

Electrolytic Conversion of Bicarbonate Solutions to CO at $>500 \text{ mA cm}^{-2}$ and 2.2 V

Zishuai Zhang,¹ Eric W. Lees,² Shaoxuan Ren,¹ Aoxue Huang,¹ and Curtis P. Berlinguette^{*1,2,3,4}

¹Department of Chemistry, The University of British Columbia, 2036 Main Mall, Vancouver, British Columbia, V6T 1Z1, Canada.

²Department of Chemical and Biological Engineering, The University of British Columbia, 2360 East Mall, Vancouver, British Columbia, V6T 1Z3, Canada.

³Stewart Blusson Quantum Matter Institute, The University of British Columbia, 2355 East Mall, Vancouver, British Columbia, V6T 1Z4, Canada.

⁴Canadian Institute for Advanced Research (CIFAR), 661 University Avenue, Toronto, M5G 1M1, Ontario, Canada.

*Corresponding author: Curtis P. Berlinguette (cberling@chem.ubc.ca)

Abstract

Electrolyzers that reduce carbon dioxide (CO_2) into chemicals and fuels often use high-purity gaseous CO_2 feedstocks that need to be isolated from upstream carbon capture units. If CO_2 were to be captured directly from air, the eluent is likely to be an aqueous solution rich in bicarbonate ions (HCO_3^-). This scenario provides the impetus to electrolytically reduce these bicarbonate-rich carbon capture solutions into the same products as a CO_2 electrolyzer. We report here an electrolyzer configuration that couples the conversion of bicarbonate to CO at the cathode with hydrogen oxidation at an anode. This unique system is capable of reaching a commercially-relevant current density of 500 mA cm^{-2} at merely 2.2 V, which is $>0.5 \text{ V}$ more efficient than any other reported electrolyzer that reduces HCO_3^- or CO_2 at these current densities.

The CO₂ reduction reaction (CO₂RR) is a means of using electricity to convert CO₂ into fuels and chemicals¹⁻⁴. A commercial CO₂RR electrolyzer will likely need to operate at current densities (J) greater than 200 mA cm⁻² and cell voltages (V_{cell}) below 3 V⁵⁻⁸. The highest-performing CO₂RR lab-scale electrolyzers are now capable of meeting these criteria when a pure gaseous CO₂ feedstock is used⁹⁻¹⁴. However, CO₂RR electrolyzers must be effectively integrated with upstream carbon capture units (as well as downstream processes) to minimize capital and operational costs. A gaseous CO₂ feedstock will inevitably require CO₂ isolation and compression steps (Fig. 1)^{15,16}. The isolation of CO₂ from air capture streams, for example, requires a series of reactions that require significant energy (e.g., 22.8 MJ to convert 100 mol of K₂CO₃ into CO₂; Fig. 1)¹⁵. The compression of CO₂ (2.0 MJ/100 mol CO₂) not only requires one-sixth the energy required for electrolysis (12.4 MJ/100 mol CO₂), but it also requires significant capital expenditures (\$1–10 million USD/MW)¹⁷. Finally, electrolytic CO₂RR produces OH⁻, which reacts with >70% of consumed CO₂ to form unreactive (bi)carbonates (Eq. 1)¹⁸⁻²⁰. Consequently, <20% of gaseous CO₂ is actually converted to product as it passes through the cathode compartment of a CO₂RR electrolyzer (Fig. 1)²¹.



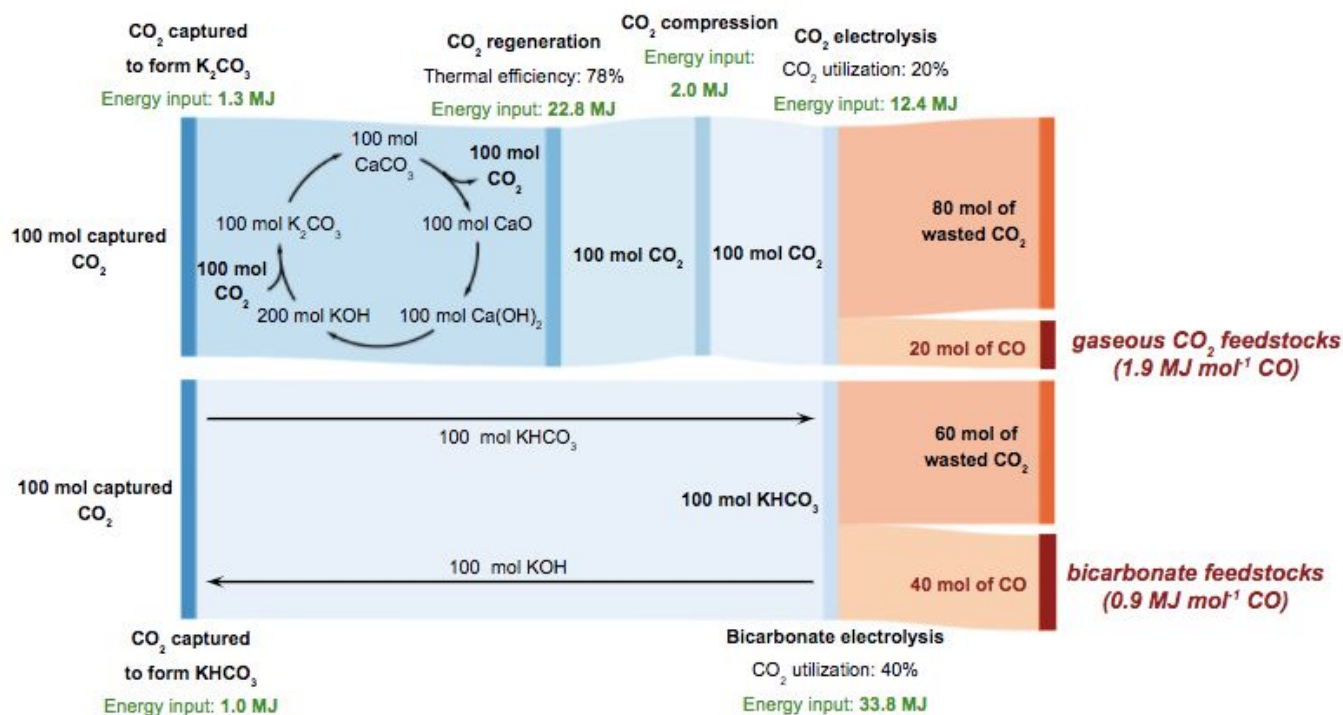


Fig 1. Sankey diagrams illustrating CO₂ mass flows and energy inputs for the capture and conversion of atmospheric CO₂ into CO using electrolysis. The top diagram assumes captured CO₂ is regenerated using a direct air capture process^{15,22}, and that the electrolyzer is fed with a compressed CO_{2(g)} feed ($FE_{CO} = 90\%$; $V_{cell} = 3.0$ V; CO₂ utilization rate = 20%). The bottom panel relies on the electrolysis of KHCO₃, and bypasses the CO₂ regeneration and compression steps ($FE_{CO} = 50\%$; $V_{cell} = 2.2$ V; CO₂ utilization rate = 40%). Energy inputs are sourced from Refs. 15, 22.

We sought to bypass these challenges by developing a CO₂RR electrolyzer that uses a liquid bicarbonate feed instead of gaseous CO₂^{23–26}. The efficient electrolysis of bicarbonate solutions (e.g., KHCO_{3(aq)}), a common eluant of carbon capture units, can form the same CO₂RR products as an electrolyzer fed with gaseous CO₂, but without the need for CO₂ regeneration and pressurization (Fig. 1)²². Bicarbonate electrolyzers are also proven to yield CO₂ utilization values (the fraction of the CO₂ feedstock that is converted into the desired product) >40%; these values are much higher than the 1–20% typically reported for gaseous CO₂-fed electrolyzers^{21,24,27}. The Sankey diagram in Fig 1 illustrates how a bicarbonate electrolyzer with a CO₂ utilization value of 40% makes a carbon product with twice the energy efficiency per mole of captured CO₂ as a gaseous CO₂-fed electrolyzer operating with an

aggressive CO₂ utilization value of 20%. This analysis makes a compelling case for considering the electrolysis of bicarbonate solutions over CO₂ feedstocks.

All reports of bicarbonate electrolysis to date use bipolar membranes (BPMs)^{23,24,26,28–30}. These BPMs deliver H⁺ to the cathode and convert HCO₃[−] into CO₂ (Eq. 2), which is then electrochemically reduced at the cathode^{23,30}. A key challenge in using a BPM is that an applied voltage of >0.83 V is required to dissociate water into OH[−] and H⁺ (Eq. 3)³¹. This voltage penalty makes it challenging to design an electrolyzer capable of operating at an industrially-relevant voltage of <3 V at high rates of product formation (Figs. S1, S2)²⁰.



A significant voltage is also required to drive the oxygen evolution reaction (OER) at the anode (Eq. 4). This reaction provides a source of protons for CO₂RR at the cathode, but the efficiency of the electrolyzer is constrained by the OER accounting for 90% of the equilibrium cell potential. This voltage penalty is seemingly unnecessary because the dioxygen product has little economic value and is usually flared to the environment. One strategy for eliminating this energy penalty is to source protons for the CO₂RR from oxidation reactions that are more thermodynamically favourable than the OER^{32–35}. Consider, for example, that the standard half-cell potential (E^0) for the hydrogen oxidation reaction (HOR; Eq. 5) is merely 0.0 V vs. the reversible hydrogen electrode (RHE) (*c.f.* $E^0 = +1.23$ V vs. RHE for the OER). HOR is widely used at the anode of fuel cells, but there is little precedent for its use in CO₂RR electrolyzers^{36,37}.



We report here a CO₂RR electrolyzer designed to mediate bicarbonate electrolysis at the cathode in tandem with hydrogen oxidation at the anode. This system, which contains a cation exchange membrane (Nafion) that separates the cathode and anode compartments, operates with unprecedented performance parameters: a V_{cell} of 2.2 V (1.4 V after resistance compensation) at a current density of 500 mA cm⁻², and at a CO₂ utilization value of >25%. The lowest voltage (without resistance compensation) previously reported in the literature is >2.8 V at 500 mA/cm² ⁹. This electrolyzer is configured to use the HOR at the anode to form protons, which are then transported through a Nafion membrane to the cathode compartment for reaction with bicarbonate to form CO₂ (Fig. S1). The CO₂ is formed at an electrocatalyst surface, and is therefore positioned to be reduced to form CO₂RR products such as CO.

The title “zero-gap” electrolyzer reported here (denoted “HOR|Nafion|HCO₃⁻” to indicate the anode|membrane|cathode configuration) presses the anode and cathode tightly against opposite faces of a Nafion membrane (25 μm). Flowplates with serpentine channels were used to deliver humidified H₂ gas and 3 M KHCO₃ to the anode and cathode, respectively (Fig. 2a). The gas diffusion electrode (GDE) in the anode chamber consisted of Pt on carbon black, while a silver foam electrode was used in the cathode chamber. This electrolyzer was used to perform electrolysis experiments at applied current densities over a 100 to 1000 mA cm⁻² range. Product formation rates of CO and H₂ from the cathode compartment along with V_{cell} (the full cell voltage measured across the anode and cathode) were recorded over the course of the electrolysis experiments.

Using this reactor architecture, an electrolysis experiment at an applied current density of 100 mA cm⁻² yielded a V_{cell} of 1.7 V. This value represents the lowest V_{cell} ever reported for a zero-gap CO₂RR membrane reactor. When the current density was held at 500 mA cm⁻² for 1 h, the measured V_{cell} was held below 2.2 V for the duration of the experiment (Fig. S2), which also sets a new benchmark for CO₂RR electrolysis (Figs. S3, S4). Importantly, the CO₂ utilization values were measured to be >25% at 500 mA cm⁻².

We benchmarked these V_{cell} values against those obtained with our previously reported bicarbonate electrolyzer. This control system (“OER|BPM|HCO₃⁻”) contains a bipolar membrane (instead of Nafion) and mediates OER at a nickel anode (instead of HOR at a platinum anode). In order to maintain a current density of 100 mA cm⁻², the control system required a V_{cell} of 4.4 V. This value is more than twice as high as our new electrolyzer that performs HOR at the anode. The V_{cell} of the control system spiked to 18 V at 500 mA cm⁻², whereas the V_{cell} of our new electrolyzer was only 2.2 V at the same current density (Fig. 2b). The voltage penalties for water dissociation and the OER render the V_{cell} of the control system impractical for industrially-relevant current densities (i.e., $J > 200$ mA cm⁻²).

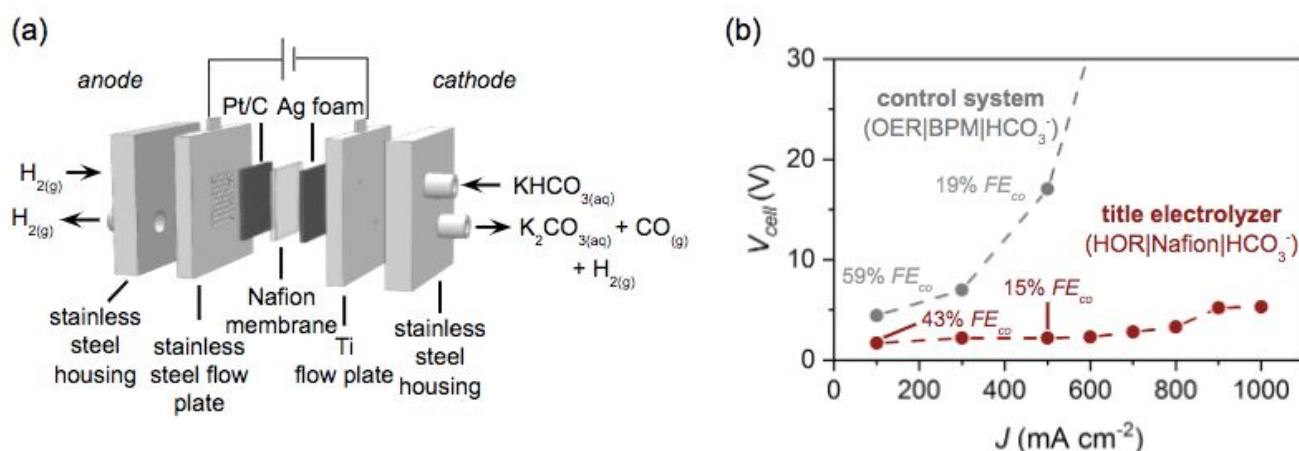


Fig 2. The flow electrolyzer for efficient bicarbonate electrolysis with low full cell voltages. (a) Schematic depiction of the title electrolyzer architecture with the anodic HOR and a Nafion membrane (25 μ m). (b) V_{cell} values measured as a function of current density for the control system and the title electrolyzer with a Nafion membrane (25 μ m).

While the V_{cell} and CO₂ utilization values from our electrolyzer that couples bicarbonate reduction and HOR are state-of-the-art, a major shortcoming of the system is that the measured faradaic efficiencies for CO production (FE_{CO}) were merely 43% at 100 mA cm⁻² (15% at 500 mA cm⁻²; Fig. 2b). We tested thicker Nafion membranes as a means of driving a higher proton flux through the membrane²⁷, but we did not observe any meaningful changes in FE_{CO} values for membrane thicknesses of 25 and 50 μ m. However, we did observe higher FE_{CO} values upon integration of a 500- μ m microfluidic buffer layer between the silver foam cathode and Nafion membrane (Fig. S5)^{13,38}. This buffer layer serves to suppress

hydrogen evolution reaction (HER) by inhibiting H^+ transport from the membrane to the surface of the cathode (Eq. 5)³⁹. Our experiments corroborated this effect, as the FE_{CO} increased from 47% to 71% at an applied current density 100 mA cm^{-2} with the thicker 50- μm membrane (Fig. S5). Notwithstanding, there is a substantial voltage penalty at high current densities when the buffer layer is used (Fig. S6). Electrocatalysts that favor CO₂RR over HER in acidic media will be needed to increase FE_{CO} .

Another feature of our system is that the anode chamber is fed with H_2 gas instead of aqueous media (e.g., NaOH). Consequently, H_2 must be produced by the electrolysis of water or the steam-methane reformation (SMR) of natural gas. Our techno-economic analysis (TEA) shows that the title electrolyzer can produce CO profitably if the price of H_2 gas remains below \$2.3/kg (Fig. S7, see Supplementary Materials for details), a value that is within the current price range of H_2 produced by SMR (i.e., \$1.0-2.4/kg)⁴⁰⁻⁴². Moreover, we calculate that bicarbonate electrolysis coupled with H_2 produced by SMR is carbon-negative if the H_2 utilization value is >32% (See Supplementary Materials for details). We expect H_2 utilization values >70% based on related hydrogen fuel cell studies^{43,44}. There are also opportunities to couple our title electrolyzer to industrial processes (e.g., chlor-alkali process, chlorate production) where H_2 is generated as a waste by-product⁴⁰, and thus $H_{2(g)}$ could be provided at an even lower cost. Finally, we have also contemplated scenarios where $H_{2(g)}$ is recycled to further minimize the cost of using $H_{2(g)}$. Experiments shown in Fig. S8 shows that producing a liquid product (e.g., formate) enables $H_{2(g)}$ produced by HER to be recycled, thereby reducing the amount of virgin H_2 supplied to the system.

We demonstrate here an electrolyzer that mediates the conversion of bicarbonate into CO (or formate) at the CO_2 utilization values >25% at 500 mA cm^{-2} . By sourcing protons from the HOR instead of the OER, this electrolyzer requires merely 2.2 V to drive bicarbonate electrolysis at 500 mA cm^{-2} . Moreover, we show that the FE_{CO} of the electrolyzer can be increased to 71% at 100 mA cm^{-2} by integrating a 500- μm buffer layer between the silver foam cathode and Nafion membrane to slow the competitive HER. With these performance parameters, our TEA shows that this new electrolyzer can

produce CO economically at the market price for H₂ gas. These findings demonstrate a practical method for producing value-added carbon products from bicarbonate solutions with high energy efficiency.

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