystallinity. Upon screening a
 101 variety of synthesis solvent systems, acetonitrile and a 1:1 (v/v) mixture of 1,3,5-trimethylbenzene
 102 (mesitylene) and 1,4-dioxane (dioxane) were identified as two systems capable of both solubilising
 103 the starting materials and producing crystalline samples of TPB-DMTP-COF. However, whereas the
 104 1:1 (v/v) mixture of mesitylene and dioxane produced powder samples consisting of aggregated
 105 particles > 500 nm in diameter (**Figure S5a**), the acetonitrile system produced dense pellets consistent
 106 with those previously described for MOF monoliths and composed of particles of *ca.* 40 nm in
 107 diameter (**Figure S5h**) – well within limits previously established for monolith formation in MOFs¹⁷,

108 ¹⁸ (*i.e.* < 120 nm). Taking these two systems as extremes, solvent compositions consisting of different
109 fractions of each were used to prepare pellets following a process workflow that consisted of:
110 (1) reaction for a fixed amount of time (typically 30 minutes), (2) centrifugation, (3) purification and
111 solvent exchange to methanol, and (4) controlled drying and activation (**Figure 2**).
112

113 Upon processing, scanning electron microscopy (SEM) of the finished pellets revealed a gradual
114 progression in microstructure from larger, loosely aggregated particles to densely packed monoliths
115 exhibiting conchoidal fracture and little to no inter-particle free volume (**Figure S5**). Analysis of the
116 nitrogen adsorption isotherms (**Figure S3**) collected for these pellets, however, revealed a striking
117 trend. Whereas we observed a monotonic increase in Brunauer-Emmett-Teller (BET) area –
118 calculated using BETSI²¹ – for pellets synthesized in solvent systems containing acetonitrile fractions
119 ranging from 0.000 – 0.750 (v/v), a sharp decrease in BET area to 4 m² g⁻¹ was observed for samples
120 prepared at higher acetonitrile fractions (**Figure 3c**). As a result, the highest BET area that could be
121 obtained for TPB-DMTP-COF using methanol as the activation solvent was 1,122 m² g⁻¹ suggesting
122 the presence of a lower limit in inter-crystallite pore size beyond which pore disruption takes place.
123 To test whether this pore disruption was being induced by capillary-action,⁸ a further sample was
124 prepared in a pure acetonitrile solvent system and processed as before, but was dried and activated in
125 supercritical carbon dioxide (scCO₂) instead of in methanol and air. The finished pellet not only
126 recovered full porosity but lay on the monotonic trend previously described, exhibiting a BET area
127 of 2,125 m² g⁻¹ – slightly above those previously described for powder analogues of TPB-DMTP-
128 COF. When a higher rate of scCO₂ pressure release (8 bar h⁻¹ vs. 3 bar h⁻¹) was used during the
129 activation of an identically prepared 1.000 acetonitrile pellet, a reduction in BET area to 1,439 m² g⁻¹
130 was observed, further suggesting that losses in BET area occur as a result of capillary-action induced
131 damage.
132

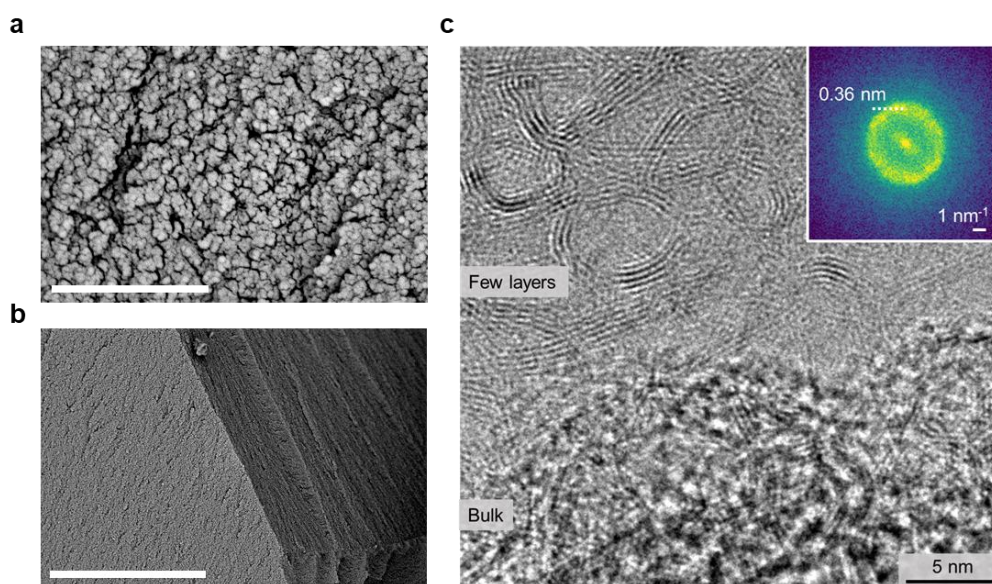
133 To gain deeper insights into the structural changes accompanying these bulk characteristics, we
134 used a combination of pair distribution function (PDF) and X-ray diffraction (XRD). Non-negative
135 matrix factorisation of the PDF-XRD data revealed three independent underlying components that
136 we attribute to non-crystalline layer COF content, residual starting material content, and multilayer
137 (*i.e.* crystalline) COF content – components A, B and C respectively (**Figure 3e**). For methanol-
138 activated pellets below an acetonitrile fraction of 0.75, a respective decrease and increase in
139 components A and C were observed as the acetonitrile fraction was increased, indicating that TPB-
140 DMTP-COF crystallinity gradually improves before the onset of mechanical damage. Above an
141 acetonitrile fraction of 0.750 (v/v), crystallinity sharply declines, resulting in an increased content of
142 non-crystalline layer TPB-DMTP-COF as seen from the increasing weighting of component A. When

143 scCO_2 is used during drying and activation, the multi-layer content is recovered – an observation
 144 consistent with findings from nitrogen adsorption studies and providing clear evidence for a
 145 correlation between mechanical disruption of COF crystallites during post-processing and observable
 146 gas uptake capacities as previously noted for powdered COF systems⁶.
 147



148
 149 **Figure 3 | Structural characterization of TPB-DMTP-COF monoliths.** (a) N_2 adsorption isotherms at 77 K
 150 for the 3 bar h^{-1} scCO_2 activated 1.000 (v/v) TPB-DMTP-COF monolith (turquoise squares), and powder (grey
 151 diamonds). (b) Mercury pore size distribution (PSD) of the 3 bar h^{-1} scCO_2 activated 1.000 (v/v) TPB-DMTP-
 152 COF monolith (turquoise), and powder (grey). (c) BET area vs. acetonitrile fraction (v/v); methanol activated
 153 samples (turquoise squares), samples with mechanical damage (white triangles), and supercritically activated
 154 (3 bar h^{-1}) sample (yellow star). (d) SAXS data of the supercritically activated (3 bar h^{-1}) TPB-DMTP COF
 155 monolith (turquoise), and powder (grey). (e) Bar chart showing the % of component A (non-crystalline layer
 156 content), component B (starting material content), and component C (multilayer content) as a function of
 157 acetonitrile fraction (v/v) for each sample studied.

158 To better understand the mechanism of crystallite disordering into non-crystalline layers within
 159 COF monoliths, we performed high-resolution transmission electron microscopy (HR-TEM) on a
 160 methanol-activated 1.000 acetonitrile control sample for which crystallites are sufficiently disrupted
 161 to afford a BET area of $4 \text{ m}^2 \text{ g}^{-1}$ (**Figure 4**). Analysis of the structure both within the bulk and within
 162 a few layers indicated a series of multi-layer crystalline domains bridged by turbostratic regions
 163 similar to those observed in graphitic carbon. Fourier transform analysis of the image (**Figure 4c**
 164 **inset**) further revealed that these features result in a single diffuse band corresponding to a real-space
 165 length of 0.36 nm – consistent with interlayer spacing values obtained from analysis of components
 166 A (0.37 nm) and C (0.35 nm) derived from the PDF-XRD data. Collectively, these findings both
 167 confirm the presence of disrupted crystallites in non-porous monoliths and suggest that a turbostratic
 168 disordering mechanism is responsible for such observable losses in porosity.



169
 170
 171 **Figure 4 | SEM and TEM images of the methanol-activated 1.000 acetonitrile fraction TPB-DMTP-COF**
 172 **monolith (a,b)** Scanning electron microscopy (SEM) images of the TPB-DMTP-COF monolith where the
 173 scale bar is 1μm for (a) and 10μm for (b). (c) HR-TEM image of the TPB-DMTP-COF monolith, showing
 174 locally layered structures connected by turbostratically disordered regions where the scale bar is 5 nm. The
 175 inset shows a fast fourier transform (FFT) from a thin area, indicating a broad ring, with the peak corresponding
 176 to 0.36.
 177

178 With post-processing conditions capable of explicitly avoiding crystallite damage established,
 179 we then used a combination of mercury porosimetry and small-angle X-ray scattering (SAXS) to gain
 180 insights into the structure of monolith free volume elements across the mesoscale. Pore size
 181 distributions derived from mercury intrusion curves for a scCO₂-activated 1.000 acetonitrile pellet
 182 revealed the presence of sharp mesoporosity at 18.7 nm attributable to well-defined interparticle free
 183 volume elements (**Figure 3b**). Broader macroporosity centred at pore width of around 3 μm was also
 184 observed. By contrast, a non-monolithic powder control prepared using the method of Xu *et al.* (BET

area of $1985 \text{ m}^2 \text{ g}^{-1}$)¹⁴ exhibited no well-defined meso- or macroporosity. Analysis of the respective mercury areas for accessible pore widths down to 3.9 nm (above that of the intrinsic framework, i.e. 2.5 nm) further showed an area of $504 \text{ m}^2 \text{ g}^{-1}$ for the monolith compared to $196 \text{ m}^2 \text{ g}^{-1}$ for the powder. These results were consistent with those derived from SAXS (**Figure 3d**). The scCO₂-processed monolith was well fit by a spheroidal particle model with two log normalized-distributions models with mean diameters of 25.8 nm ($\sigma = 0.4$) and 99.8 nm ($\sigma = 0.2$), indicating the presence of a mesoporous inter-particle free volume element and providing evidence for additional macroporosity. By contrast, the non-monolithic powder control was found to possess an inter-particle size distribution beyond the 0.5-100 nm range and was accordingly not fit. These results suggest that COF processing into monoliths can not only be used to avoid pore collapse but can provide additional mesoporosity, inaccessible from powders, that can be used to tune final uptake performance characteristics – potentially beyond those of purely crystalline systems.

To examine the impact of crystallite disordering on mesoporous free-volume elements, a scCO₂-processed monolith activated at an accelerated depressurisation rate of 8 bar h^{-1} (BET area of $1439 \text{ m}^2 \text{ g}^{-1}$) was also analysed using SAXS (**Figure S4**). The sample was fit by three spheroidal size-distribution models exhibiting mean diameters of 14.7 nm ($\sigma = 0.3$), 21.1 nm ($\sigma = 0.6$), and 98.5 nm ($\sigma = 0.1$). The emergence of a third, narrow free volume element along with an overall shift in mesopore distribution to smaller values suggests that disruption of crystallites is concomitant with a reduction in inter-particle free volume. As this reduction in inter-particle pore size can be controlled by the scCO₂ pressure release rate, future opportunities exist for top-down control over monolith microstructure and gas adsorption properties.

4. Molecular simulations and lattice gas model

To accurately capture the adsorption characteristics of TPB-DMTP-COF *in silico*, we carried out grand canonical Monte Carlo (GCMC) simulations on TPB-DMTP-COF crystalline fragments exhibiting varying degrees of interlayer slip. Starting from perfect AA stacking (0% slip), one of two sequential layers of the COF was gradually shifted until perfect AB stacking was achieved (100% slip). Using cells derived from 0, 25, 40, 50, 75, and 100% slipped starting structures (**Figure S1**), GCMC simulations were then used to generate predicted nitrogen isotherms at 77 K. Upon comparison of the respective low-pressure region and mesoporous step of the experimental adsorption isotherms to those derived from theory, a 40% slipped structure was found to provide the best agreement with experiment, giving almost identical low-pressure adsorption characteristics up to the mesoporous step (**Figure 5d**). Above the mesoporous step, however, whereas experimental isotherms for TPB-DMTP-COF powders maintained a reasonable agreement with those calculated from the

220 40% slipped structure until saturation, substantial deviations from theory were observed for
221 experimental isotherms derived from TPB-DMTP-COF monoliths as a result of inter-particle
222 mesoporosity. As these deviations ultimately push total nitrogen uptake within the monolith above
223 levels expected for purely crystalline systems, the ability to accurately capture such deviations
224 computationally is critical in evaluating and subsequently tuning final gas uptake characteristics for
225 a desired target application.

226

227 To model contributions to total gas uptake arising from inter-particle mesopores, we moved to a
228 lattice gas model of the TPB-DMTP-COF monolith. Lattice gas models have been extensively used
229 in the past to study the nature of sorption hysteresis for fluids in confined interconnected void spaces
230 of porous glasses.^{18,19} The structural model of the monolith (**Figure 5b**) used in the lattice-gas model
231 was numerically reconstructed from the SAXS data for the TPB-DMTP-COF monolith by means of
232 generating a two-point correlation function $S_2(r)$ and using it in the reconstruction algorithm. A 3D
233 reconstructed structure and its 2D slice used in the lattice gas model for the TPB-DMTP-COF
234 monolith activated using supercritical carbon dioxide are shown in **Figures 5a** and **5c** respectively.
235 To model the trajectory of the system in the grand canonical ensemble, we subsequently employed
236 kinetic Monte Carlo (kMC) simulations from which nitrogen adsorption isotherms at 77 K could be
237 obtained. The numerically generated isotherms show an excellent agreement with experimental data
238 for the TPB-DMTP-COF monolith within the high-pressure region of the adsorption isotherms,
239 providing complementary data to the GCMC-calculated isotherms and demonstrating the
240 applicability of lattice gas models in capturing the inter-particle mesoporosity of COF monoliths.
241 Collectively, these results suggest that the hierarchical porosity of COF monoliths can be accurately
242 described computationally across the micro and mesoporous range, enabling robust future predictions
243 of adsorption characteristics.

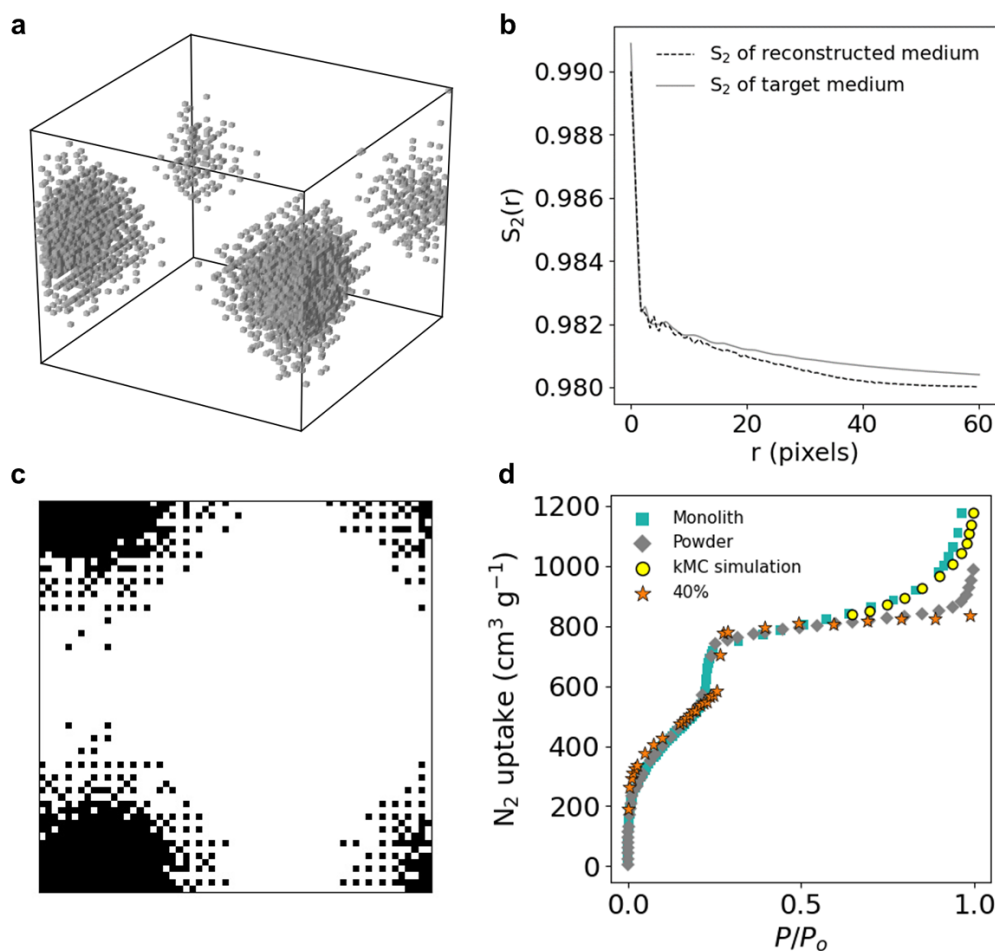


Figure 5 | Lattice gas model reconstruction and molecular simulations. (a) Reconstructed 3D realization of the TPB-DMTP-COF monolith defined on a bcc lattice with periodic boundaries; grey (white) voxels represent the solid (void) phase. (b) Comparison of $S_2(r)$ functions of target and reconstructed medium. The $S_2(r)$ function of the TPB-DMTP-COF monolith (target medium) is shown in grey and the $S_2(r)$ function of the reconstructed medium is shown in black (dashed line). (c) a 2D slice of the 3D realization showing all the possible sites occupied by the solid (in black) and void (in white) phases. The size of the system is 60 x 60 x 60 pixels for the 3D realization, and 60 x 60 pixels for the 2D slice. (d) Comparison of experimental adsorption isotherms to simulated adsorption isotherms of N_2 at 77 K. The experimental adsorption isotherms are represented by using the turquoise squares for the 3 bar h^{-1} scCO_2 activated 1.000 (v/v) monolith and grey diamonds for the powder. Yellow circles correspond to data points obtained by performing kMC simulations within the lattice gas model. Orange stars correspond to data points obtained by GCMC simulations taking into consideration a 40% slip between layers.

5. Gas adsorption characteristics of TPB-DMTP-COF monoliths

To demonstrate the utility of monolithic processing of COFs in gas storage applications, we performed pure-component adsorption studies on TPB-DMTP-COF powders and monoliths. Low-pressure isotherms collected at 298 K revealed good CO_2 (Figures 6a and 6d) uptake for both powders and monoliths with modest to low CH_4 (Figure 6a) and N_2 (Figure 6d) uptake respectively for both systems. However, up to pressures of 1 bar, while higher CO_2 uptake was obtained for monoliths over powders, lower uptake for both CH_4 and N_2 were obtained for monoliths relative to powders. These results suggest that the presence of inter-particle mesopores in monoliths can not only

be used to improve final storage capacities for a single component but can be used to favourably or disfavouredly influence final uptake characteristics of various components within a mixed feed.

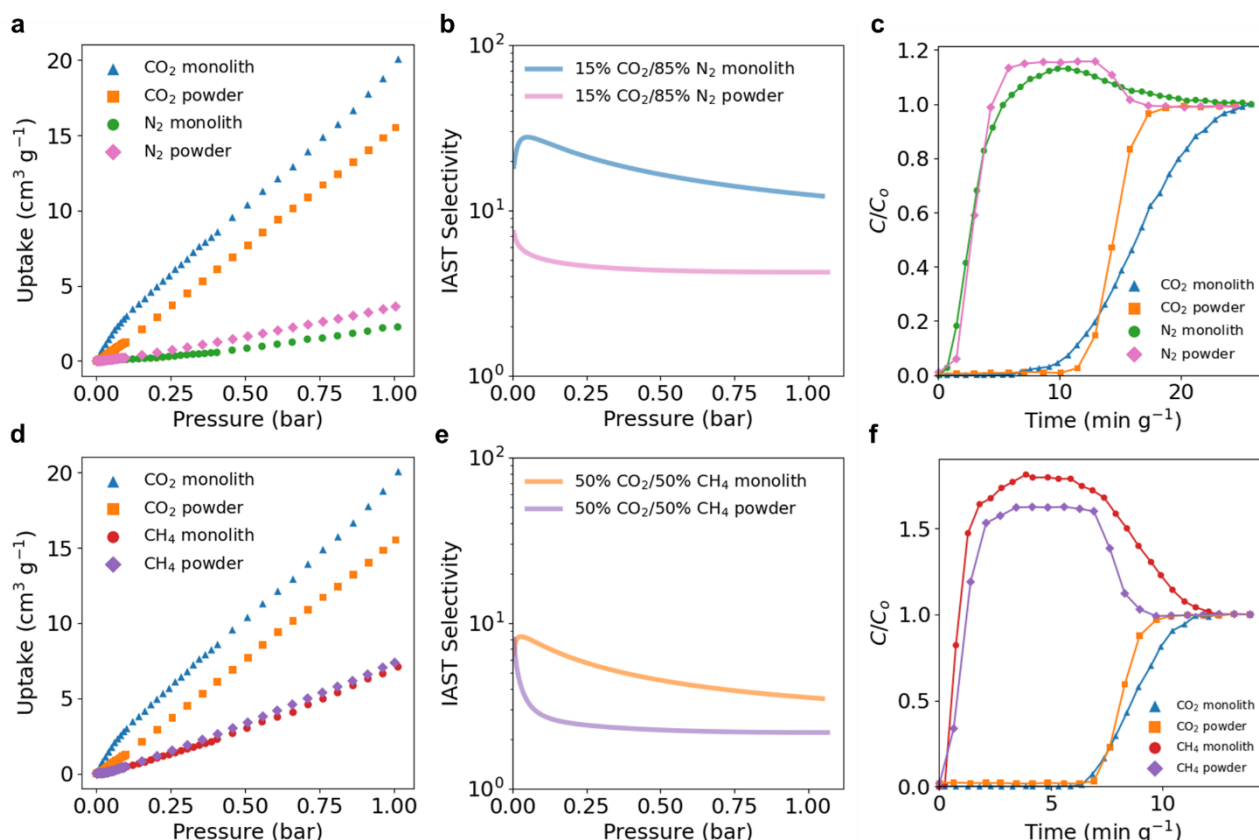


Figure 6 | Low-pressure adsorption isotherms, IAST selectivity, and breakthrough studies of TPB-DMTP-COF (3 bar h^{-1} scCO_2 activated 1.000 (v/v) monolith and powder control). (a) Low-pressure adsorption isotherms of CO_2 and N_2 at 298 K in TPB-DMTP-COF monolith – blue triangles for CO_2 and green circles for N_2 – and powder – orange squares for CO_2 and pink diamonds for N_2 . (b) IAST selectivity as a function of pressure for a 15% CO_2 /85% N_2 gas mixture for TPB-DMTP-COF monolith (blue) and powder (pink). (c) Breakthrough studies for a 15% CO_2 /85% N_2 gas mixture for TPB-DMTP-COF monolith (CO_2 – blue triangles, N_2 – green circles) and powder (CO_2 – orange squares, N_2 – pink diamonds) at 298 K. (d) Low-pressure adsorption isotherms of CO_2 and CH_4 at 298 K in TPB-DMTP-COF monolith – blue triangles for CO_2 and red circles for CH_4 – and powder – orange squares for CO_2 and purple diamonds for CH_4 . (e) IAST selectivity as a function of pressure for a 50% CO_2 /50% CH_4 gas mixture for TPB-DMTP-COF monolith (orange) and powder (purple). (f) Breakthrough studies for a 50% CO_2 /50% CH_4 gas mixture for TPB-DMTP-COF monolith (CO_2 – blue triangles, CH_4 – red circles) and powder (CO_2 – orange squares, CH_4 – purple diamonds) at 298 K.

To examine these characteristics within the context of chemical separations, we evaluated adsorption selectivities for industrially relevant compositions of CO_2 , CH_4 and N_2 mixtures. From pure-component adsorption isotherms, and using the Ideal Absorbed Solution Theory (IAST), we calculated selectivities for 15% CO_2 / 85% N_2 (Figure 6e) and 50% CO_2 / 50% CH_4 (Figure 6b) (v/v) mixtures. At low pressures, the selectivity for CO_2 relative to other components was substantially improved, providing evidence that monolithic COF structuring can be used to provide separation enhancements relative to unstructured COF powders. To confirm this, we performed dynamic

breakthrough studies on TPB-DMTP-COF monoliths and powders using mixed gas feeds. For the 15% CO₂ / 85% N₂ mixture (**Figure 6f**), while a comparable separation was achieved for the monolith relative to the powder, with some additional evidence for axial dispersion observed, the total CO₂ uptake was found to be 13.4% higher for the monolith. For the 50% CO₂ / 50% CH₄ mixture (**Figure 6c**), a markedly sharper separation for the monolith was observed relative to the powder with an additional improvement in CO₂ capacity of 8.6% achieved. Collectively, these results not only demonstrate the utility of monolithic processing for adsorbent-based chemical storage and separation but afford additional degrees of freedom through which the properties of COFs can be systematically designed and tuned.

6. Conclusions

Using a simple and general processing workflow, we introduce methods for the preparation of hierarchically porous COF monoliths without the need for additional materials or processing components. We show that such processing methods are compatible with mechanically weak materials, and further afford degrees of design freedom in the control of both extrinsic and intrinsic porosity. These characteristics endow monolithic COFs with properties that are distinct from both powder and single-crystal analogues, which we accurately capture *in silico* using a lattice gas model. We envision that such computational approaches can be used in future to predict gas uptake properties for broad classes of monolithic mesoporous materials. The extrinsic porosity present in COF monoliths can further be leveraged to simultaneously increase and decrease the final uptake capacities for various gas constituents relative to powder benchmarks, which we make use of in demonstrating improved separation performance for industrially relevant gas compositions. We believe that this study not only opens up new possibilities for the practical applicability of COFs but provides a pathway forward for tuning sorbent-analyte interactions where changes to the underlying framework chemistry may not be possible or synthetically accessible.

7. Methods

Materials

Scandium(III)trifluoromethanesulfonate (98%) was purchased from Alfa Aesar, 1,3,5-tris(4-aminophenyl)benzene (93%) was purchased from TCI, 2,5-dimethoxybenzene-1,4-dicarboxaldehyde (97%) was purchased from Sigma-Aldrich, methanol (99.9%), acetonitrile (99.9+%), 1,3,5-trimethylbenzene (99%), 1,4-dioxane (99.5%), were purchased from Acros Organics. All chemicals were used as received without further purification.

324 **Synthesis of TPB-DMTP-COFs**

325 *Monoliths*

326 To a 50 mL centrifuge tube were added 1,3,5-tris(4-aminophenyl)benzene (140.60 mg, 400 μ mol)
327 and 2,5-dimethoxybenzene-1,4-dicarboxaldehyde (29.13 mg, 150 μ mol). Solvent (16 mL) was then
328 added and the mixture was sonicated briefly to a homogenous suspension.
329 Scandium(III)trifluoromethanesulfonate²² (12 mg, 24 μ mol) was added, the tube was sealed, and the
330 mixture was sonicated again for *ca.* 20 seconds. The mixture was then left to react for 30 minutes
331 undisturbed. The sample was collected by centrifugation for 50 minutes, washed with three portions
332 of solvent (40 mL each) and an additional portion of methanol (40 mL), and was solvent exchanged
333 in methanol (40 mL) at 50 °C for 48 hours, with the solvent being replaced after 24 hours. The solvent
334 was then decanted, and the sample was washed with methanol (40 mL), and left to dry at 20 °C for a
335 further 24 hours, or dried using supercritical carbon dioxide. The sample was activated overnight at
336 120 °C under vacuum prior to characterization.

337 *Powders*

338 The TPB-DMTP-COF powder controls were synthesized using a previously reported procedure¹⁴.

339

340 **Characterization of TPB-DMTP-COF**

341 Total scattering data was collected at beamline 11-ID-B of the Advanced Photon Source (APS),
342 Argonne National Laboratory (ANL), IL, USA.²³ Monoliths were segmented into regions (rim, top,
343 and bottom; **Figure S6**) and lightly ground before loading into 1.1 mm (O.D.) Kapton™ capillaries.
344 High energy X-ray scattering data were recorded using a Perkin Elmer amorphous silicon-based area
345 detector using an X-ray wavelength of 0.2115 Å at a sample-to-detector distance of *ca.* 180 mm –
346 experimental geometry was calibrated using a CeO₂ diffraction standard. The images were calibrated
347 and reduced to 1D diffraction data within GSAS-II.²⁴ The X-ray scattering measured for an empty
348 Kapton™ capillary was used as the sample background. The data were background corrected in
349 xPDFsuite,²⁵ and $G(r)$ was calculated using data in the range $0.1 \text{ Å}^{-1} \leq Q \leq 23.1 \text{ Å}^{-1}$. Full details and
350 discussion on the total scattering data are included in the Supplementary Information, page S11.
351 Scanning Electron Microscope (SEM) images were acquired using an FEI XL30 FEGSEM with an
352 accelerating voltage of 5 kV. Samples were sputter coated with gold. Transmission Electron
353 Microscopy was carried out on a FEI Tecnai F20 TEM operated at 200 kV, and images were acquired
354 using a Gatan OneView camera.

355

356 **Helium pycnometry** was obtained using an AccuPyc 1330 Pycnometer from Micromeritics. This
357 technique was used to estimate the particle density and the volume of both powders and monoliths
358 by measuring the pressure change of helium in a calibrated volume. Each volume was recorded as an

359 average value of six consecutive runs. Prior to the analysis, all samples were activated overnight at
360 120 °C (vacuum) before measuring the mass.

361

362 **Mercury Porosimetry** was obtained up to a final pressure of 2,000 bar using an AutoPore IV 9500
363 instrument from Micromeritics. This technique was used to estimate the particle density of both
364 powders and monoliths at atmospheric pressure. Prior to the analysis, all samples were activated
365 overnight at 120 °C (vacuum) before measuring the mass, and then degassed in situ thoroughly before
366 the mercury porosimetry.

367

368 **Critical point dryer-CO₂ procedure.** A SPI-DRY Critical Point Dryer - Jumbo modify with a
369 manometer at the chamber was used to dry and activate the COF monoliths. First, the sample was
370 transferred into a dialysis membrane (Spectra/P.1 MWCO 6-8 kD) and sealed. Then, the membrane
371 was introduced into the critical point drying equipment. Then, it was immersed in subcritical (l) CO₂
372 at 283 K and 50 bar for half an hour. Then, the exchanged methanol was removed through a purge
373 valve followed by flushing with fresh (l) CO₂. This process was repeated three times. Subsequently,
374 the temperature was raised 5 K min⁻¹ up to 313 K to exceed supercritical CO₂ point. Finally, under
375 constant temperature (313 K), the chamber was vented at 8 bar h⁻¹ or 3 bar h⁻¹ to atmospheric pressure.

376

377 **Gas Adsorption Measurements.** Ultra-high-purity grade CH₄, N₂ and CO₂ were used for gas
378 sorption experiments. Adsorption experiments (up to 1 bar) for different pure gases were performed
379 on Micromeritics 3 Flex surface area and pore size analyzer. About 200 mg of activated samples were
380 used for the measurements. A temperature-controlled bath was used to maintain a constant
381 temperature in the bath through the duration of the experiment. Samples were degassed on a
382 Micromeritics PrepStation instrument prior to the analysis.

383

384 **Dynamic mixed gas breakthrough studies**

385 In a typical experiment, *ca.* 0.3 g of pre-activated sample was placed in a quartz tube (\varnothing = 8 mm) to
386 form a fixed bed held in place using quartz wool. For monolithic samples, individual monoliths were
387 broken and sieved to reduce the particle diameter to *ca.* 2 mm to ensure good packing within the
388 sample tube. Each sample was heated to 353 K under a dry helium flow to remove atmospheric
389 contaminants. Upon cooling, the chosen gas mixture was passed over the packed bed with a total flow
390 rate of 2 cm³ min⁻¹ at 298 K. The outlet gas concentration was continuously monitored using an
391 Agilent 5975 MSD mass spectrometer (MS). Upon complete breakthrough and saturation of the

392 packed bed adsorbent, the gas mixture is switched off and dry helium was flowed over the solid.
393 Heating was switch on and samples were heated to 353 K to aid regeneration.

394 To calculate the CO₂ uptake, initially, the gas mixture is passed through an empty reactor containing
395 quartz wool at a flow rate of 2 cm³ min⁻¹ as a blank reference. The gas flow is constantly monitored
396 using the MS. The CO₂ curve is integrated to calculate the area of the curve (A_{Ref}). Upon completion
397 of a CO₂ breakthrough experiment with an adsorbent, the area of the CO₂ adsorption curve is also
398 integrated (A_{Exp}). To calculate the total amount of CO₂ adsorbed, the following equation is used:

399
$$\text{Total CO}_2 \text{ Uptake} = (A_{\text{Ref}} - A_{\text{Exp}}) \times \text{CO}_2 \text{ flow (cm}^3 \text{ min}^{-1}\text{)}$$

400 **Molecular simulations**

401 The adsorption isotherms of N₂ are simulated using the grand canonical Monte Carlo (GCMC)
402 method as implemented in the RASPA simulation package²⁶. The geometric properties have been
403 calculated using Poreblazer^{27, 28}. A more detailed description about the methodology and model
404 parameters is given in the Supplementary Information, page S3.

406 **Lattice gas model**

407 First, the SAXS data collected was converted into a two-point correlation function $S_2(r)$ - defined as
408 the probability of two points separated a distance r apart, belong to the pore space of the medium -
409 which was then used as a benchmark to create a 3D reconstruction of the TPB-DMTP-COF monolith.
410 In order to model the trajectory of the system in the grand canonical ensemble, and to obtain the
411 adsorption isotherms we employ kinetic Monte Carlo (kMC) simulations. A more detailed description
412 about the reconstruction procedure and the kMC simulations is given in the Supplementary
413 Information, page S8.

415 **Mechanical properties calculation**

416 Mechanical properties for the COFs present in the CURATED COF database are calculated using
417 classical molecular mechanics via the ‘constant strain approach’ as implemented in the Forcite
418 module of Materials Studio. Some structures in the CURATED COF database for which, either the
419 mechanical or geometric property calculation failed, are excluded. The mechanical properties
420 calculated include the shear modulus, bulk modulus, and young’s modulus. A more detailed
421 description of the methodology used is given in the Supplementary Information, page S10.

423 **BET area calculation**

424 BET areas have been calculated using a computational tool called BET surface identification (BETSI)

425 - a tool that makes an unambiguous calculation of the BET area possible. More details about BETSI
426 can be found in the Supplementary Information, page S23.

427

428 **Data availability**

429 The experimental dataset generated and/or analysed during the current study are available from the
430 corresponding author on reasonable request.

431

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445

446 **Author contributions**

447 M.E.C. and D.F.-J. designed the research. M.E.C. performed the material synthesis and
448 characterization. M.E.C., D.G.M. and C.C. did the N₂ gas adsorption at 77K. D.G.M. and C.C. did
449 the N₂, CO₂, CH₄ gas adsorption at 298K. D.G.M. did the dynamic mixed gas breakthrough analysis.
450 N.P.M.C. carried out the SAXS and WAXS data collection. D.O.N. did the SAXS and WAXS data
451 analysis. D.O.N and K.C. did the PDF-XRD data collection and analysis. G.D. carried out the TEM
452 analysis. M.E.C. carried out the SEM analysis. N.R. and R.C. carried out the lattice gas modelling
453 under the supervision of S.T. N.R. carried out the molecular simulations and mechanical property
454 screens. J.A.M.I. did the scCO₂ drying and activation under the supervision of F.Z. J.S.A. carried out
455 the mercury porosimetry. M.E.C., N.R., and D.F.-J. wrote the the manuscript with contributions from
456 all authors.

457

458 **Conflict of Interest**

459 M.E.C. and D.F.-J. are inventors on International (WO) Patent Application No:

460 PCT/EP2020/075779 submitted by Cambridge Enterprise Limited that covers COF monoliths, as
461 well as aspects of their use. D.F.-J. has a financial interest in the start-up company Immaterial Labs,
462 which is seeking to commercialize metal–organic frameworks.

463

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