

The use of zeolite-based geopolymers as adsorbent for copper removal from aqueous media

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Abstract

Copper has been proven to have hazardous effects on human beings depending on its concentration levels. Recently, there has been a growing interest in developing geopolymers using local industrial minerals and by-products. However, research on the adsorption of heavy metals by geopolymer based on mordenite-rich tuffs is still limited. In the present study, an Ecuadorian zeolite-based geopolymer's removal capacity on copper ions in aqueous solutions, varying concentration, and contact time was tested. Kinetic models were developed using pseudo-first-order, pseudo-second-order, and the Elovich model. The adsorption data, using Cu^{2+} concentrations from 20 to 160 ppm, at 25 °C were described by the Langmuir and Freundlich isotherms and assessed by the linear coefficient of determination (R^2), resulting in the best fit for the Langmuir model. The attained adsorption capacity of 52.63 mg g⁻¹ demonstrates the low-cost geopolymer's effectiveness for this study and its competitiveness compared with other studies.

Keywords: Geopolymer; adsorption; zeolites; wastewater; kinetics; adsorption isotherms.

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1. Introduction

Copper, a heavy metal, has long and short-term adverse effects on human health, especially on the gastrointestinal system and the environment in general (National Research Council (US) Committee on Copper in Drinking Water, 2000; Taylor et al., 2020). Copper is widely used in the photographic and electronic industries, power plants in general, and consequently, is commonly found in wastewater. Therefore, its availability beyond a critical threshold in the environment is undoubtedly dangerous for human beings and animals. So, it is crucial to control and remove a significant amount of copper from water (Duan et al., 2016).

Adsorption processes are a feasible alternative due to their flexibility in design and operation, and, in many cases, they generate high-quality treated effluents. Several factors such as the size of the hydrated ions, free energy of hydration, and metal ions activity may be responsible for this selectivity of adsorption (Cheng et al., 2012). On the other hand, a geopolymer is an amorphous material generated by the reaction of an aluminum silicate with an alkali hydroxide, usually NaOH (Baykara et al., 2017; Arnoult et al., 2018). Recently, there has been a growing interest in developing geopolymers using local industrial minerals and by-products for immobilization of dangerous elements as a possible solution to struggle against heavy metal contamination (Barrie et al., 2015; Andrejkovicoá et al., 2016; Cristelo et al., 2020; Obenaus-Emler et al., 2020).

The removal of copper on metakaolin, fly ash, and zeolite-based geopolymers and other inorganic solids have been demonstrated in several studies (Wang et al., 2007; Yousef et al., 2009; Cheng et al., 2012; Sen Gupta and Bhattacharyya, 2014; Al-Harashseh et al., 2015). Fixed bed trials were carried out to assess modified silica capability to selectively remove Cu^{2+} from a multi-component solution (Kim and Yi, 2000; Sthiannopkao and Sreesai, 2009), by using boiler mud and ash to remove copper by adsorption and precipitation processes from metal refining water.

There has been little investigation done on the adsorption of heavy metals by geopolymer based on mordenite-rich tuffs to the best of our knowledge. In this case, the use of natural raw materials in geopolymer synthesis has been challenging, mainly due to their heterogeneity.

The purpose of this study is to evaluate the capacity of the Ecuadorian zeolite-based geopolymer for the removal of copper ions in aqueous solutions by varying concentrations and contact times.

2. Materials and methods

Preparation of the geopolymer

The Ecuadorian zeolite was pulverized in a ball mill to collect the fraction less than 60 μm . Subsequently, it was added to an activating solution composed of Na_2SiO_3 (Merck, density 1.35 g mL^{-1} at $20 \text{ }^\circ\text{C}$, Na_2O 7.5-8.5%, and SiO_2 25.5-28.5%) and 10 M NaOH (Merck-Millipore, 99% purity) at a ratio of 2.5:1. The solution was mixed with zeolite at a ratio of 0.45 mL g^{-1} and stirred for 2 minutes. The resulting mixture was poured in 5 x 5 x 5 cm wooden molds, covered with plastic bags, and placed in an oven at $60 \text{ }^\circ\text{C}$ for 24 hours. Finally, the cubes were left at room temperature ($26 \pm 2 \text{ }^\circ\text{C}$) for 9, 16, and 27 days before the compressive strength testing.

Characterization of the geopolymer

For structural stability, compressive strength tests were performed to assess the zeolite-based geopolymer's strength, using the ASTM C109 / C109 M-16a standard method and a SHIMADZU UTM-600KN, Universal Testing Machine. Prior testing, geopolymer blocks labeled as B3, C3, and D3, were sanded, sized (46.86mm x 50.52mm x 46.24 mm, 48.30mm x 50.60mm x 46.80 mm and 51.78mm x 47.45mm x 45.62 mm, respectively), and analyzed for compression tests at 10, 17 and 28 curing days. The tensile rupture strength values were 40.3875, 52.1888, and 66.0000 kN for B3, C3, and D3, respectively. Geopolymer blocks were placed in an oven at 60°C for one day and then cured at room temperature ($26 \pm 2^\circ\text{C}$) for an additional 9, 16, and 27 days before compressive strength tests were carried out.

For quantitative X-ray diffraction analysis, a PANalytical X'Pert PRO equipment was used at 30 mA, 45 kV, and angular measurement range of 0-80 (2°Theta). According to the study reported by Baykara *et al.* (Baykara et al., 2017). The peaks of the crystalline structures present in the samples were determined with an X'Per High Score Plus Software.

The elemental composition of the zeolite-based geopolymer samples was analyzed utilizing Dispersive Energy Spectrophotometry using an FEI-Inspect S Scanning Electron Microscope. For this purpose, the samples were crushed, and a small portion was taken on a plate with a graphite sheet. The gold coating was applied for the high-resolution micrographs of geopolymer samples.

For the Fourier-Transform-Infrared Spectroscopy (FTIR) test, 2 mg of the zeolite-based geopolymer samples (previously dried at 60 °C for 6 hours) were mixed and homogenized with 200 mg KBr, in an agate mortar. A pressure of 9 MPa was applied for 7 minutes for the pellet preparation. A Spectrum 100 Perkin Elmer spectrophotometer was used for the testing, with an atmosphere of UHP nitrogen, with a spectrum range between 4000 and 400 cm^{-1} and a resolution of 1 cm^{-1} .

For the thermogravimetric and the differential scanning calorimetry analysis, 10.0 ± 0.5 mg of the geopolymer sample was weighed in a previously red hot burned capsule. The equipment used was a thermogravimetric calorimeter TA SDT Q600, with a nitrogen flow of 100 mL min^{-1} and a ramp of 10.00 $^{\circ}\text{C min}^{-1}$ in a range between 25 up to 1000 $^{\circ}\text{C}$. The data were interpreted using an Advantage TA Universal Analysis 4.5A software.

Adsorption experiments

For the adsorption experiments, the geopolymer samples were grounded to a particle size of less than 60 μm . The tests were carried out in batch mode. For that, the synthesized geopolymer was dried for 2 hours at 100 $^{\circ}\text{C}$ and weighed before each adsorption experiment. On the other hand, standard solutions of 100 ppm and 250 ppm of Cu^{2+} were prepared for the batch mode experiments, and for the determination of the adsorption isotherm, the Cu^{2+} concentration varied between 20 ppm and 160 ppm at a temperature of 25 $^{\circ}\text{C}$. First, 50 mL of copper solution was poured into glass flasks previously immersed in a water bath to stabilize the temperature. Subsequently, 0.1 g of geopolymer was added to each flask, gently homogenized, and allowed to stand still for 2 hours. The solution was immediately vacuum filtered using 0.45 μm filter paper and analyzed by flame atomic absorption spectroscopy (FAAS). The quantity of the copper adsorbed onto the geopolymer samples has been determined quantitatively using the atomic absorption spectrometer (Thermo Scientific ICE 3000 Series).

For the kinetic analysis, flasks containing 100 ppm of Cu²⁺ in aqueous solution and adsorbent dose of 2 g L⁻¹ were placed in a water bath at 25°C. The flasks were vacuum filtered using 0.45 µm filter paper at a specified time and analyzed by FAAS.

The Effective removal of methylene blue from water using phosphoric acid based geopolymers: synthesis, characterizations and adsorption studies capacity q (mg g⁻¹) and the efficiency were determined with equations 1 and 2, respectively:

$$q = \frac{(C_o - C_e) * V}{m} \quad (1)$$

$$E = \frac{(C_o - C_e)}{C_o} * 100\% \quad (2)$$

Where C_o (mg L⁻¹) is the initial concentration, C_e (mg L⁻¹) is the equilibrium concentration, V (L) is the volume of the solution, and m is the mass of the adsorbent.

3. Results and discussion

3.1. Characterization of the geopolymer

3.1.1. Quantitative X-ray diffraction (XRD)

Table 1 and figure S1 (in supplementary files) present the XRD analyses of the zeolite and the three geopolymer samples prepared (G-10, G-17, and G-28) and cured for an additional 9, 16, 27 days at room temperature. The tuffs are mainly composed of mordenite, quartz, and calcite. For the geopolymer samples, the amount of amorphous, ill-crystallized, or non-crystallized phases increases with the curing time but decreases silica and mordenite. It seems that during the curing time, mordenite and quartz react with the alkaline activator to form an amorphous phase, mainly sodium aluminosilicate hydrate, as a result of geopolymerization reaction (Ruiz-Santaquiteria et al., 2013; Garcia-Lodeiro et al., 2015; Biel et al., 2020).

Table 1. XDR analysis for crystalline structures and amorphous content of zeolite and geopolymer samples at room temperature.

XRD	Quartz (Qz) (%)	Mordenite (%)	Calcite (%)	Amorphous (%)
Zeolite	20.8	28.5	4.2	46.4
G-10	18.4	28.3	5.7	47.6
G-17	15.5	24.7	5	54.8

G-28	13.4	19.6	3.3	63.7
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3.1.2. FTIR analyses

Both zeolite and geopolymer samples have been analyzed in the wavenumber range from 4000 to 400 cm^{-1} (see Figure S2 in supplementary files). Different bands were identified: (i) The band located around 3460 cm^{-1} is attributed to an asymmetric extension of H-O. Likewise, (ii) the band around 1636 cm^{-1} is due to H-OH bending and the adsorption of hydroxyl groups by excess alkali and water, respectively. Similarly, (iii) the vibration around 1040 cm^{-1} is credited to asymmetric extensions between Si-O-Si or Al-O-Si. Finally, (iv) the peaks around 1430 and 876 cm^{-1} are attributed to carbonate formed by exposure to atmospheric air (Singhal et al., 2017; Yan et al., 2019). The other peaks below 798 cm^{-1} are endorsed to different stretching modes, ring vibration of the structural network, and bending between Si-O and Al-O bonds.

3.1.3. Thermogravimetric analysis and differential scanning calorimetry (TGA-DSC)

Table 2 and figure S3 (in supplementary files) indicate the zeolite's thermogravimetric analysis and the geopolymers studied in this study. Between 0-110 $^{\circ}\text{C}$, there is a significant loss of mass due to solid residual NaOH, a possible increase in the material's porosity, which is evidenced in a more significant loss of surface water. In the range between 550- 750 $^{\circ}\text{C}$, the zeolite losses more mass compared to the geopolymer. This can be explained by the fact that the zeolite contains CaCO_3 , whose decomposition point is around 700-750 $^{\circ}\text{C}$, while the geopolymer, containing NaOH in excess, replaces Ca for Na, forming Na_2CO_3 , which decompose in CO_2 and Na_2O at temperatures above 1000 $^{\circ}\text{C}$. Considering ca. 14-15% total mass loss, it is evident that geopolymer samples are highly thermally stable. Due to this reality, this kind of materials can be used as at high temperatures for different applications (Khan et al., 2015).

Table 2. TGA-DSC analysis (up to 1000 °C) for zeolite and geopolymer samples

Sample	Mass loss (%)						Total mass loss (%)	
	Temperature (°C)	0-110	110-200	200-320	320-550	550-750		750-990
Zeolite		3.77	1.72	1.08	1.52	7.48	0.41	15.98
Temperature (°C)	0-150	150-212	212-350	350-600	600-700	700-750		
G- 10	8.39	1.96	2.01	1.21	0.7	0.1	14.37	
G- 17	8.09	1.96	1.97	1.66	0.82	0.07	14.57	
G- 28	7.26	2.12	2.15	1.73	0.81	0.05	14.12	

3.1.4. Scanning electron microscopy and energy dispersive spectroscopy (SEM-EDS)

As seen in figure 1, there is an increase in sodium percentage in the geopolymer sample analyzed. This change is attributed to NaOH and sodium silicate used for geopolymer synthesis. On the other hand, the increase in carbon percentage is due to the uptake of CO₂ (carbonation) with unreacted and excess alkaline activators. Semi-quantitative elemental analysis by SEM-EDS of both raw material zeolite and all corresponding synthesized geopolymers are presented in figure 1.

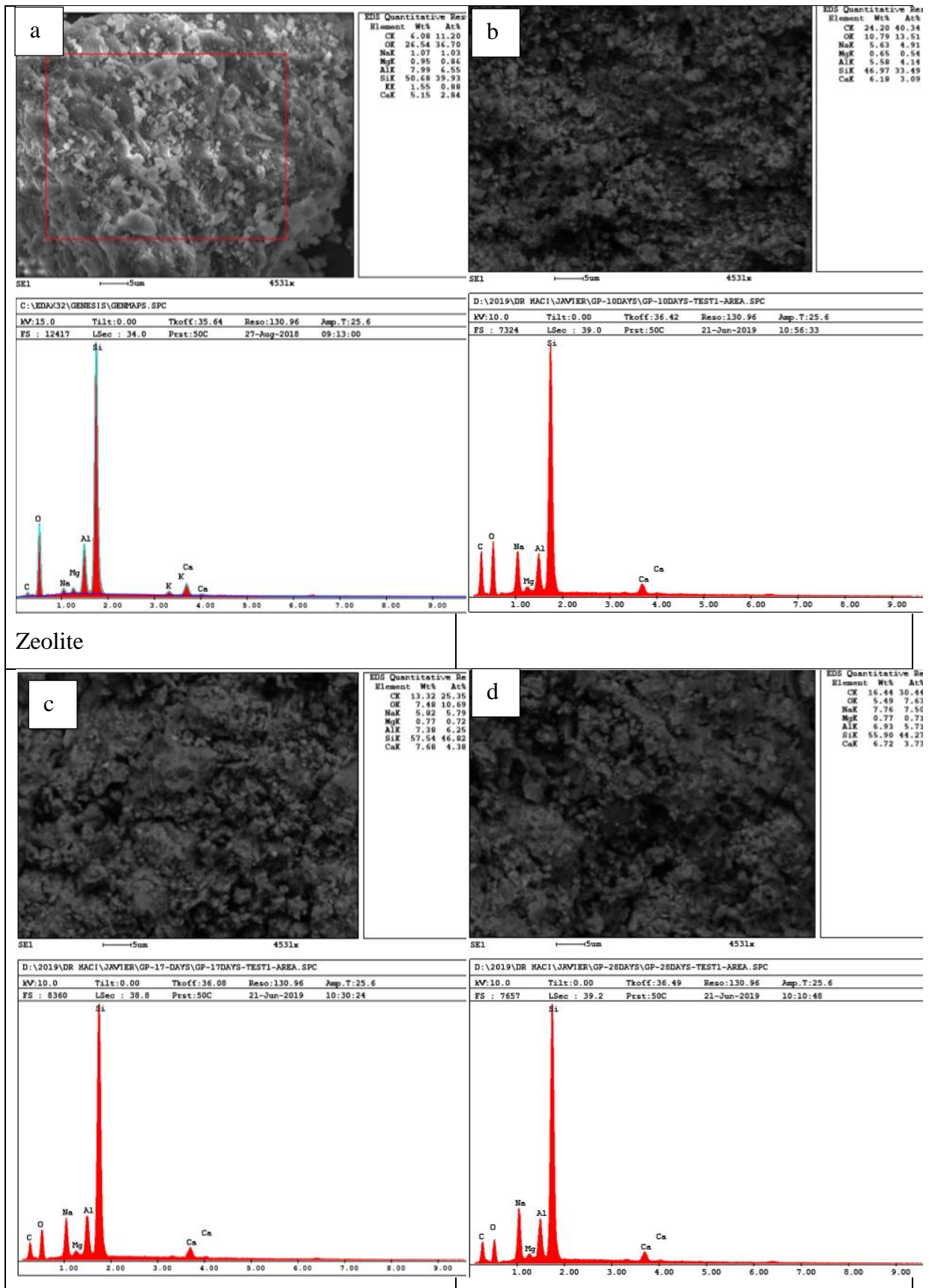


Figure 1. SEM-EDS images for **a)** zeolite, **b)** geopolymer cured for 9 days, **c)** geopolymer cured for 16 days, and **d)** geopolymer cured for 27 days.

As seen in SEM-EDS images (see figure 1), it is clear that there is an increase in C and Na elements attributed to the formation of carbonates and activators used NaOH and sodium silicate, respectively (Baykara et al., 2020).

Figure 2 shows the microstructure of natural zeolite and geopolymer synthesized.

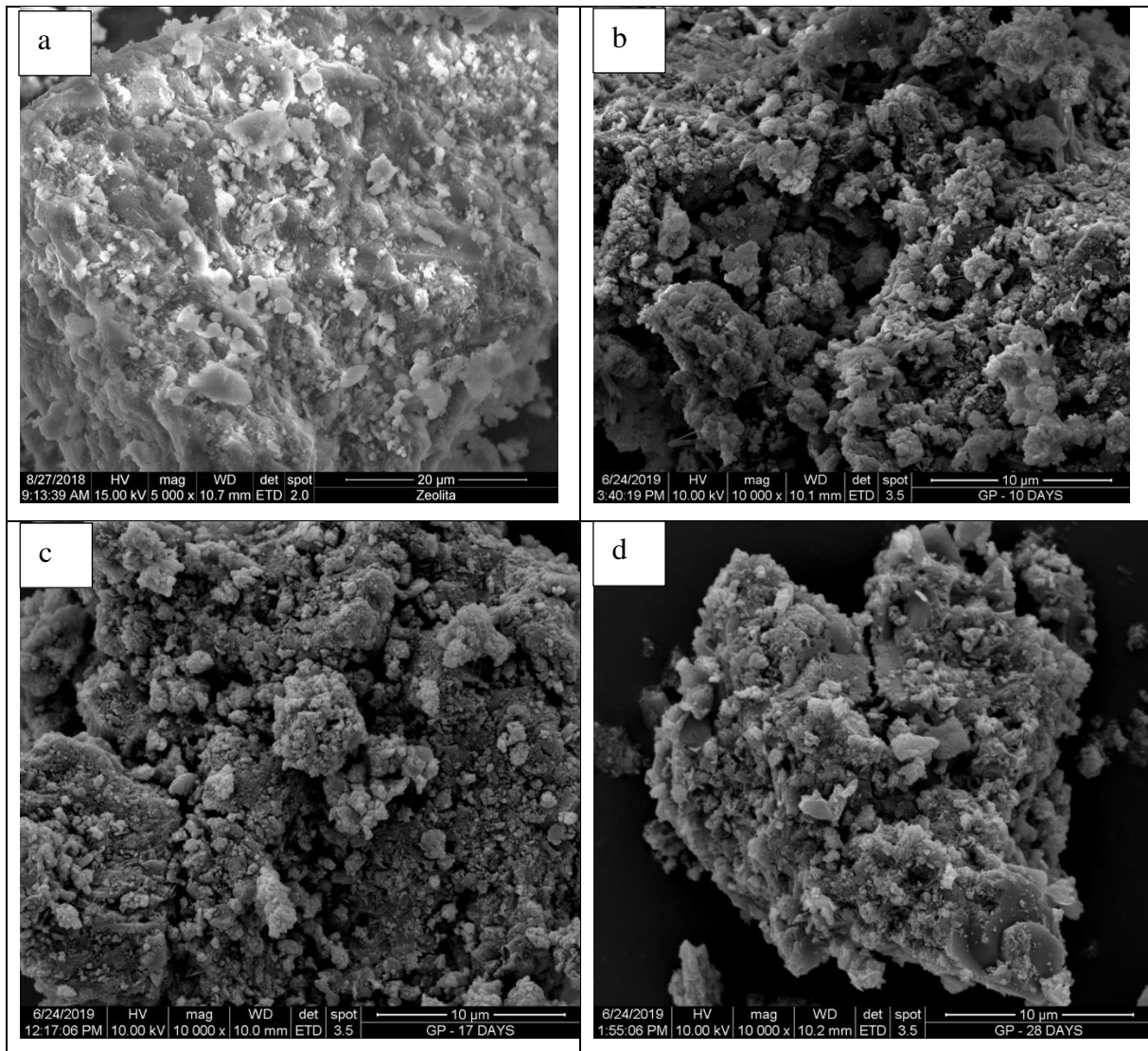


Figure 2. SEM micrographs a) zeolite, b) geopolymer cured for 9 days, c) geopolymer cured for 16 days, and d) geopolymer cured for 27 days.

Micrographs demonstrate that especially geopolymer samples have porous structures, which allows them to be used as adsorbents for copper removal from wastewater (Cheng et al., 2012; Duan et al., 2016).

3.2. Geopolymer compressive strength tests

Table 3 shows the compressive strength of the geopolymers developed for this study. Additionally, the stress and strain curve of geopolymer samples' compressive strength tests can be seen in figure S4 (in supplementary files). There is a direct relationship between the curing time and the mechanical properties. Thus, the longer the curing time, the higher the compressive strength obtained. The geopolymer structure's hardening behavior suggests transforming mordenite and calcite into a load-bearing material as time increases. Several studies reported the highest curing days for different compressive strength tests and temperatures: 28 days (15.84 MPa and 50°C) for a mixture of metakaolin, zeolite and cork residues (Sudagar et al., 2018); 14 days (9.95 MPa and 50 °C) for a mixture containing metakaolin and zeolite (Andrejkovičová et al., 2016); 28 days (10 MPa at 60 °C) for an Ecuadorian zeolite-based geopolymer (Baykara et al., 2017) and 14 days (about 19 MPa at 80 °C) for other type of Ecuadorian zeolite-based geopolymer (Ulloa et al., 2018).

Table 3. Compressive strengths geopolymer blocks

Block	Curing Time (Day)	Maximum compressive strength (MPa)
B-3	10	17.06
C-3	17	21.35
D-3	28	26.86

3.3. Kinetic results

Figure 3 shows the variation of Cu^{2+} concentration plotted versus time. It can be seen a step-down in Cu^{2+} concentration within the first minute of contact of the geopolymer with the Cu^{2+} solution, dropping from 94.7 to 28.32 ppm. Then, a slight decrease begins for 2 hours, reaching 5.02 ppm of Cu^{2+} in the solution. The kinetic model was determined by the linearization approach using equations 3 to 5 for pseudo-first-order, pseudo-second-order, and Elovich, respectively (figure 4-6). The results obtained can be seen in table 4.

$$q_t = q_e(1 - e^{-k_1 t}) \quad (3)$$

$$q_t = \frac{q_e^2 k_2 t}{1 + q_e k_2 t} \quad (4)$$

$$q_t = \frac{1}{\beta} \ln(v_o \beta) + \frac{1}{\beta} \ln(t) \quad (5)$$

Where q_e is the adsorption capacity at equilibrium, q_t is the adsorption capacity until t , k_1 is the pseudo-first-order constant, k_2 is the pseudo-second-order constant, β is the desorption constant, and v_o ($\text{mg g}^{-1} \text{t}^{-1}$) is the initial adsorption rate.

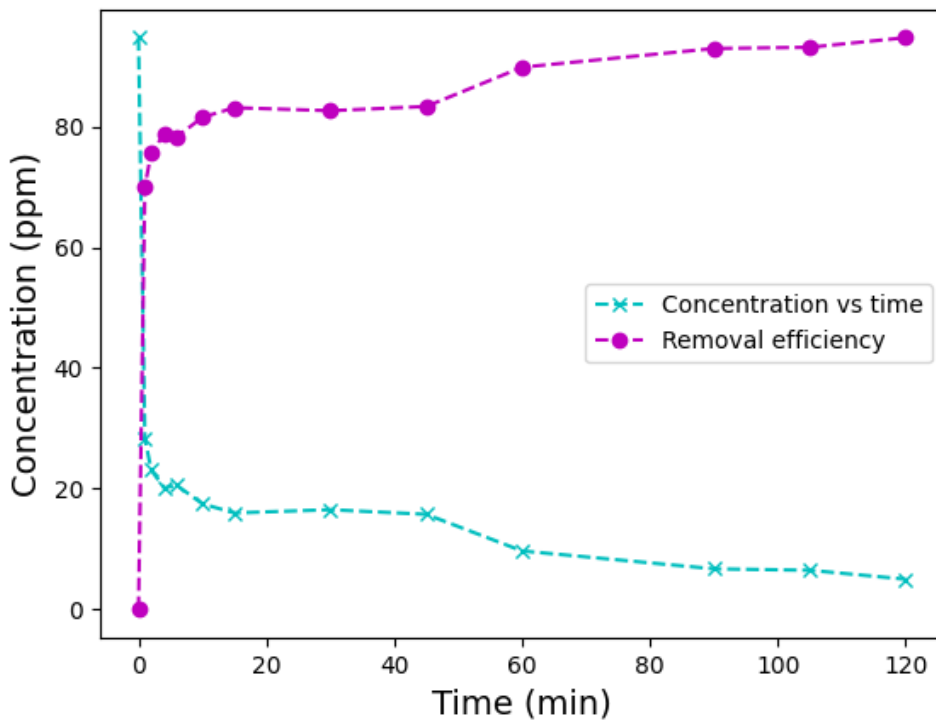


Figure 3. Change of Cu^{2+} concentration and geopolymer percentage of removal versus Cu^{2+} initial concentration as a function of time: 94.7 ppm; period: 120 minutes; batch constant temperature: 25 °C.

When comparing figures 3 to 5, it can be asserted that the adsorption process is better described by the pseudo-second-order equation rather than the pseudo-first-order equation, based on the linear coefficient of determination (R^2).

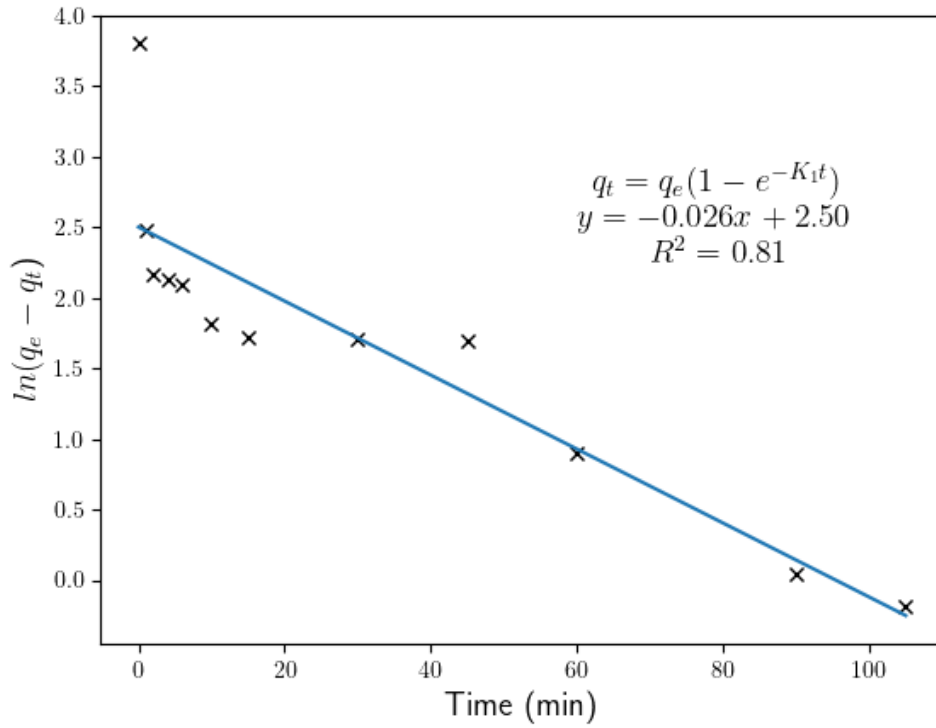


Figure 4. Kinetic result of the pseudo-first-order model in Cu^{2+} adsorption

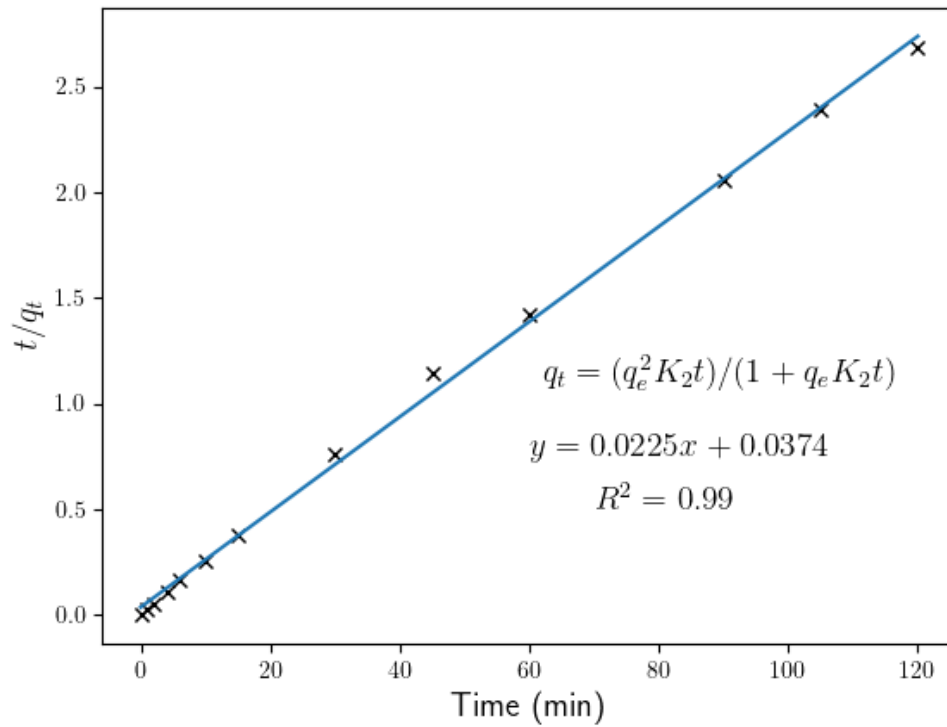


Figure 5. Kinetic result of the pseudosecond-order model in Cu^{2+} adsorption

It must be said that each known theoretical ground of pseudo-second-order equation is based on fundamental theories of surface reactions (Azizian, 2004). Therefore, this equation is more accurate as the system reaches equilibrium and diffusion-driven sorption kinetics in non-equilibrium processes (Plazinski et al., 2013). This equation is linked to the direct adsorption/desorption process controlling the overall rate of sorption kinetics (Plazinski et al., 2009), which is the present study's case.

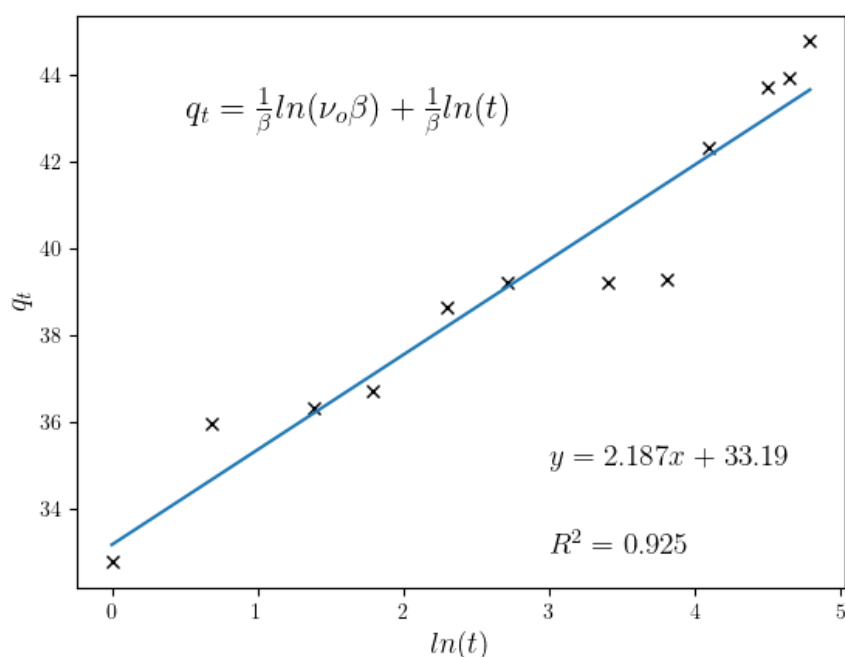


Figure 6. Kinetic result of the Elovich model in Cu^{2+} adsorption

Table 4. Kinetic parameters for adsorption of Cu^{2+} on geopolymer. Cu^{2+} initial concentration: 94.7 ppm. Experimental period: 120 minutes, batch temperature: 25°C.

Model	Parameters	Value	Unit
Pseudo first order	R^2	0.81	
	K_1	0.0262	min^{-1}
	q_e	12.21	mg g^{-1}
Pseudo second order	R^2	0.99	
	K_2	0.0135	$\text{g mg}^{-1} \text{min}^{-1}$
	q_e	44.44	mg g^{-1}
Elovich	R^2	0.925	

	β	0.4571	g mg^{-1}
	V_0	8517998.22	$\text{mg g}^{-1} \text{min}^{-1}$

Other models, such as the Weber-Morris model (equation 6), are based on intraparticle diffusion, which explains that the ion exchange phenomenon is proportional to the square root of time.

$$q_t = K_{id}t^{0.5} + C \quad (6)$$

K_{id} is the intraparticle diffusion ratio, and C is a constant model (Luukkonen et al., 2016b, 2016a). This model can explain whether the adsorption mechanism occurs on the surface or in the geopolymer's pores. In Figure 7, a multilinearity is observed in the diffusion model, indicating a slow ingress of ions into the pores (sodium ion exchange), which appears to be slow, as reflected by the slope. The experimental results brought about for stage K_{id} : 0,9863 and for C : 34,116 (R^2 : 0,9199) (see figure 7). Nevertheless, it can be asserted that the Weber-Morris plot for this study, indicates that the sorption process consists of several phases. Furthermore, the plots do not pass through the origin, showing that the rate-limiting step is not the pore diffusion (i.e., intraparticle) but the film diffusion (i.e., boundary-layer). Therefore, the first phases of sorption are related to the attachment to the most readily available surface sites, whereas the latter phases involve the slow diffusion of adsorbate from the surface to the inner pores (Luukkonen et al., 2016a).

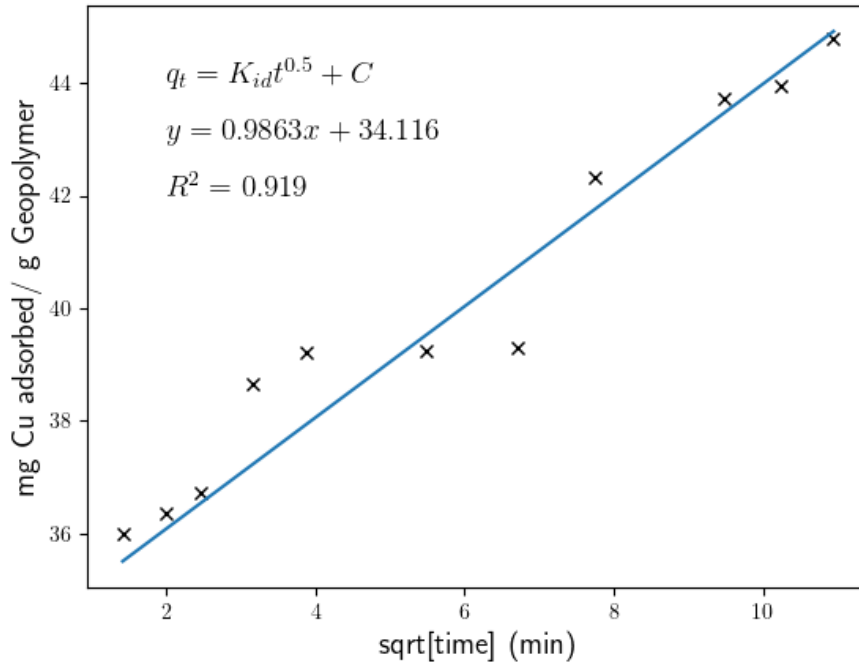


Figure 7. Kinetic result of the Weber-Morris model (intraparticle diffusion model).

3.4. Adsorption isotherms

The results were fitted to the linearized Langmuir and Freundlich models (Equations 7-8 and 9-10, respectively) to clarify the adsorption mechanism.

$$q_e = \frac{k_L C_e q_m}{1 + C_e k_L} \quad (7)$$

$$\frac{C_e}{q_e} = \frac{1}{K_L q_m} + \frac{C_e}{q_m} \quad (8)$$

$$q_e = K_F C_e^{\frac{1}{n}} \quad (9)$$

$$\log(q_e) = \log(K_F) + \frac{1}{n} \log(C_e) \quad (10)$$

Where q_m is the maximum adsorption capacity for the adsorption monolayer formation, n is the adsorption intensity ($0 < 1/n < 1$ for favorable adsorption); K_L ($L \text{ mg}^{-1}$), and K_F ($\text{mg g}^{-1} (L \text{ mg}^{-1})^{1/n}$) are the constants of Langmuir and Freundlich respectively.

The highest and lowest removal efficiencies (from initial concentrations of 20.4, 69.9, 100.3, 129.6 y 160.7 ppm, as measured in the atomic adsorption equipment), were 97.7% and 67.76% for 69.9 and 160.7 ppm, the latter suggesting saturation condition

of the active sites of the geopolymer. Figure 9 presents Freundlich model isotherm. It was found a low correlation value of 0.636. However, for the Langmuir model (see figure 8), the correlation value was 0.995, implying a possible formation of monolayers on the adsorbent surface, with a maximum adsorption capacity of 52.63 mg g⁻¹ and an isotherm constant (K_i) of 0.42.

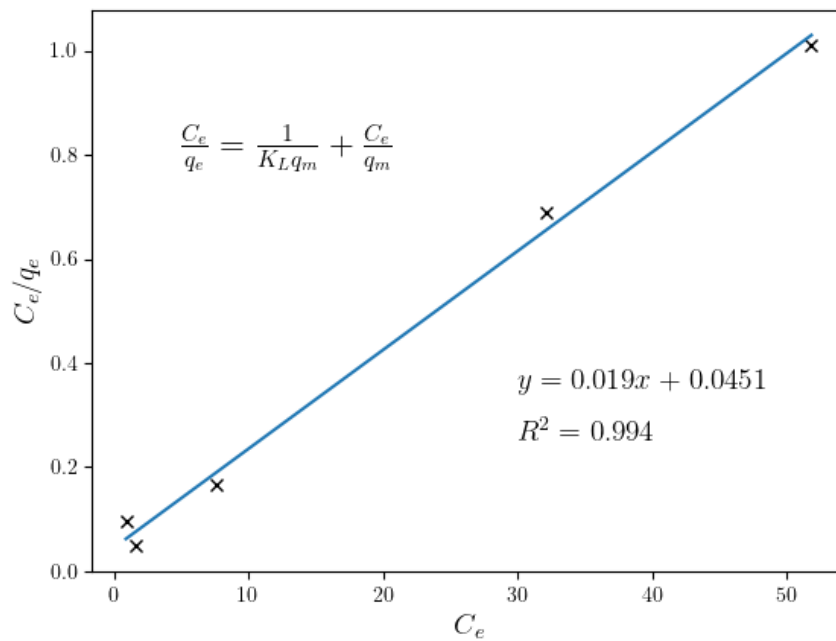


Figure 8. Results of the Langmuir isotherm model. Constant temperature, batch, 2g L-1 dose.

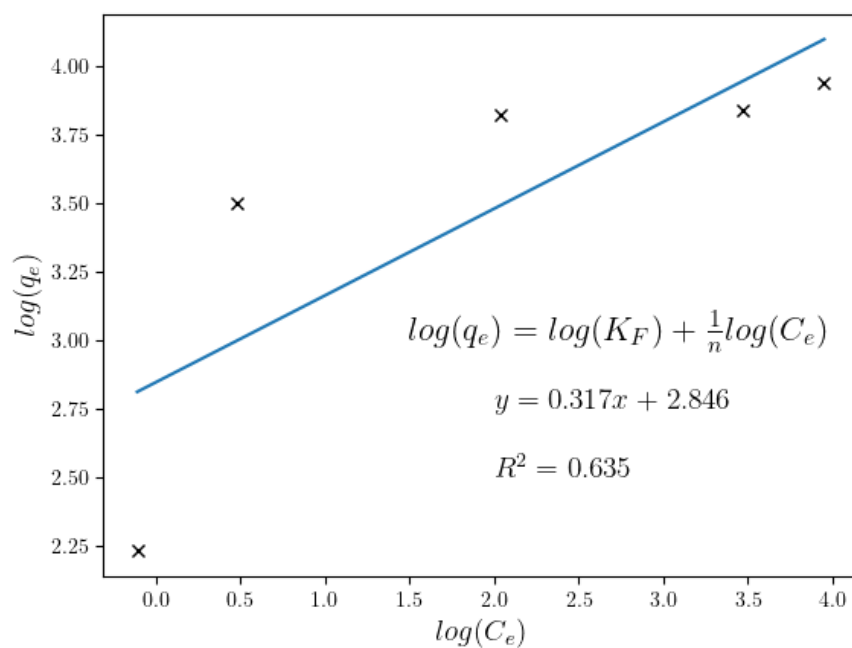


Figure 9. Results of the Freundlich isotherm model. Conditions: Constant temperature, batch, 2g L⁻¹ dose.

Figure 10 represents a comparison of experimental and theoretical Langmuir isotherm model. This result is consistent with the studies of Singhal *et al.* (Singhal et al., 2017) and Cheng *et al.* (Cheng et al., 2012) which demonstrates that using porous geopolymers for copper removal from water follows the Langmuir model.

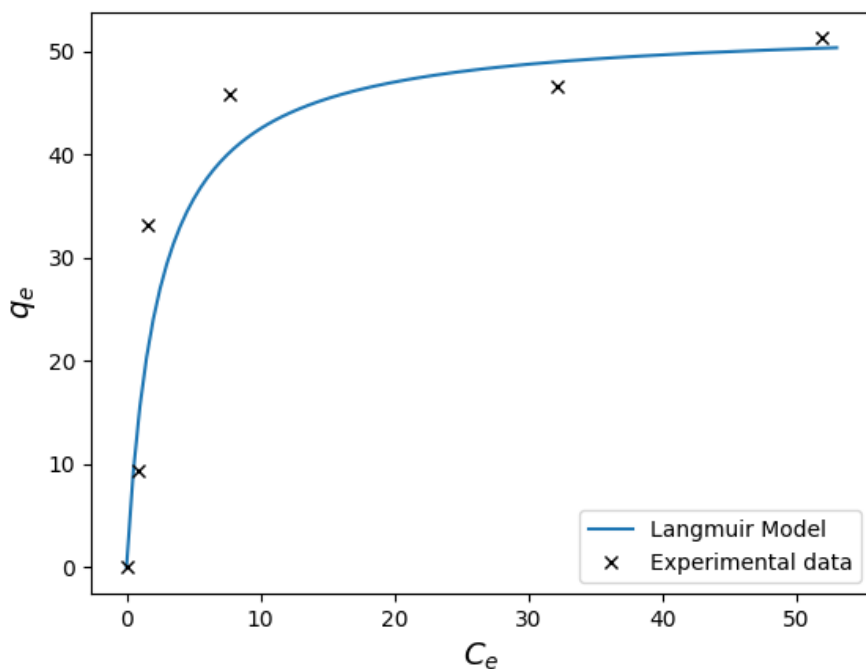


Figure 10. Comparison between experimental data and the Langmuir isotherm

Table 5 demonstrates the compared *the adsorption capacity values for Cu²⁺* adsorption of various studies. Considering adsorption capacity values, the present study shows a competitive adsorption capacity relatively close to that reported by Sudagar *et al.*, (2018), using metakaolin-based *geopolymer* spheres.

Table 5. Comparison of copper adsorption capacity of the geopolymer under study with other studies

Material	Adsorption Capacity (mg g ⁻¹)	Reference
Metakaolin based geopolymer	40.9	(Cheng et al., 2012)

Metakaolin based geopolymer	15	(López et al., 2014)
Metakaolin based geopolymer	44.73	(Andrejkovičová et al., 2016)
Metakaolin based geopolymer	40	(Singhal et al., 2017)
Metakaolin based geopolymer spheres	35	(Tang et al., 2015)
Metakaolin-zeolite based geopolymer	55.92	(Sudagar et al., 2018)
Zeolite based geopolymer	52.63	Present study

Conclusions

This study aims to synthesize Ecuadorian natural zeolite-based geopolymers for a potential industrial application to remove copper from aqueous media. The results indicated that the prepared geopolymer samples with a particle size of less than 60 μm are an efficient adsorbent for copper removal compared to similar studies.

Kinetic study reveals that the Cu^{2+} adsorption on the geopolymers follows a pseudo-second-order linear behavior. Consequently, based on the linear coefficient of determination (R^2), the present study is in good agreement with a sorption process of copper on the zeolite-based geopolymer from a very high concentration. Simultaneously, it obeys the pseudo-second-order kinetics model at the lower initial concentration of the adsorbate.

Adsorption isotherms calculation results fit perfectly with the Langmuir adsorption model.

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