

A Universal Porous Adsorbent for the Selective Capture of Carbon Dioxide

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Abstract

Efficient and sustainable methods for carbon dioxide (CO₂) capture are essential. Its atmospheric concentration must be reduced to meet climate change targets, and its removal from sources such as chemical feedstocks is vital. While mature technologies involving chemical reactions that absorb CO₂ exist, they have many drawbacks. Porous materials with void spaces that are complementary in size and electrostatic potential to CO₂ offer an alternative. In these materials, the molecular CO₂ guests are trapped by noncovalent interactions, hence they can be recycled by releasing the CO₂ with a low energy penalty. Capacity and selectivity are the twin challenges for such porous adsorbents. Here, we show how a metal-organic framework, termed MUF-16 (MUF = Massey University Framework), is a universal adsorbent for CO₂ that sequesters large quantities of CO₂ from a broad palette of gas streams with record selectivities over competing gases. The crystallographically-determined position of the CO₂ molecules captured in the framework pores illustrate how complementary noncovalent interactions envelop CO₂ while repelling other guest molecules. The low affinity of the pore environment for other gases underpins the strikingly high selectivity of MUF-16 for CO₂ over methane, nitrogen, hydrogen, acetylene, ethylene, ethane, propylene and propane. Breakthrough gas separations under dynamic conditions benefit from short time lags in the elution of the weakly-adsorbed component to deliver a repertoire of high-purity products. MUF-16 is an inexpensive, robust, recyclable adsorbent that is universally applicable to the removal of CO₂ from sources such as natural gas, syngas, flue gas and chemical feedstocks.

Introduction

Chemical separation processes consume vast quantities of energy. Economical and practical pathways to alleviating this burden are required. This is especially relevant to the capture of CO₂. The release of CO₂ into the atmosphere underlies the greenhouse effect and subsequent temperature increases. There is a pressing need to mitigate CO₂ emissions, which can be achieved using a multifaceted approach involving an overall reduction in energy intensity coupled to the uptake of carbon-free fuels and enhanced CO₂ sequestration techniques. Fossil fuels can be decarbonized by trapping CO₂ from syngas prior to use, and emitted CO₂ can be captured at point sources where its concentration is high.¹ Negative emissions that accrue by capturing CO₂ directly from air are also baked in to most future climate scenarios.² CO₂ must be removed from gas streams in many other situations, for example from natural gas and biogas, and purify valuable hydrocarbons prior to polymerization or chemical derivatization. All of these processes are separations that rely on the selective capture of CO₂ over other gases. The established technology for trapping CO₂ involves chemical reactions with absorbents, typically amines, in solution.³ This incurs multiple drawbacks, including high energy penalties during regeneration, losses due to degradation and evaporation, and the corrosion of hardware and pipelines.⁴

The adsorption of CO₂ in nanoporous materials is an attractive alternative to solution chemisorption.⁵ The weak, noncovalent bonding interactions that underlie physisorption rely on accessible pores that are structured on the molecular scale. They lower the energy requirements for driving off the trapped CO₂ to deliver materials that are sustainable and recyclable. Effective physisorbents combine high uptake, rapid guest diffusion, and long-term stability with selectivity for CO₂ over competing gases at relevant concentrations. In this context, metal-organic frameworks (MOFs) have risen to prominence.⁶⁻⁹ MOF materials are built up from metal ions and organic ligands, and their pore shape, size and chemical environment can be systematically designed. This in turn leads to tailored interactions between framework hosts and molecular guests. For example, the Ni-(4-pyridylcarboxylate)₂ framework is able to capture large quantities of CO₂ and exhibits an appreciable selectivity for CO₂ over H₂ at high pressures. This makes it amenable to the purification of syngas.¹⁰ While natural gas and biogas are primarily composed of methane (at high pressure and low pressure, respectively), contamination by CO₂ can be considerable and cause pipeline corrosion and dry ice formation. MOFs such as SIFSIX-14-Cu-I and NbOFFIVE-1-Ni, however, offer a means of significantly reducing the CO₂ concentration in the presence of dominant quantities of methane.^{6,11,12} Designing analogues of these MOFs by changing the metal ion or altering the interpenetration level has dramatic consequences for their adsorption behaviour.¹³ Despite these advances, challenges remain in identifying MOF adsorbents that combine a good separation performance with the other requisite characteristics. For example, Mg-MOF-74 is distinguished by its high CO₂ uptake, but this arises from a high density of open metal sites that are irreversibly blocked by traces of water vapour and oxygen.¹⁴ Impregnation of the material with amines improves the stability and selectivity of the material, but high temperatures are required to recycle the material by CO₂ desorption.¹⁵

The recent surge of interest in porous frameworks has largely focussed on the separation of specific gas pairs.^{6,8} However, a truly universal adsorbent that can capture CO₂ from a diverse array of gas streams with various compositions and operating pressures is yet to emerge. Such a material would have many advantages, such as economies of scale in manufacturing, well understood adsorption metrics, industry acceptance, and facile deployment. Traditional adsorbents such as zeolites, silica gel and activated carbon approach this kind of universality for other gases, which highlights the opportunities for next-generation materials with improved selectivities and physicochemical characteristics.

Inspired by the superb properties of MOFs derived from straightforward and readily-available linkers,^{16,17} we sought to develop an adsorbent that could efficiently trap CO₂. Our interest was captured by the MUF-16 (MUF = Massey University Framework) series of materials. These frameworks are prepared simply by combining 5-aminoisophthalic acid (H₂aip), an inexpensive, commercially-available linker, with cobalt(II), nickel(II), or manganese(II) salts in alcoholic solvent (Figure 2a). This delivers a family of compounds with the general formula [M(Haip)₂],^{18,19} referred to as MUF-16 (M =Co), MUF-16(Ni) and MUF-16(Mn), respectively. These crystalline materials are high yielding on multi-gram scales and tolerant to typical laboratory atmospheres. Their crystal structures were determined by single crystal X-ray diffraction (Table S4). The three frameworks are isostructural, belonging to the *I*2/a space group. Individually, the metal ions adopt an octahedral geometry with four carboxylate and two amino donors, arranged *trans* to one another, from six different Haip ligands. These ions are aligned into one-dimensional chains along the crystallographic *b* axis supported on each side by μ_2 -bridging carboxylate groups (Figure 1b). Adjacent chains are connected into two-dimensional sheets by Haip ligands that extend across the *bc* plane by coordinating to the metal centres with both their amino and carboxylate donors (Figure 1b). Only one of the two carboxyl groups of each Haip ligand coordinates to the metal. The other remains protonated and engages in hydrogen-bonding with a partner extending from an adjacent layer (Figure 1c). These interactions link the layers into three-dimensional frameworks. The frameworks support one-dimensional channels running along a crystallographic axis with dimensions of approximately 3.3 × 6.5 Å (Figure 1d). In their as-synthesized form the pores contain occluded water, which can be easily removed by heating *in vacuo*.

MUF-16 frameworks are obtained in high purity, as established by both elemental analysis and the match between the powder X-ray diffraction patterns recorded on bulk material and those simulated from the single-crystal X-ray diffraction structures (Figure S7). Thermogravimetric analysis demonstrated their thermal stability beyond 330 °C under nitrogen (Figure S4). The frameworks are chemically robust, being unaffected by soaking in water or exposure to air for prolonged periods, as confirmed by powder X-ray diffraction and gas adsorption analysis (*vide infra*).

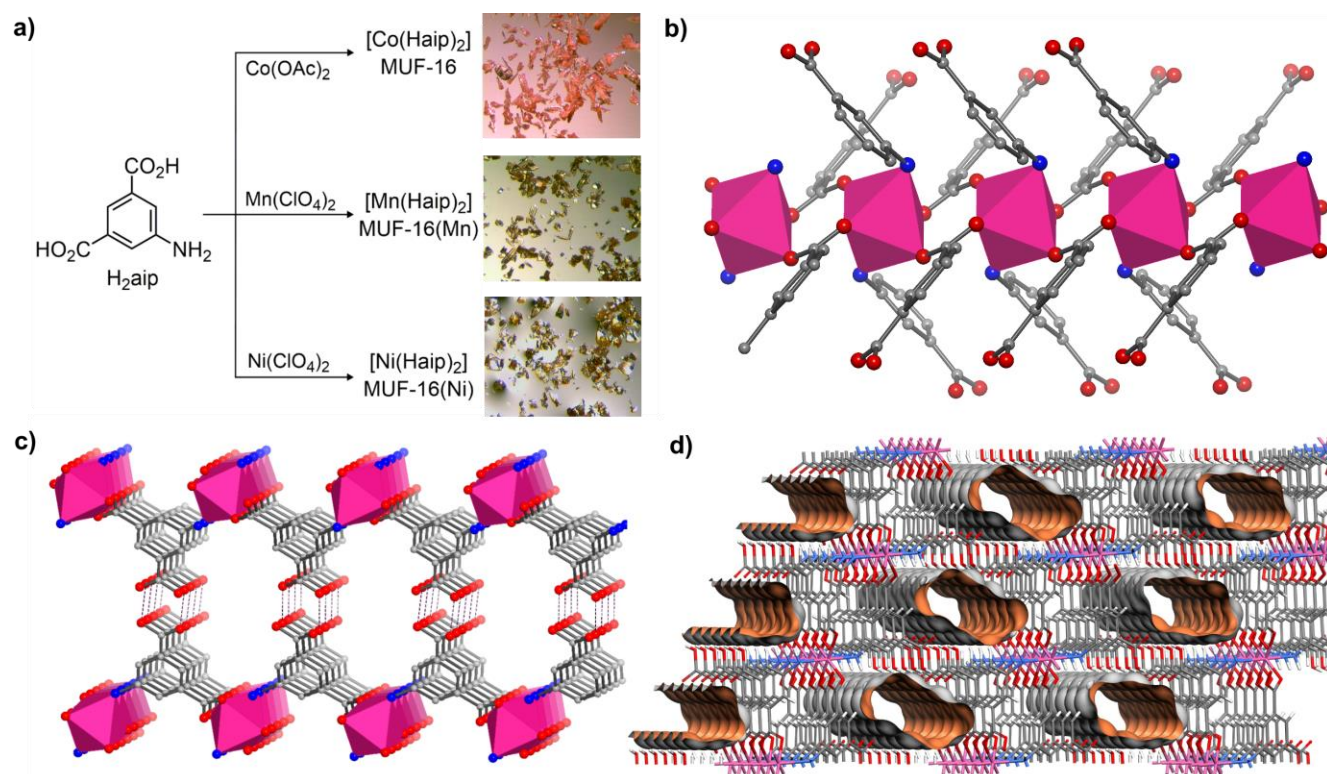


Figure 1. (a) Synthetic routes to the MUF-16 family and optical micrographs of the reaction products. (b) Infinite secondary building units (iSBUs) in MUF-16 comprise one-dimensional cobalt(II) chains connected by μ_2 -bridging carboxylate groups of the Haip ligands (H_2aip = 5-aminoisophthalic acid).

The cobalt(II) ions are depicted as filled octahedra. (c) The iSBUs are linked into planar two-dimensional sheets by the Haip ligands and further connected into a three-dimensional framework by hydrogen bonding (depicted as dashed lines) between adjacent sheets. (d) MUF-16 features one-dimensional channels that propagate through the framework. The Connolly surface of the framework is shown in orange and defined with a probe of diameter 1.0 Å. Colour code: cobalt = magenta; oxygen = red; carbon = grey; hydrogen (where shown) = white.

As suggested by SCXRD, the MUF-16 frameworks are accessible to a range of incoming gases. Activation to give permanently porous materials is straightforward, and nitrogen adsorption isotherms measured at 77 K gave BET surface areas of 215, 209 and 238 m^2/g for MUF-16, MUF-16(Mn), and MUF-16(Ni), respectively (Figures S18-S20). Total pore volumes of 0.11 cm^3/g were measured for all three frameworks (Table S1). These values are comparable with the geometric surface areas and pore volumes calculated from the crystallographic coordinates. CO_2 adsorption isotherms were collected at 293 K (Figure 2a). These isotherms rise steeply at low pressures and nearly plateau towards 1 bar, which indicates a strong affinity of the frameworks for the CO_2 guests. The capacities of these materials to host CO_2 is considerable: both MUF-16 and MUF-16(Ni) take up 2.13 mmol/g (48 cm^3/g) at 1 bar, and MUF-16(Mn) adsorbs 2.25 mmol/g (50.5 cm^3/g). This equates to approximately 0.9 molecules of CO_2 per metal site (Table S6). Since the framework pores are nearly saturated at 293 K and 1 bar, CO_2 uptake is only marginally higher at 273 K (Figure S11). The isosteric heat of adsorption (Q_{st}) at zero-coverage was calculated to be around 33 - 37 kJ/mol (Figure 2b). The Q_{st} increases at higher loadings, which can be attributed to intermolecular interactions between the adsorbates when the framework pores approach saturation. These interactions were experimentally verified by SCXRD (*vide infra*). Since Q_{st} values

remain moderate even at high CO₂ loading, and well below values observed for MOFs with open metal sites, the energy required to regenerate the frameworks by CO₂ desorption is likely to be low. Furthermore, the risk of irreversible poisoning by traces of pernicious contaminants is minor.

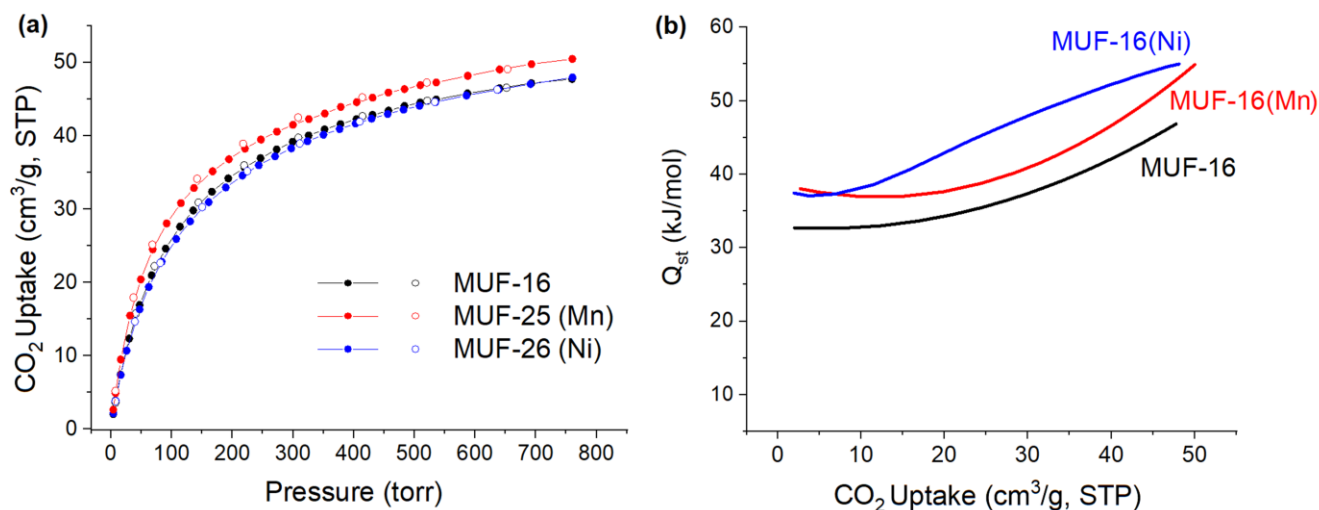


Figure 2. (a) Volumetric adsorption (filled circles) and desorption (open circles) isotherms of CO₂ measured at 293 K and for MUF-16 (black), MUF-16(Mn) (red), and MUF-16(Ni) (blue). (b) Heats of adsorption (Q_{st}) calculated for CO₂ binding to MUF-16 (black), MUF-16(Mn) (red), and MUF-16(Ni) (blue) as a function of CO₂ uptake. A high affinity for CO₂ coupled to a moderate heat of adsorption promise an adsorbent that takes up significant quantities of gas yet is easily recycled.

Single-crystal X-ray diffraction was used to identify the CO₂ binding sites in these frameworks. MUF-16(Mn) was selected for this study since its darker colour streamlined crystal handling, but the results are applicable to the other members of the MUF-16 family. After transferring a MUF-16(Mn) single crystal into a capillary, it was activated *in vacuo* and the capillary flame-sealed. This allowed the guest-free structure of MUF-16(Mn) to be crystallographically determined under a vacuum (Table S5). We then filled CO₂ into the capillary to a pressure of 1.1 bar to determine the structure of the CO₂-loaded framework. We noted only minor changes to the framework itself upon either evacuation or filling with CO₂. A clear picture of the affinity of MUF-16 for CO₂ was revealed by the CO₂-loaded SCXRD structure. First, the dimensions of the framework pores match the size of the CO₂ molecules, which allows these guests to be enveloped by multiple non-covalent contacts (Figure 3a). Second, these contacts are favourable since the electric quadrupole of the CO₂ is complementary to the polarization of the MUF-16 pore surface. For example, one of the electronegative oxygen atoms of the CO₂ molecule engages in N-H...O and C-H...O interactions with hydrogen atoms of amino and phenyl groups at distances of 2.55 and 2.81 Å, respectively. Similarly, the electropositive carbon atom of the CO₂ molecule contacts an oxygen atom of a non-coordinated carboxylate group with a distance of 2.87 Å. Two sites, which are related by crystallographic symmetry and share a common location for one of the oxygen atoms, are available to the CO₂ guests. They are occupied with a 50/50 ratio to give one CO₂ molecule per Mn centre overall. The CO₂ guest molecules are aligned along the pore axis in a tilted

fashion (Figure 3b). These arrays take advantage of short attractive $\text{C}\cdots\text{O}$ intermolecular interactions between adjacent molecules at 3.78 Å, which underlie the observed increase in Q_{st} as a function of gas loading observed in the adsorption isotherms.

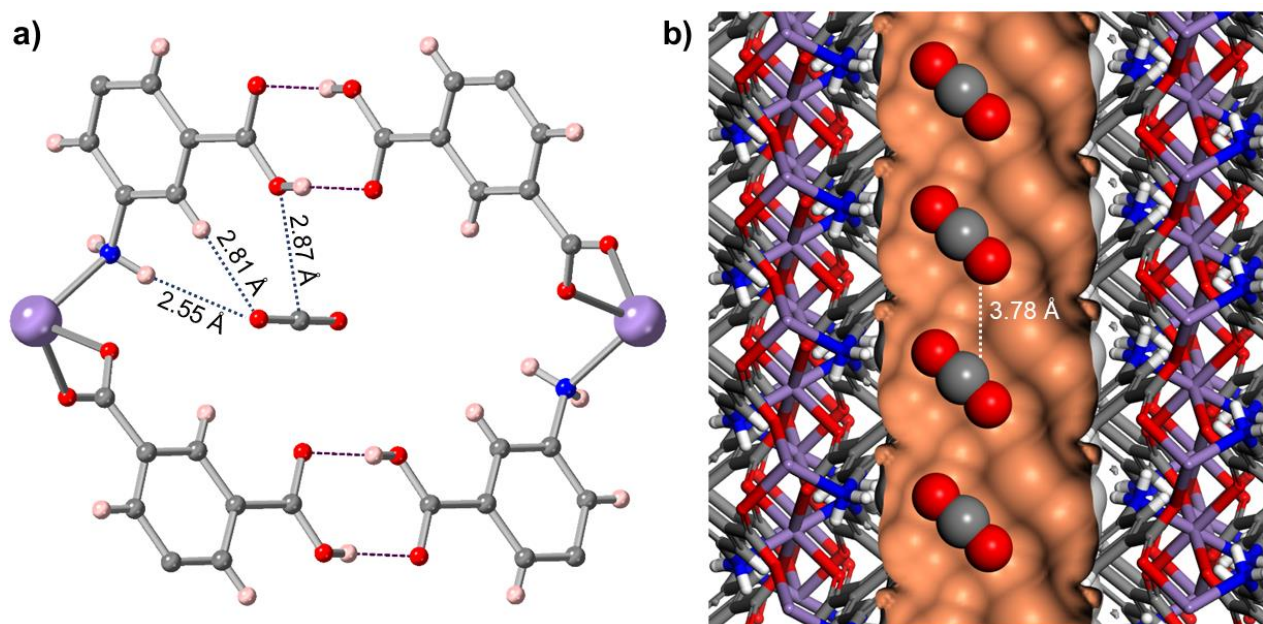


Figure 3. (a) The adsorption sites of CO_2 molecules in the pores MUF-16(Mn) as determined by single-crystal X-ray diffraction. A view down the long axis of the channel is depicted. A second, symmetry-equivalent CO_2 adsorption site is present. (b) Arrays of adsorbed CO_2 molecules observed in the channels of MUF-16(Mn) highlighting potential attractive noncovalent interactions between adjacent guests. The CO_2 molecules in are shown in representative orientations that correspond to one of the two symmetry-related crystallographic orientations. Colour code: manganese = light purple; nitrogen = blue; oxygen = red; carbon = grey; hydrogen = white; pore Connolly surface = orange.

Selectivity of MUF-16 for CO_2 and gas separations

The high uptake of CO_2 by MUF-16 stands in contrast to other gases. Adsorption isotherms of H_2 , Ar, N_2 , CH_4 , O_2 , C_2H_2 , C_2H_4 , C_2H_6 , C_3H_6 and C_3H_8 were measured on MUF-16 at 293 K.²⁰ Only modest quantities of these gases are adsorbed, and care was taken to ensure the accuracy of these measurements (Figure 4a and Table S1). For example, MUF-16 takes up just 1.32 and 1.20 cm^3/g of N_2 and CH_4 at 1 bar and 293 K, respectively, which rises to the highest value amongst the measured adsorbates of 5.35 cm^3/g for C_3H_6 . While the low uptake of the monatomic and diatomic gases is a well-established function of their small polarizabilities and small (or zero) quadrupole moments, the diminished affinity for the larger hydrocarbon guests is notable. Electropositive regions around their termini (Figure S1) leads to repulsive interactions with the framework pore surface, as illustrated by the hypothetical loading of C_2H_2 in MUF-16 (Figure S2).

The observed uptake ratios for CO_2/N_2 , CO_2/CH_4 and CO_2/H_2 are 36.2, 39.8 and 74.6, respectively, at 293 K and 1 bar. The preferential uptake of CO_2 over N_2 is comparable to the benchmark physisorbent $[\text{Cd}_2\text{L}(\text{H}_2\text{O})]^{21}$ (36.3), and elevated beyond materials such as SIFSIX-2-Cu-i (34),²² DICRO-3-Ni-i (20),²³ and zeolite 13X (18.7) (Table S10). While some materials that trap CO_2 by chemisorption show

higher uptake ratios, including amine-functionalised frameworks en-Mg-dobpdc (47),¹⁵ mmen-Cu-BTtri (38.3)²⁴ and Mg-mmen-dobpdc (36.7),²⁵ they require significant energy input to desorb the captured CO₂. With respect to CO₂/CH₄, the uptake ratio of MUF-16 is comparable to that of [Cd₂L(H₂O)] (42.9),²¹ and is exceeded by only one other reported material (SIFSIX-14-Cu-i, 116).²⁶

MUF-16 adsorbs more CO₂ than C₂ and C₃ hydrocarbons with uptake ratios of between 9.0 and 15.9 at 293 K and 1 bar (Table 1). This contrasts with typical physisorbents, which show a preference for unsaturated hydrocarbons especially when bonding between the guest's π electrons and open metal sites can occur.²⁷⁻³⁴ The inverted selectivity for CO₂ over C₂ and C₃ hydrocarbons exhibited by MUF-16 has seldom been reported,³⁴⁻⁴² and, to the best of our knowledge, there are not any MOFs reported in the literature that preferentially adsorb CO₂ with this degree of generality. It is notable that energy efficiency gains may stem from MUF-16 since high-purity hydrocarbon products can be obtained in a single step by capturing CO₂ from crude gas streams. On the other hand, hydrocarbon-selective MOFs require additional processing and purification since CO₂ is co-adsorbed by the adsorbent.^{34,43,44} MUF-16 has a particularly high affinity for CO₂ relative to C₂H₂, which is elevated beyond earlier reported CO₂-selective materials including SIFSIX-3-Ni (1.2 at 298 K and 0.1 bar)³⁴, CD-MOF (1.3 at 298 K and 1 bar)⁴², K₂[Cr₃O(OOCH)₆(4-ethylpyridine)₃]₂[α -SiW₁₂O₄₀] (4.5 at 278 K and 1 bar)³⁸ and [Mn(bdc)(dpe)] (6.4 at 273 K and 1 bar)³⁹ (Table S11).

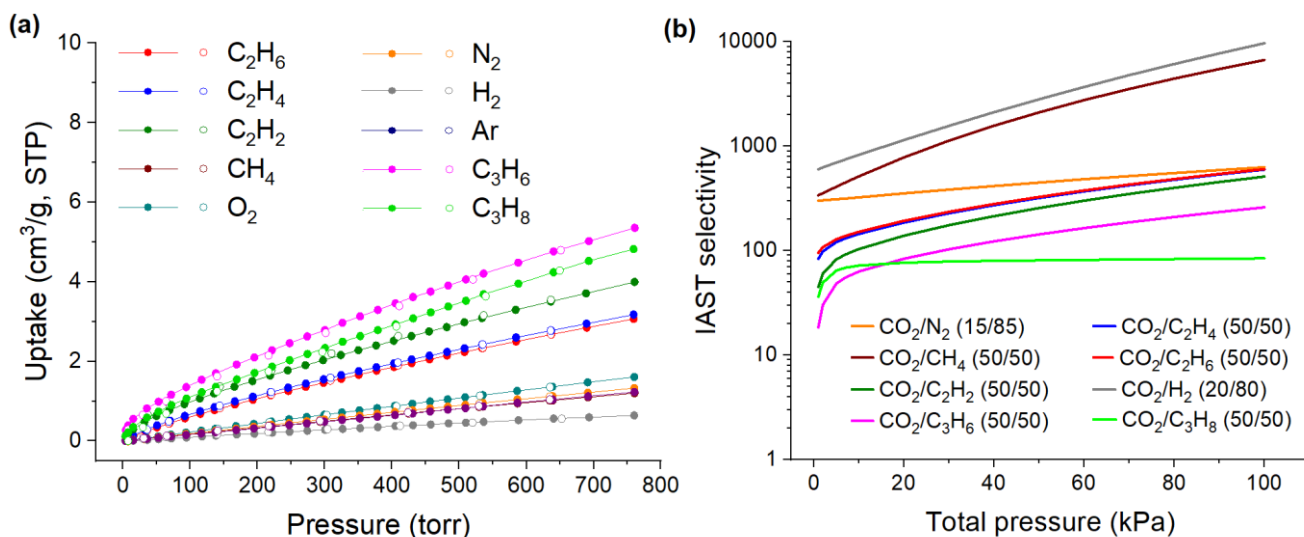


Figure 4. (a) Experimental H₂, Ar, N₂, CH₄, O₂, C₂H₂, C₂H₄, C₂H₆, C₃H₆ and C₃H₈ adsorption (solid spheres) and desorption (open spheres) isotherms of MUF-16 measured at 293 K. (b) Predicted IAST selectivities, displayed with a log scale, of MUF-16 for various gas mixtures at 293 K.

Table 1. Summary of gas adsorption data and IAST-calculated selectivities for the MUF-16 family at 1 bar and 293 K.

	Gas(es)	MUF-16	MUF-16(Mn)	MUF-16(Ni)
Uptake ^a	CO ₂	47.78	50.5	47.97
	N ₂	1.32	2.86	2.30
	CH ₄	1.20	3.10	2.77
	H ₂	0.64	1.10	0.78
	C ₂ H ₂	3.99	9.69	7.53
	C ₂ H ₄	3.17	8.31	5.42
	C ₂ H ₆	3.06	8.81	5.67
	C ₃ H ₆	5.35	-	-
	C ₃ H ₈	4.82	-	-
Selectivity	CO ₂ /N ₂ ^b	630	260	280
	CO ₂ /CH ₄ ^c	6690	470	1220
	CO ₂ /H ₂ ^d	9690	300	6830
	CO ₂ /C ₂ H ₂ ^c	510	31	46
	CO ₂ /C ₂ H ₄ ^c	600	150	130
	CO ₂ /C ₂ H ₆ ^c	600	55	110
	CO ₂ /C ₃ H ₆ ^c	260	-	-
	CO ₂ /C ₃ H ₈ ^c	84	-	-

^a In cm³/g. ^b 15/85 ratio at 1 bar and 293 K as calculated by IAST. ^c 50/50 ratio at 1 bar and 293 K as calculated by IAST. ^d 20/80 ratio at 1 bar and 293 K as calculated by IAST.

While uptake ratios provide an excellent indication of preferential affinity, the selectivity for a particular component of a gas mixture can be quantified by Ideal Adsorbed Solution Theory (IAST) calculations. At 293 K and 1 bar, the IAST selectivity of MUF-16 for CO₂ in the presence of N₂ (15/85 CO₂/N₂ mixture) is 630 (Figure 4b). This exceptional preference for CO₂ surpasses the majority of reported materials and positions MUF-16 as a remarkably good adsorbent for this key separation (Figure 5 and Table S10). For 50/50 CO₂/CH₄ mixtures, the IAST selectivity of MUF-16 is 6690, which represents a new selectivity benchmark (Figures 4b and 5, Tables 1 and S10). Similarly high selectivities were calculated for the separation of CO₂ and H₂. For equimolar mixtures of CO₂ and C2 hydrocarbons, the IAST-calculated selectivities range between 510 and 600 at 293 K and 1 bar (Figure 4b, Table 1). MUF-16 thus marks a significant new yardstick for separating CO₂ from these gases, which is a difficult and relevant challenge. The substantial improvements compared with previously-reported materials in the case of acetylene are highlighted in Figure 5 (see also Table S11). Further, MUF-16 efficiently captures CO₂ from both propane and propylene (Figure 4b, Table 1).

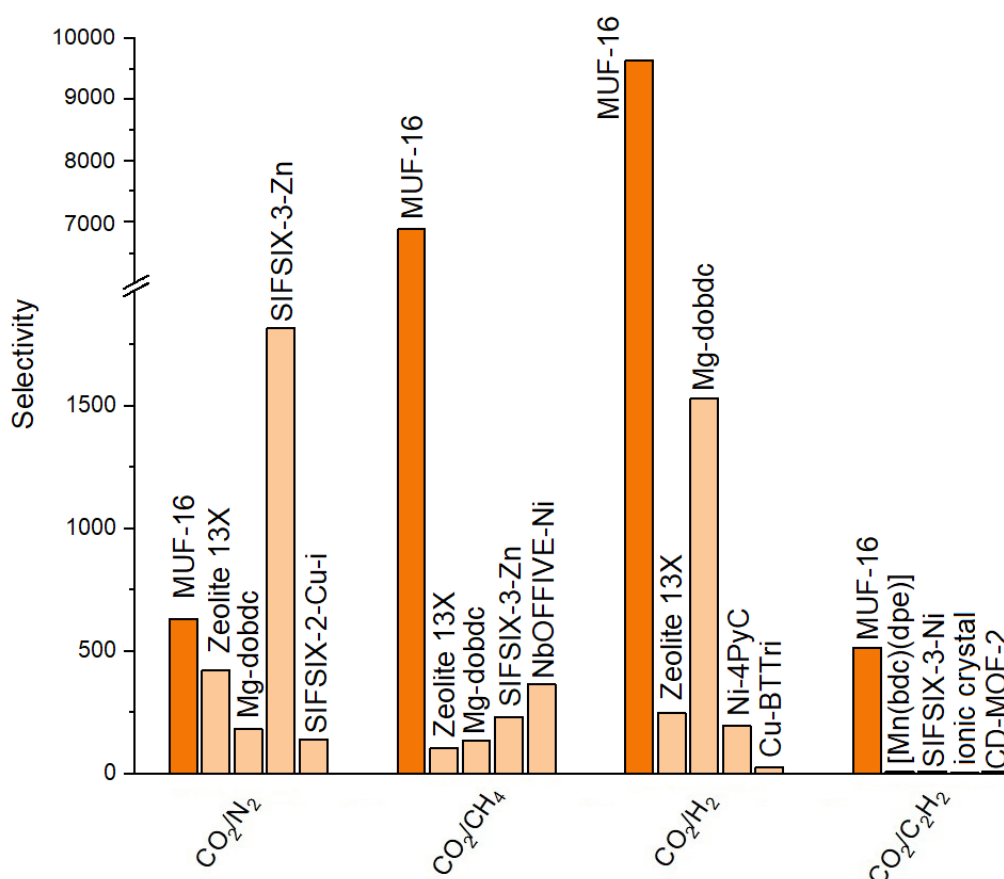


Figure 5. IAST selectivity of MUF-16 in comparison to top-performing physisorbents for CO_2/N_2 (15/85), CO_2/CH_4 (15/85), CO_2/H_2 (20/80) and $\text{CO}_2/\text{C}_2\text{H}_2$ (50/50) mixtures at ambient temperature and 1 bar. For clarity, the y axis is broken in two parts with different scales. The formula of the ‘ionic crystal’ is $\text{K}_2[\text{Cr}_3\text{O}(\text{OOCH})_6(4\text{-ethylpyridine})_3]_2[\alpha\text{-SiW}_{12}\text{O}_{40}]$.

While the pore characteristics of MUF-16 clearly favour the uptake of CO_2 over other gases, its selectivity mechanism could potentially rely on molecular sieving if the larger adsorbates are excluded from the framework on the basis of their size. This was ruled out by measuring gas adsorption isotherms at 195 K, which revealed that MUF-16 is able to take up significant amounts of C_2H_6 (Figure S14). Thus, these molecules can freely enter the pore network of MUF-16 but their interactions with the framework are weak so their uptake is low at ambient temperatures. Further, the kinetics of adsorption of several guest molecules were measured (Figure S15). All gases reach their equilibrium uptake in well under one minute and the uptake rates are similar for all gases. Therefore, thermodynamic – rather than kinetic – effects have the most decisive impact on the differential affinity of these gases for MUF-16.

Next, we applied MUF-16 to the separation of gas mixtures under dynamic conditions using an adsorption bed. While the IAST calculations indicated that MUF-16 has impressive separation capabilities, experimental data from breakthrough measurements yield data under real operating conditions. We initially focussed on the separation of CO_2 and N_2 , and employed gas feeds with 50/50, 15/85, 1/99 and 0.4/99.6 compositions. MUF-16 efficiently retained CO_2 and delivered pure N_2 with a short time lag in all four cases even with low amounts of CO_2 in the mixture (Figures 6a and S52-S54).

The dynamic capacities of MUF-16 for CO₂ derived from these breakthrough measurements (up to 1.57 mmol/g) are nearly identical to the equilibrium capacities at the corresponding partial pressures (Table S7). This indicates that MUF-16 is an excellent adsorbent under dynamic conditions, which stems from a combination of (i) differential affinity for the two gases, (ii) the short time delay for the appearance of the non-adsorbed N₂ and its near-vertical elution profile. This implies that intra- and intercrystalline gas diffusion in the adsorption bed is unimpeded.

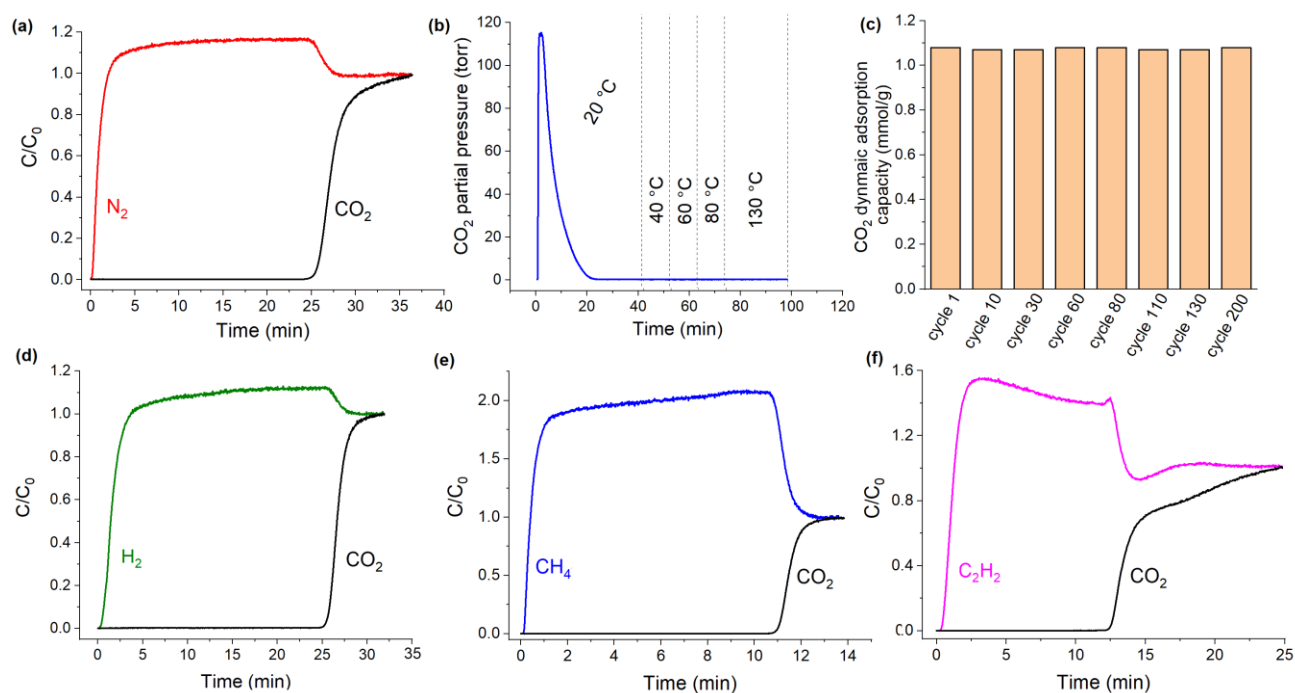


Figure 6. Experimental breakthrough curves for a (a) 15/85 mixture of CO₂/N₂ at 293 K and 1.1 bar in an adsorption column packed with MUF-16. (b) CO₂ concentration profile during regeneration with dry air at flowrates of 20 mL_N/min at 1.1 bar. All of the CO₂ was removed at 20 °C over a period of around 25 minutes, with no further loss of CO₂ observed at 40, 60, 80 or 130 °C. (c) The CO₂ dynamic adsorption capacity of MUF-16 obtained from the repeated breakthrough separation of CO₂/N₂ (15/85) followed by adsorbent regeneration. A total of 200 breakthrough cycles were measured. Experimental breakthrough curves for (d) a 15/85 mixture of CO₂/H₂ (e) a 50/50 mixture of CO₂/CH₄ and (f) a 50/50 mixture of CO₂/C₂H₂.

MUF-16 can be fully regenerated and recycled for CO₂ capture. Complete CO₂ desorption was achieved by placing it under a dynamic vacuum or by purging with a flow of dry air (CO₂ content <200 ppm) at room temperature and 1 bar. The CO₂ profile in the eluent from the adsorption bed was measured to show the CO₂ is released within 25 minutes (Figure 6b). No further loss of CO₂ was observed upon heating. Regenerating MUF-16 is simpler than typical adsorbents,⁴⁵ which is advantageous from energy efficiency and economic standpoints. The recyclability of MUF-16 was then established by more than 200 breakthrough-regeneration cycles for the separation of CO₂/N₂ (Figure 6c). In line with its high stability, MUF-16 maintains its separation performance and uptake capacity over this period. With a raw materials cost of less than \$29 USD per kilogram, MUF-16 presents a sustainable and economical

solution to CO₂ capture. As an additional measure to render MUF-16 more compatible with typical large-scale gas separation processes, we combined MUF-16 with a small quantity of polyvinylidene fluoride (PVDF) to make composite pellets (Figure S74). The PXRD pattern (Figure S75) and CO₂ adsorption isotherm (Figure S76) of these easily-handled granules exhibit the same profile as MUF-16, indicating that the structure and gas adsorption characteristics are unchanged. Furthermore, the pellets maintain their CO₂/N₂ separation performance even after boiling in water (Figure S77).

Invigorated by these results, we applied MUF-16 to the separation of other gas mixtures where its low affinity non-CO₂ gas components translates into rapid separations and high dynamic selectivities. While only a few nanoporous materials have been reported for the stripping of CO₂ from H₂/CO₂ feedstocks,^{46,47} as required during the purification of syngas, this has been identified as a high priority.^{48,49} In this light, we conducted breakthrough studies for a 15/85 mixture of CO₂/H₂ at 293 K and 1.1 bar to show that MUF-16 is able to efficiently separate CO₂ from H₂. CO₂ was retained on the MUF-16 bed while the H₂ component eluted immediately in a high purity stream (Figure 6d). Experimental breakthrough curves for gas compositions involving methane, ethane and propane were also measured with feed compositions of CO₂/CH₄ (50/50, 15/85) and CO₂/CH₄/C₂H₆/C₃H₈ (15/80/4/1). We observed complete CO₂ capture by MUF-16, whereby CH₄, C₂H₆ and C₃H₈ broke through quickly with steep elution profiles (Figures 6e and S58). The dynamic uptake capacity of CO₂ obtained from these breakthrough curves equates to 1.53 and 1.13 mmol/g, which is nearly identical to the equilibrium capacity at the relevant partial pressures of CO₂ (Table S7). These results demonstrate that the presence of the heavier adsorbates C₂H₆ and C₃H₈ does not impede the CO₂ capture capabilities of MUF-16. This is an important observation for the removal of CO₂ from both biogas and natural gas.⁵⁰ To further demonstrate its applicability to natural gas sweetening, we conducted breakthrough measurements at higher pressure (9 bar), and observed that CO₂ was cleanly removed from the gas stream (Figures S59-S60). The dynamic uptake capacity for CO₂ is higher than that measured at 1 bar. Extrapolation of these data to pressures relevant to natural gas processing (~40-60 bar) predicts that MUF-16 can efficiently sequester CO₂ from raw natural gas streams (Figure S64).

To test the ability of MUF-16 to separate CO₂ from C₂ hydrocarbons in a dynamic process, individual breakthrough curves for CO₂/C₂H₆ (50/50), CO₂/C₂H₄ (50/50) and CO₂/C₂H₂ (50/50 and 5/95) mixtures were measured at 293 K and 1.1 bar. Complete separation was realized, and the C₂ hydrocarbons were delivered in a single, direct adsorption step with a dynamic adsorption capacity for CO₂ of around 1.22 mmol/g (Figures 6f and S65-S67, Table S7). This underscores the advantages conferred by the inverted selectivity of MUF-16 for producing high-value gases. The productivity of MUF-16 is high, with 1 kg producing 27 L of the C₂ hydrocarbons from an equimolar mixture at 293 K and 1 bar. Extending these experimental results with simulated breakthrough profiles demonstrated that MUF-16 is capable of eliminating trace quantities of CO₂ from C₂H₂ to produce a stream of high-purity C₂H₂ (Figure S70), which elutes after only a short time lag. In literature reports to date, the capture of

CO₂ over C₂ hydrocarbons has so far largely been restricted to cryogenic temperatures and/or static conditions.³⁵⁻⁴⁰ With respect to CO₂/C₂H₂ mixtures at ambient temperatures, we are aware of only three reported materials, CD-MOF-1⁴², CD-MOF-2⁴² and SIFSIX-3-Ni,³⁴ for which inverse CO₂ trapping has been verified by experimental breakthrough measurements. Since these MOFs adsorb C₂H₂ strongly at moderate pressures (in addition to CO₂), their uptake ratios are modest, however, and they are limited to very low partial pressures of CO₂ and suffer from low productivity. In contrast, MUF-16 operates efficiently across range of CO₂/C₂H₂ mixtures and benefits from near-total rejection of C₂H₂ from the framework pores.

MUF-16 is a nanoporous adsorbent with universal selectivity for CO₂. It combines attractive noncovalent contacts between guest CO₂ molecules and the pore surface with rapid diffusion kinetics, robustness and recyclability. The selectivity of MUF-16 for CO₂ is elevated beyond conventional materials and relevant to contexts as diverse as natural gas, syngas and chemical feedstocks. As a low-cost material with broad applicability and abundant technical and practical advantages, MUF-16 has the potential to be deployed universally for the capture of CO₂ using pressure- or temperature-swing adsorption processes.

Acknowledgements

We are grateful to the MacDiarmid Institute for Advanced Materials and Nanotechnology and the RSNZ Marsden Fund for financial support. The data reported in the paper are presented in the supplementary information. Crystal structures of MUF-16 family collected at pristine form, under vacuum and loaded with CO₂ are available free of charge from the Cambridge Crystallographic Data Centre under reference nos. CCDC 1948901-1948905. A provisional patent has been filed with IP Australia (Application number 2018904882).

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Electronic Supplementary Information for:

A Universal Porous Adsorbent for the Selective Capture of

Carbon Dioxide

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1. General procedures and information

All starting compounds and solvents were used as received from commercial sources without further purification unless otherwise noted. Elemental analyses were performed by the Campbell Microanalytical Laboratory at the University of Otago, New Zealand.

Single crystal structures of MUF-16, MUF-16(Mn) and MUF-16(Ni) were used directly for all the calculations and simulations without modification. The Zeo++¹ code and RASPA2² were used to calculate their pore volumes and surface areas with the use of H₂ and He probes, respectively, pore limiting diameter (i.e., the diameter of smallest opening along the pore) and largest cavity diameter (i.e., the diameter of the largest sphere that can fit within the pores).

Table S1. Some calculated and experimentally determined properties of the MUF-16 family.

	MUF-16	MUF-16(Mn)	MUF-16(Ni)
Geometric surface area (m ² /g, Zeo++)	313	315	313
BET surface area (m ² /g, from experimental N ₂ isotherm/77 K)	215	209	238
Calculated void fraction (% , RASPA2)	17.3	17.0	16.7
Calculated pore volume (cm ³ /g, RASPA2)	0.10	0.11	0.11
Pore volume (cm ³ /g, from experimental N ₂ isotherm/77 K)	0.11	0.12	0.11
Largest cavity diameter (Å)	3.63	3.58	3.61
Pore limiting diameter (Å)	2.95	2.95	2.96

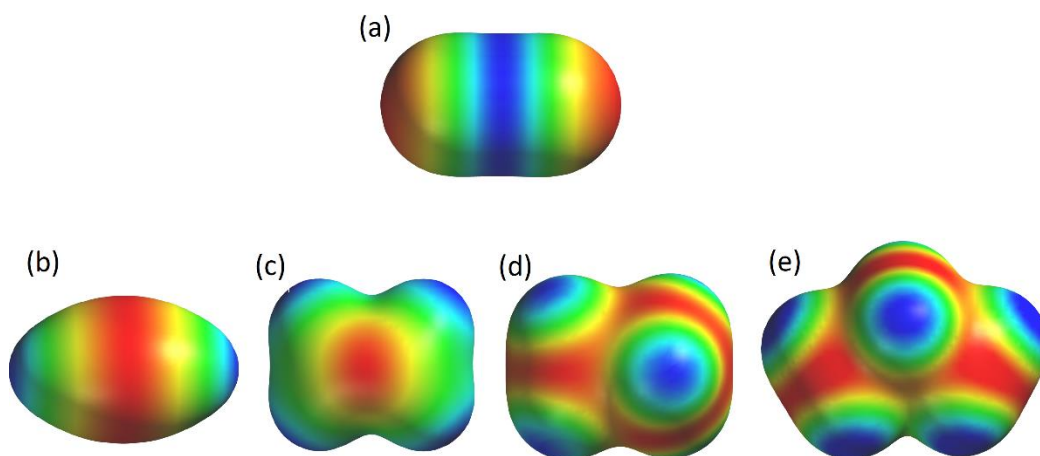


Figure S1. Electrostatic potential maps of (a) CO₂, (b) C₂H₂, (c) C₂H₄, (d) C₂H₆ and (e) C₃H₈
Blue/green = positive; red/orange = negative.

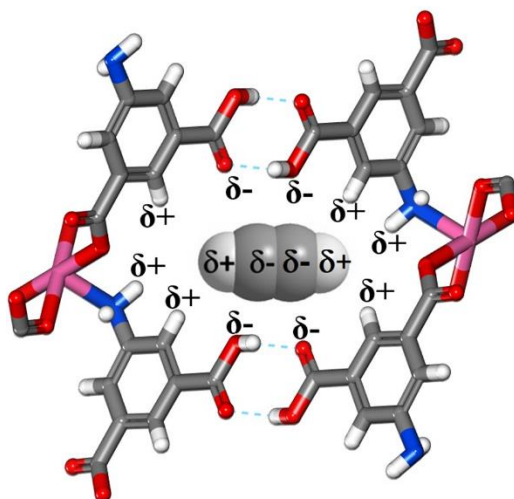


Figure S2. Schematic of electrostatic potential distribution on the pore surface of MUF-16 leads to repulsive interactions with guest C₂H₂ molecules if they occupy the sites crystallographically observed for the binding of CO₂.

Table S2. Physicochemical characteristics of different gasses relevant to their separation.³⁻⁶

	Boiling point (K)	Molecular dimensions (Å)	Polarizability (Å ³)	Dipole moment ×10 ¹⁸ /esu cm ²	Quadrupole moment ×10 ²⁶ /esu cm ²
CO ₂	216.5	3.18×3.33×5.36	2.91	0	-4.3
N ₂	77.35	2.99×3.05×4.04	0.80	0	1.52
CH ₄	111.66	3.82×3.94×4.10	2.59	0	0
H ₂	20.27	-	1.74	0	0.66
C ₂ H ₂	188.4	3.32×3.34×5.7	3.33-3.93	0	+7.5
C ₂ H ₄	169.4	3.28×4.18×4.84	4.25	0	+1.5
C ₂ H ₆	184.5	3.81×4.82×4.08	4.43-4.47	0	+0.65
C ₃ H ₈	231.0	6.80×4.20×3.80	6.29-6.37	0.084	-

2. Synthesis

2.1 MUF-16 ([Co(Haip)₂])

Small-scale synthesis:

A mixture of Co(OAc)₂·4H₂O (0.625 g, 2.5 mmol), 5-aminoisophthalic acid (1.8 g, 10 mmol), methanol (80 mL) and water (5 mL) were sonicated for 20 min in a sealed 1000 mL Schott bottle, which was then heated in a pre-heated oven at 70 °C for 2 hours under autogenous pressure. After cooling the oven to room temperature, the resulting pink crystals were isolated by decanting off the mother liquor, washed with methanol several times and dried under vacuum at 130 °C for 20 h. Yield: 0.98 g (94% based on cobalt) of guest-free MUF-16.

Large-scale synthesis:

A mixture of $\text{Co}(\text{OAc})_2 \cdot 4\text{H}_2\text{O}$ (5.0 g, 20 mmol), 5-aminoisophthalic acid (12 g, 68 mmol), methanol (490 mL) and water (40 mL) were sonicated for 20 min in a sealed 2000 mL Schott bottle, which was partly (~20%) prefilled with glass beads. The bottle was then heated in a pre-heated oven at 70 °C for 5 hours under autogenous pressure. After cooling the oven to room temperature, the resulting pink crystals were isolated by decanting off the mother liquor, washed with methanol several times and dried under vacuum at 130 °C for 20 h. Yield: 7.8 g (92% based on cobalt) of guest-free MUF-16.



Figure S3. Photograph of MUF-16 produced on a large-scale after drying.

Cost estimate: Commercial prices are approximately H_2aip = 15 USD/kg and $\text{Co}(\text{OAc})_2 \cdot 4\text{H}_2\text{O}$ = 10 USD/kg. Therefore, 1 kg of $\text{Co}(\text{OAc})_2 \cdot 4\text{H}_2\text{O}$ (10 USD) requires 2.4 kg of H_2aip (36 USD) and produces 1.56 kg of MUF-16 for approx. 46 USD. The raw materials cost of MUF-16 is ≤ 29 USD/kg.

2.2 MUF-16(Mn) and MUF-16(Ni) ($[\text{Mn}(\text{Haip})_2]$ and $[\text{Ni}(\text{Haip})_2]$)

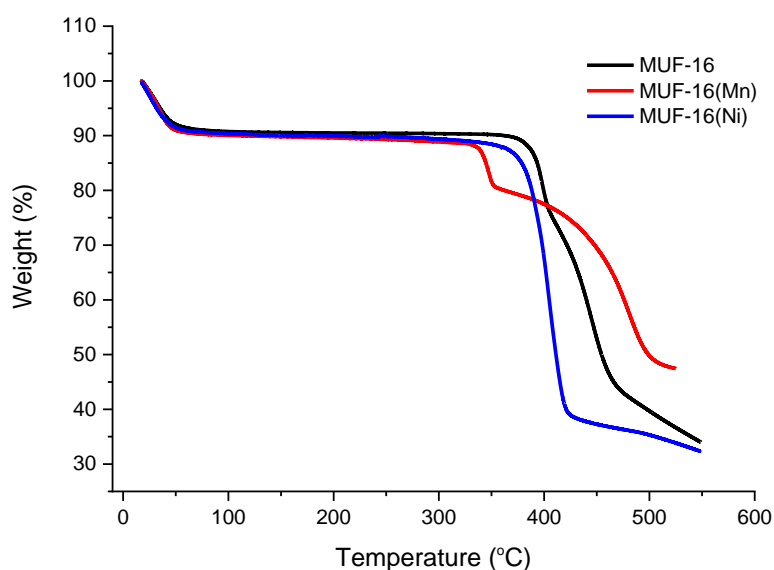
A mixture of $\text{M}(\text{ClO}_4)_2 \cdot 6\text{H}_2\text{O}$ (where M = Mn or Ni) (1.25 mmol), 5-aminoisophthalic acid (2.50 mmol, 0.45 g), and NH_4NO_3 (2.50 mmol, 0.20 g) with a mixed-solvent of CH_3CN (20 mL) and CH_3OH (15 mL) were sonicated for 20 min and sealed in a 100 mL Teflon-lined stainless-steel reaction vessel and heated at 160 °C for two days under autogenous pressure. After cooling the oven to room temperature, the resulting brownish crystals were isolated by decanting off the mother liquor, washed with methanol several times and dried under vacuum at 130 °C for 20 h. Yields: 0.21 g (40% based on Mn) of guest free MUF-16(Mn), and 0.28 g (53% based on Ni) of guest-free MUF-16(Ni).

Table S3. Elemental analysis of the MUF-16 frameworks.

	C: calcd./found	H: calcd./found	N: calcd./found
MUF-16·H ₂ O	43.95/43.49	3.23/3.23	6.41/6.40
MUF-16(Mn)·H ₂ O	44.36/44.05	3.26/3.42	6.47/6.64
MUF-16(Ni)·H ₂ O	43.98/44.18	3.23/3.57	6.41/6.90

3. Thermogravimetric Analysis (TGA)

Freshly prepared MOF samples were washed with MeOH, and then activated at 130 °C under vacuum for 10 hours. Samples were exposed to air for 1 hour and then transferred to an aluminium sample pan, and then measurements were commenced under an N₂ flow with a heating rate of 5 °C /min.

**Figure S4.** TGA curves of MUF-16, MUF-16(Mn), and MUF-16(Ni).

4. Single crystal X-ray diffraction

A Rigaku Spider diffractometer equipped with a MicroMax MM007 rotating anode generator (Cu α radiation, 1.54180 Å), high-flux Osmic multilayer mirror optics, and a curved image plate detector was used to collect SCXRD data.

4.1 As-synthesized MUF-16, MUF-16(Ni) and MUF-16(Mn)

MOF crystals were analysed after removing them from methanol. Room temperature data collections produced better refinement statistics than low temperature data collections. All atoms were found in the electron density difference map. All atoms were refined anisotropically, except hydrogen atoms and certain of the water molecules in the pores. A solvent mask was calculated for MUF-16(Ni) and 124 electrons were found in a volume of 308 Å³ in 1 void per unit cell. This is consistent with the presence of three disordered water molecules per asymmetric unit, which account for 120 electrons per unit cell.

Table S4. Crystal data and structure refinement details for MUF-16, MUF-16(Mn) and MUF-16(Ni).

	MUF-16	MUF-16(Mn)	MUF-16(Ni)
Formula	Co(Haip) ₂ ·2H ₂ O	Mn(Haip) ₂ ·3H ₂ O	Ni(Haip) ₂ ·3H ₂ O
CCDC deposition no.	1948901	1948902	1948903
Empirical formula	C ₁₆ H ₁₆ CoN ₂ O ₁₀	C ₁₆ H ₁₈ MnN ₂ O ₁₁	C ₁₆ H ₁₈ N ₂ NiO ₁₁
Formula weight	455.24	471.28	473.3
Temperature / K	292	292	293.0
Crystal system	monoclinic	monoclinic	monoclinic
Space group	I2/a	I2/a	I2/a
a / Å	15.3514(15)	25.2367(14)	15.4963(11)
b / Å	4.4232(4)	4.57990(10)	4.5780(2)
c / Å	25.614(4)	15.4895(11)	25.230(2)
α / °	90	90	90
β / °	94.294(10)	96.046(8)	96.177(8)
γ / °	90	90	90
Volume / Å ³	1734.4(4)	1780.34(17)	1779.5(2)
Z	4	4	4
ρ _{calc} / g cm ⁻³	1.743	1.758	1.564
μ / mm ⁻¹	8.357	6.682	2.020
F(000)	932.0	972.0	856.0
Resolution range for data/ Å	0.81	0.81	1.0
Reflections collected	7472	14132	6610
Independent reflections	1594 [R _{int} = 0.0918, R _{sigma} = 0.0917]	1668 [R _{int} = 0.1054, R _{sigma} = 0.1158]	925 [R _{int} = 0.0917, R _{sigma} = 0.0852]
Data/restraints/parameters	1594/2/136	1668/1/149	925/0/126
Goodness-of-fit on F ²	1.301	1.152	1.649
Final R indices [I>2σ(I)]	R ₁ = 0.1185, wR ₂ = 0.3035	R ₁ = 0.0740, wR ₂ = 0.1821	R ₁ = 0.1517, wR ₂ = 0.3672
Final R indices [all data]	R ₁ = 0.1576, wR ₂ = 0.3785	R ₁ = 0.1350, wR ₂ = 0.2421	R ₁ = 0.2061, wR ₂ = 0.4467
Largest diff. peak/hole / e Å ⁻³	0.93/-1.26	0.57/-0.51	0.77/-0.83

4.2 Single crystal X-ray crystallography under vacuum and loaded with CO₂

Capillary SCXRD was performed for a single crystal of MUF-16(Mn) both under vacuum and loaded with CO₂ at around 1.1 bar and 20 °C based on the following steps:

First a single crystal was chosen with an appropriate size ($\sim 0.1 \times 0.1 \times 0.1$ mm) and soaked in ethanol. A small capillary tube with around 0.2 mm in diameter and 50 mm in length (which is open at both ends) was made by burning and shaping the neck of a glass pipette (referred to as the ‘home-made capillary’). The home-made capillary was then used to trap the crystal inside it. Normally, the crystal flowed through the capillary carried by the ethanol stream.

The home-made capillary was then transferred into a standard 0.3 mm capillary. A long capillary (0.2 mm in diameter) was used to push the home-made capillary to the very bottom of the 0.3 mm capillary.

Around 6 or 7 crystals of cobalt chloride hydrate were then transferred to the 0.3 mm capillary and placed on the top of the home-made capillary. The cobalt chloride was used as a visual indicator of the level of water vapour in the capillary based on its pink \rightarrow blue colour change upon dehydration.

The top of the 0.3 mm capillary was then covered by glass wool to avoid the elutriation of cobalt chloride crystals during activation.

The capillary assembly was then connected to an adsorption apparatus (Quantachrome-Autosorb-iQ2) using appropriate Swagelok fittings (Figure S4) and was kept under vacuum and a temperature of 140 °C for around 5 hours so that the vacuum level reached 0.0008 torr. At this point the cobalt chloride crystals were blue in colour (anhydrous).

The capillary was flame sealed to trap the crystal under vacuum. Alternatively, the capillary was filled with CO₂ to a pressure of 1.2 bar and then flame sealed.

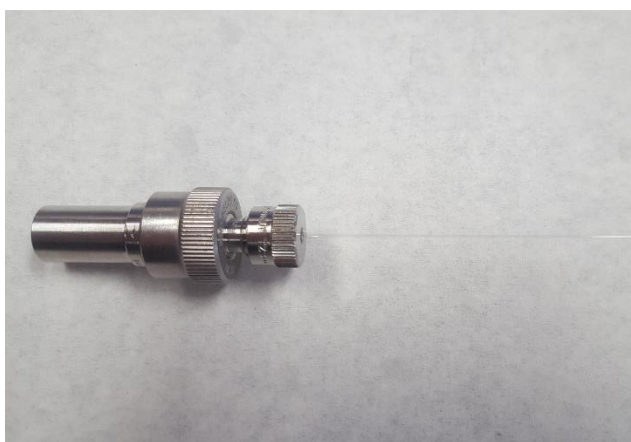


Figure S5. Swagelok fittings for connecting capillary to Quantachrome-Autosorb-iQ2.

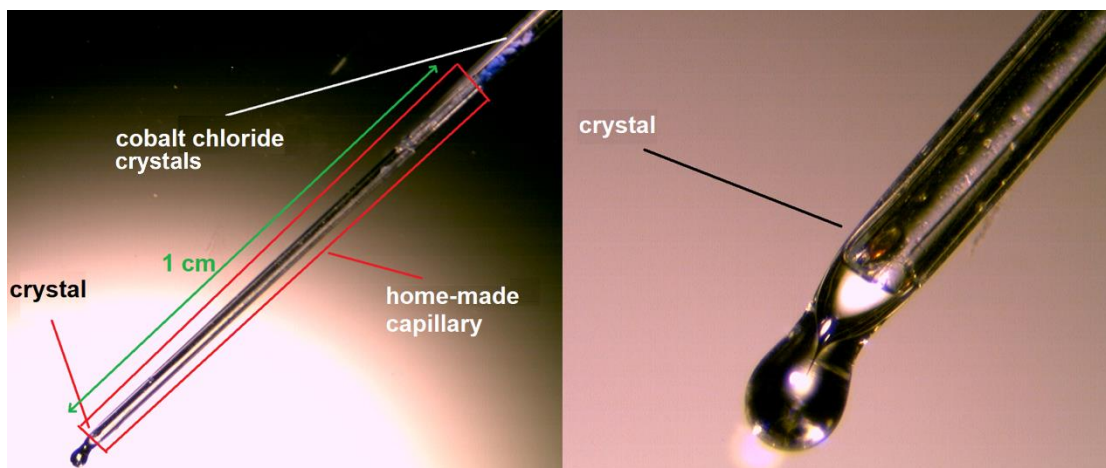


Figure S6. Schematic and dimensions of capillaries used for SCXRD.

4.3 Refinement details for guest-free and CO₂-loaded MUF-16(Mn)

Certain reflections were omitted from the refinement process since they were mismeasured due to the presence of the glass capillary. All non-hydrogen atoms were found in the Fourier difference map. For the CO₂-loaded structure, a strong electron density peak was observed in the middle of the pore and two weaker areas of electron density towards the pore surface. The central dense area was assigned to be an oxygen (O15) with a fixed occupancy of 1 (lowering for its location on a special position), while the other two areas were ascribed to oxygen (O16) and carbon (C17) atoms with fixed occupancies of 0.5. This describes two disordered CO₂ molecules that occupy one of two sites. The two molecules share an O atom. Overall, this equates to one CO₂ molecule per Mn centre which is in agreement with the adsorption isotherm. The C=O bond lengths were restrained to 1.16 Å and the O=C=O angle to 180° and C and O atoms refined isotropically.

Table S5. SCXRD data and refinement details of guest-free and CO₂-loaded MUF-16(Mn).

	MUF-16(Mn) <i>in vacuo</i>	MUF-16(Mn) under CO ₂ (1.1 bar)
Formula	Mn(Haip) ₂	Mn(Haip) ₂ ·CO ₂
CCDC deposition no.	1948905	1948904
Empirical formula	C ₁₆ H ₁₂ MnN ₂ O ₈	C ₁₇ H ₁₂ MnN ₂ O ₁₀
Formula weight	415.22	459.23
Temperature/K	292	292
Crystal system	monoclinic	monoclinic
Space group	<i>I</i> 2/a	<i>I</i> 2/a
a/Å	15.4872(11)	15.5719(10)
b/Å	4.51930(10)	4.52010(10)
c/Å	25.4913(13)	25.438(2)
α/°	90	90
β/°	97.080(16)	97.108(8)
γ/°	90	90
Volume/Å ³	1770.56(17)	1776.7(2)
Z	4	4
ρ _{calc} /g cm ⁻³	1.558	1.717
μ/mm ⁻¹	6.512	6.646
F(000)	844.0	932.0
Data range for refinement/ Å	0.90	1.08
Reflections collected/ind.	7515/1214 [R _{int} = 0.1632, R _σ = 0.1964]	8177/713 [R _{int} = 0.1104, R _σ = 0.0804]
Data/restraints/parameters	1214/0/129	713/90/136
Goodness-of-fit on F ²	0.862	1.216
Final R indexes [I>=2σ (I)]	R ₁ = 0.0510, wR ₂ = 0.0954	R ₁ = 0.0868, wR ₂ = 0.2280
Final R indexes [all data]	R ₁ = 0.1341, wR ₂ = 0.1112	R ₁ = 0.1278, wR ₂ = 0.2915
Largest diff. peak/hole / e Å ⁻³	0.35/-0.48	0.56/-0.58

5. Powder X-ray diffraction patterns

The data were obtained from freshly prepared MOF samples that had been washed several times with MeOH. MOF crystals were analysed right after removing them from MeOH. The two-dimensional images of the Debye rings were integrated with 2DP to give 2θ vs I diffractograms. Predicted powder patterns were generated from single crystal structures using Mercury.

For aging experiments on the frameworks, after washing as-synthesized samples several times with MeOH, they were activated and were aged in air at 70-85% relative humidity or water at 20 °C.

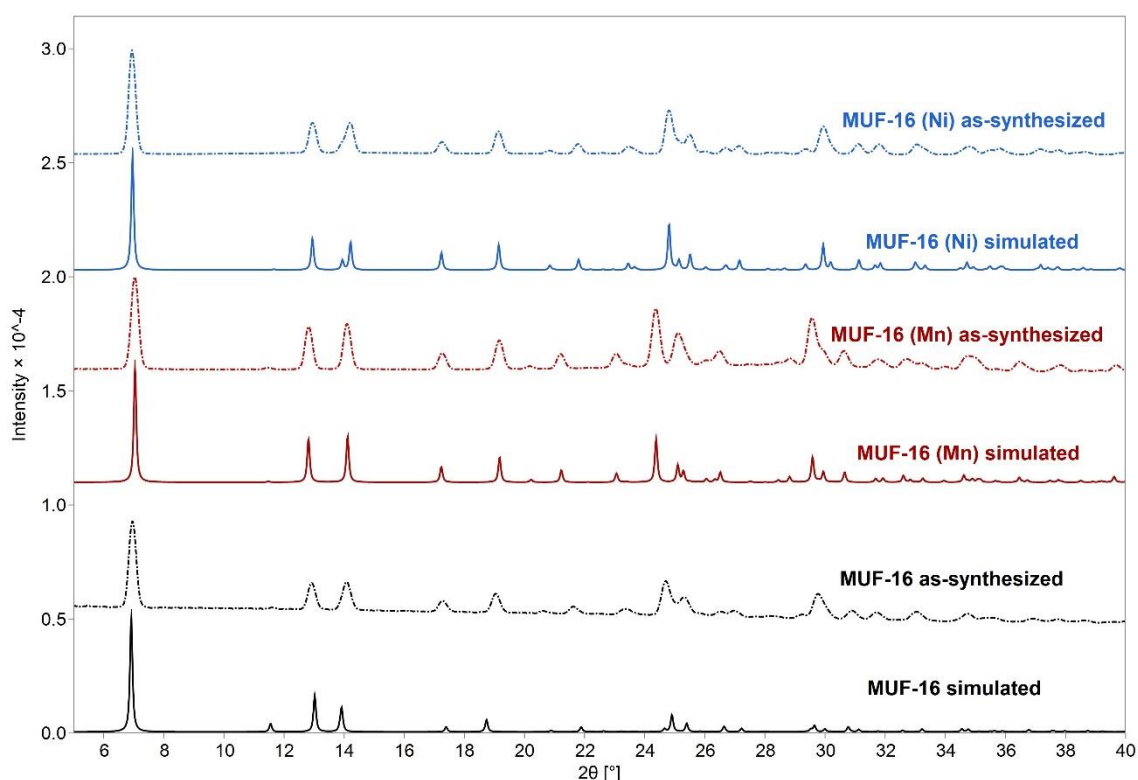
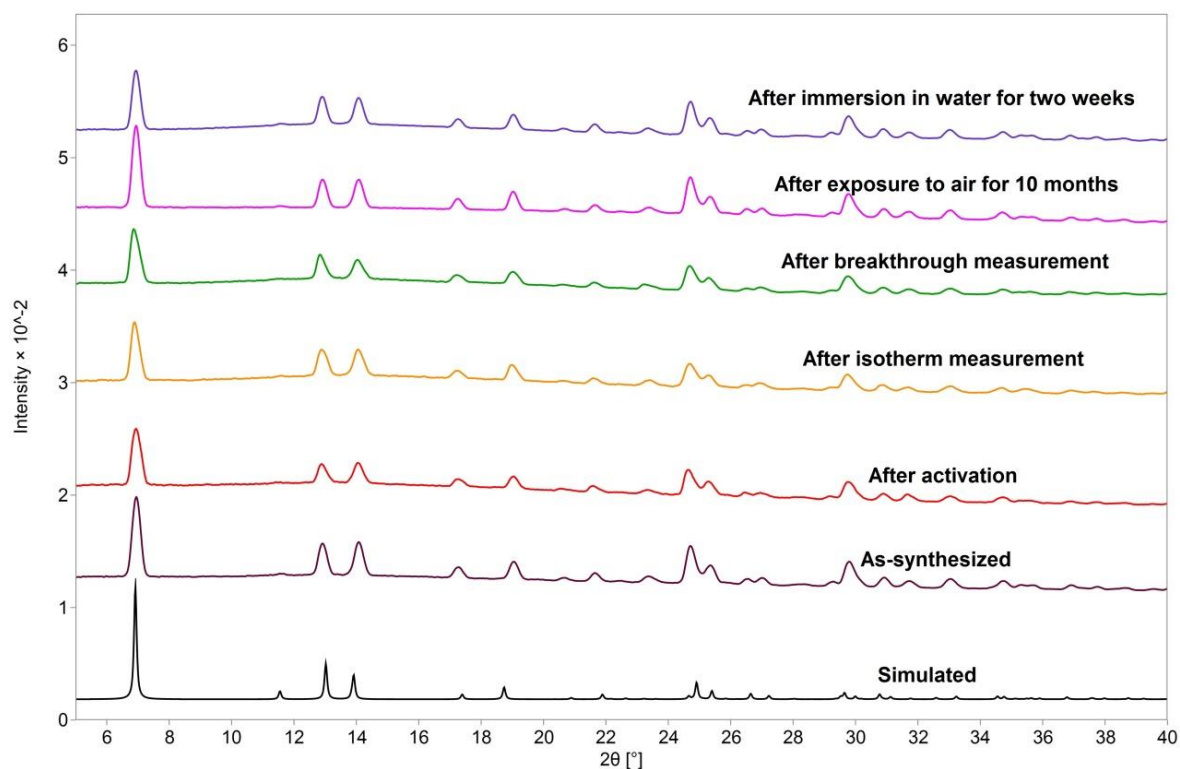


Figure S7. PXRD patterns of MUF-16, MUF-16(Mn) and MUF-(Ni) with comparisons between measurements on as-synthesized bulk samples and diffractograms predicted from SCXRD structures.



FigureS8. PXRD patterns of MUF-16 showing that its structure remains unchanged after activation at 130 °C under vacuum, after isotherm measurements, after breakthrough experiments, after exposure to an air with relative humidity of >80% for at least 12 months and after immersion in water for two weeks.

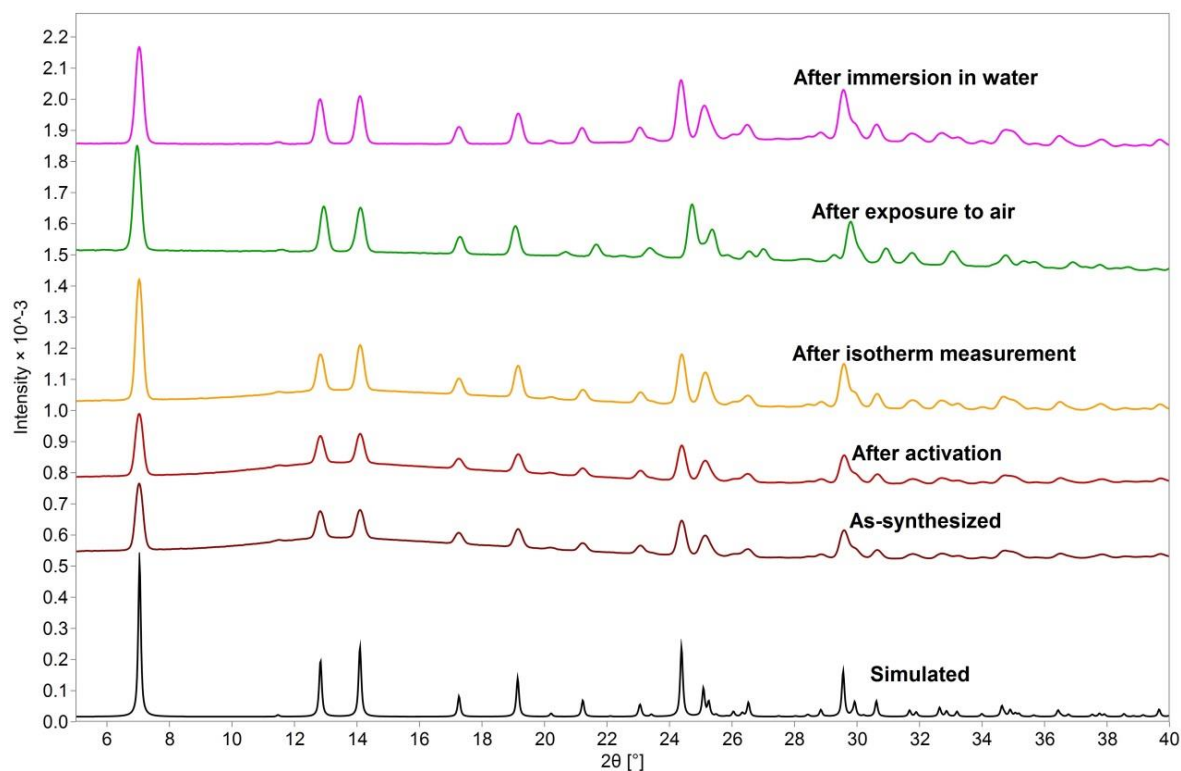


Figure S9. PXRD patterns of MUF-16(Mn) showing that its structure remains unchanged after activation at 130 °C under vacuum, after isotherm measurements, after exposure to an air with relative humidity of >80% for at least 12 months and after immersion in water for 2 weeks.

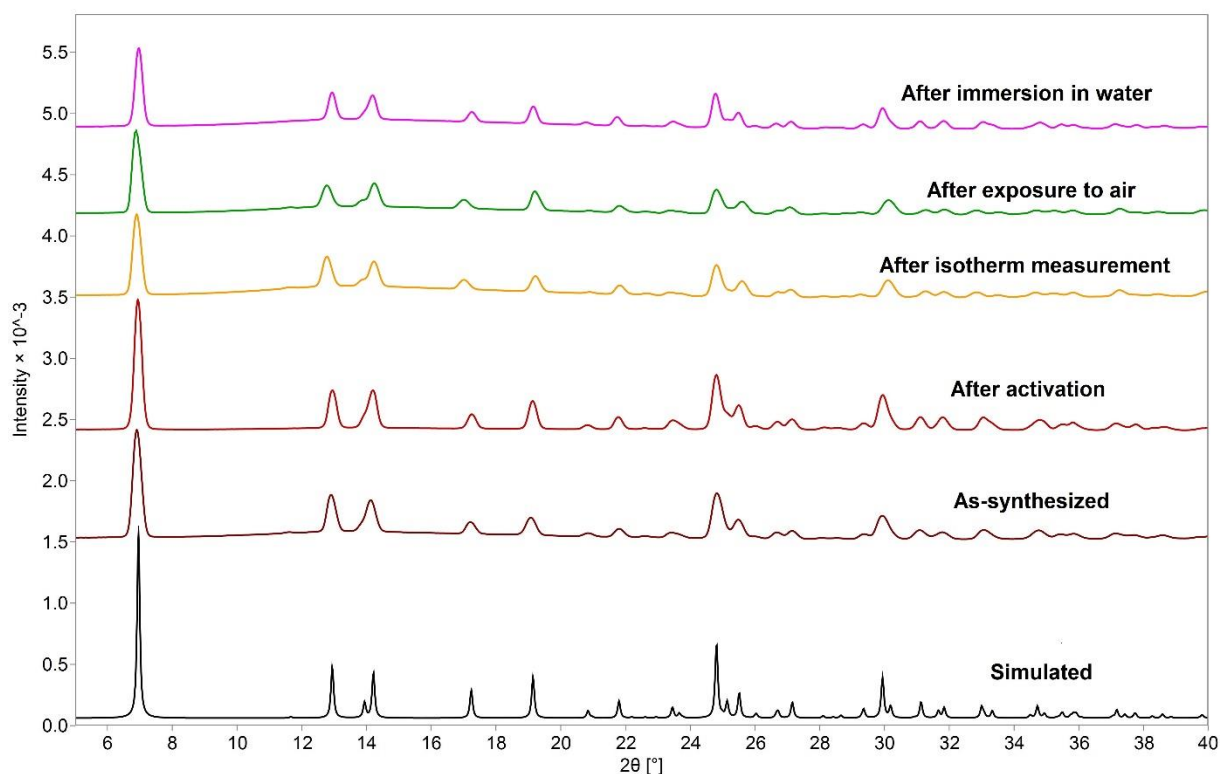


Figure S10. PXRD patterns of MUF-16(Ni) showing that its structure remains unchanged after activation at 130 °C under vacuum, after isotherm measurements, after exposure to an air with relative humidity of >80% for at least 12 months and after immersion in water for 2 weeks.

6. Low-pressure gas adsorption measurements

The as-synthesized samples were washed with anhydrous methanol several times and 50-1000 mg was transferred into a pre-dried and weighed sample tube. Large sample quantities were used to measure isotherms of the weakly-adsorbing gases to ensure reliable results. To activate the sample, it was heated at rate of 10°C/min to a temperature of 130 °C under a dynamic vacuum with a turbomolecular pump for 20 hours.

Table S6. Uptake capacity of CO₂ at 293 K and 1 bar of MUF-16.

	Uptake (wt%)	Molecules of CO₂ per unit cell	Molecules of CO₂ per metal	Fraction of void volume occupied by CO₂*
MUF-16	9.38	3.57	0.89	0.67
MUF-16(Ni)	9.41	3.58	0.89	0.68
MUF-16(Mn)	9.90	3.74	0.93	0.70

*The fraction of the total free volume of MUF-16 that is occupied by adsorbate molecules. This was calculated from the accessible void fraction given by RASPA2 software (Table S1), the molecular volume of the CO₂ adsorbates (56.75 Å³/molecule) and the total number of adsorbate molecules.

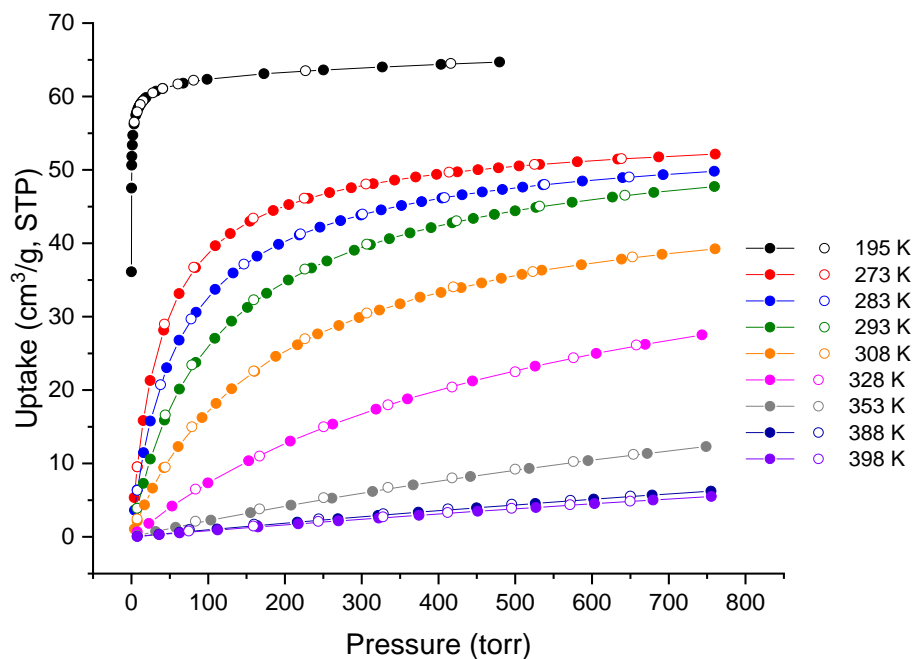


Figure S11. Volumetric adsorption (filled circles) and desorption (open circles) isotherms of CO₂ at different temperatures for MUF-16.

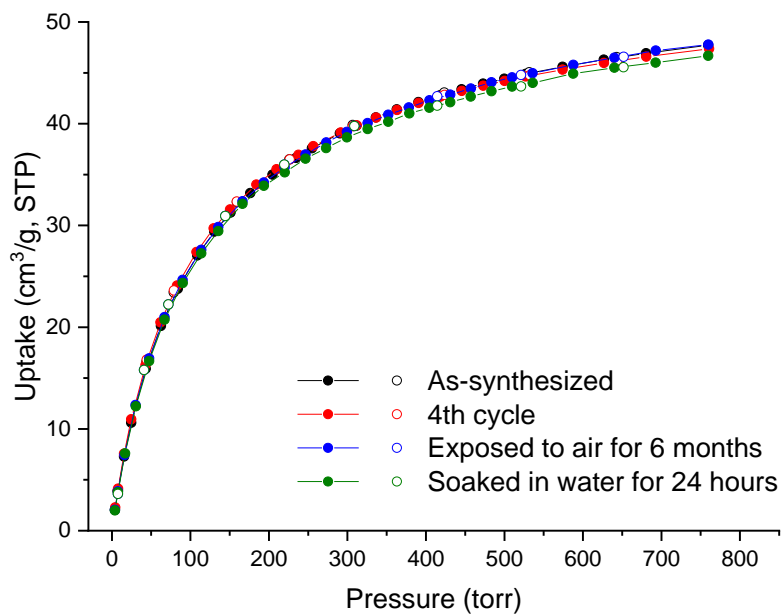


Figure S12. CO₂ adsorption isotherms (293 K) of as-synthesized MUF-16 after four consecutive adsorption-desorption cycles, after exposing it to air with ~80% humidity for 6 months, and after immersion in water for 48 hours.

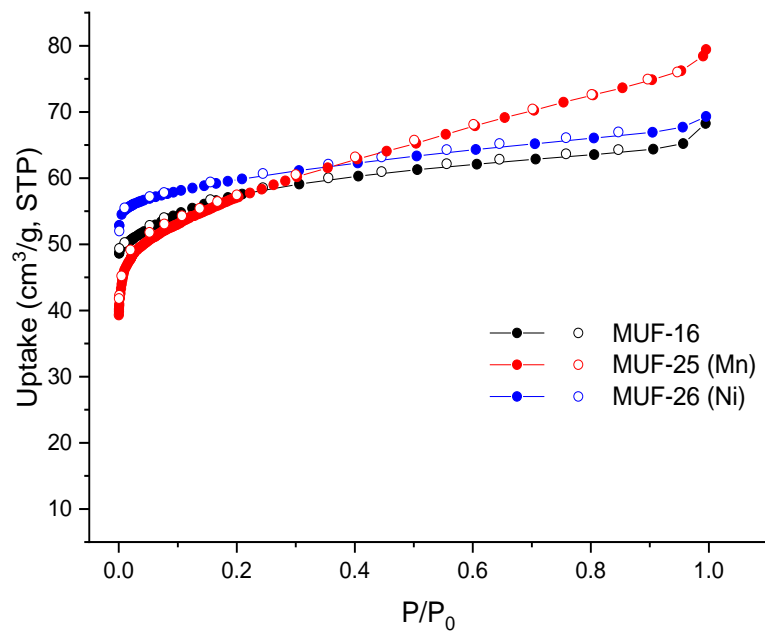


Figure S13. Volumetric adsorption (filled circles) and desorption (open circles) isotherms of N_2 for MUF-16 (black), MUF-16(Mn) (red) and MUF-16(Ni) (blue) measured at 77 K.

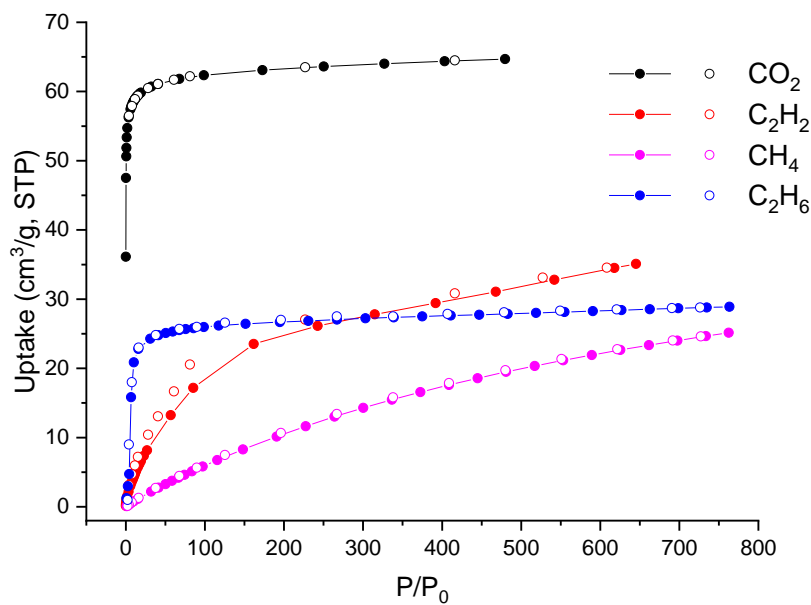


Figure S14. Volumetric adsorption (filled circles) and desorption (open circles) isotherms of CO_2 (black), C_2H_2 (red), C_2H_6 (blue) and CH_4 (purple) measured at 195 K for MUF-16.

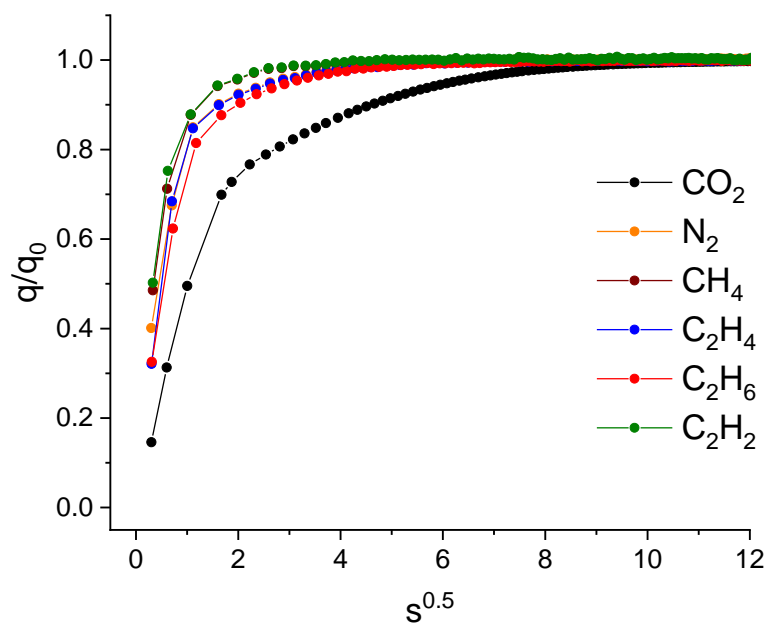


Figure S15. Kinetic profiles of different gas uptake by MUF-16 at 293 K upon exposing an evacuated sample to a dose of gas equal to its measured total adsorption of that gas at 1 bar. q is the amount of uptake at time t and q_0 is the final uptake amount.

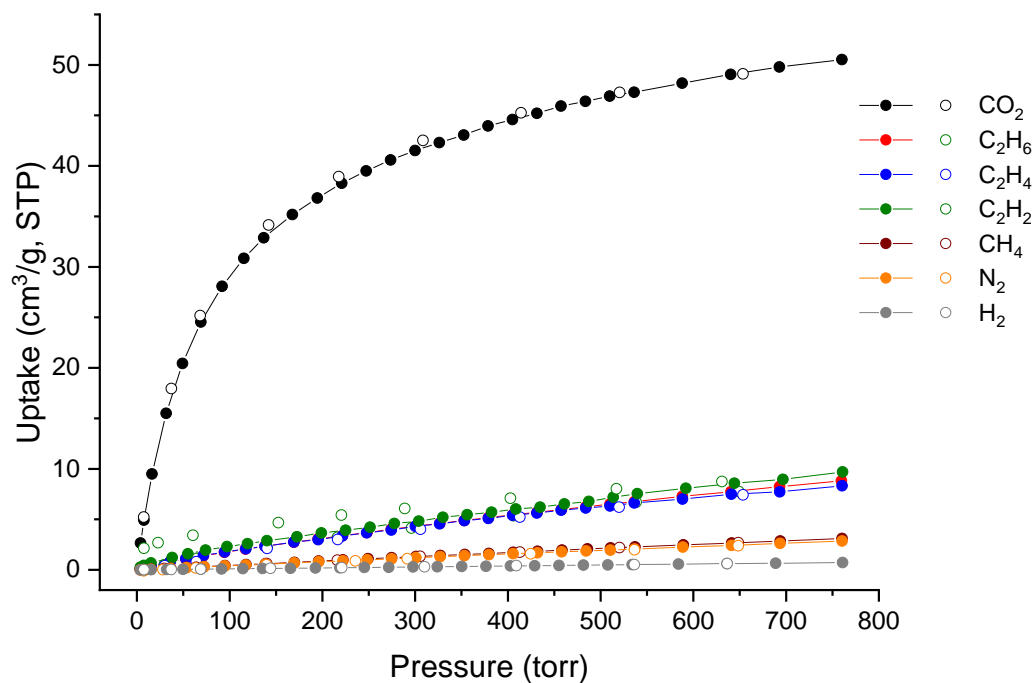


Figure S16. Volumetric adsorption (filled circles) and desorption (open circles) isotherms of different gases by MUF-16(Mn) at 293 K.

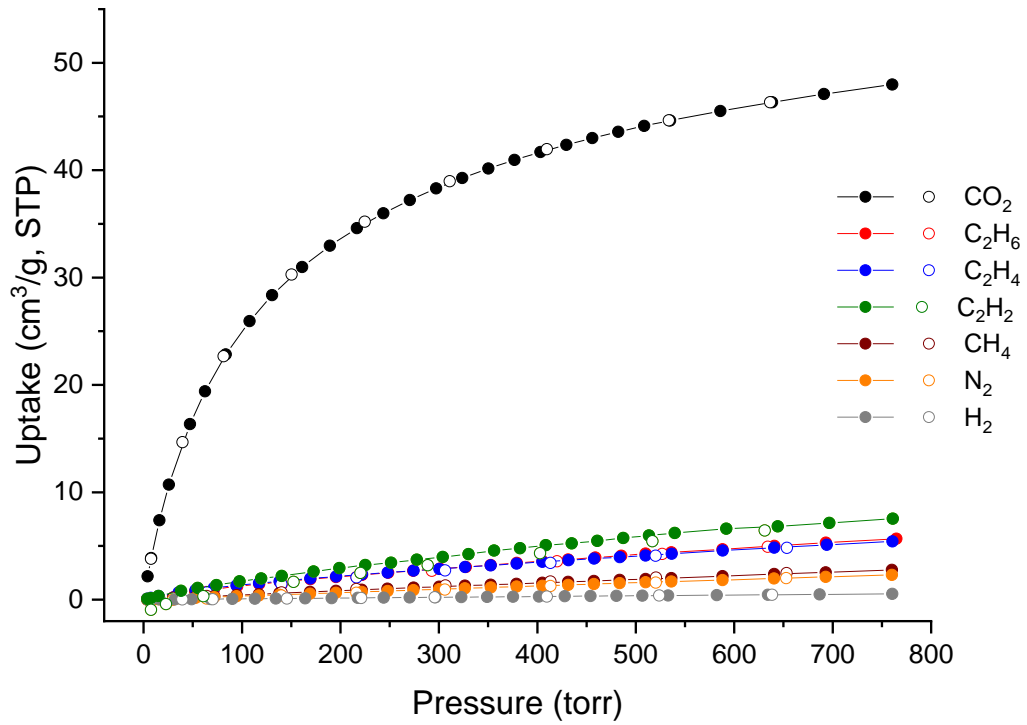


Figure S17. Volumetric adsorption (filled circles) and desorption (open circles) isotherms of different gases by MUF-16(Ni) at 293 K.

7. Calculation of BET surface areas

BET surface areas were calculated from N₂ adsorption isotherms at 77 K according to the following procedures⁷:

- 1) The isotherm region where $v(1 - P/P_0)$ increases versus P/P_0 , where v is the amount of N₂ adsorbed, was identified.
- 2) Within this isotherm region, sequential data points that led to a positive intercept in the plot of $\frac{P/P_0}{v(1-P/P_0)}$ against P/P_0 , were found. This plot yields a slope a , and a positive intercept b . The amount of gas molecules adsorbed in the initial monolayer is $v_m = \frac{1}{a+b}$.

- 3) The BET surface area was calculated according to the following equation:

$$A_{BET} = v_m (cm^3 g^{-1}) * \frac{1 (mol)}{22400 (cm^3)} * \sigma_0 (\text{\AA}^2) * N_A (mol^{-1}) * 10^{-20} \left(\frac{m^2}{\text{\AA}^2}\right)$$

Where N_A is Avogadro's constant, and σ_0 is the cross-sectional area of a N₂ molecule, which is 16.2 Å².

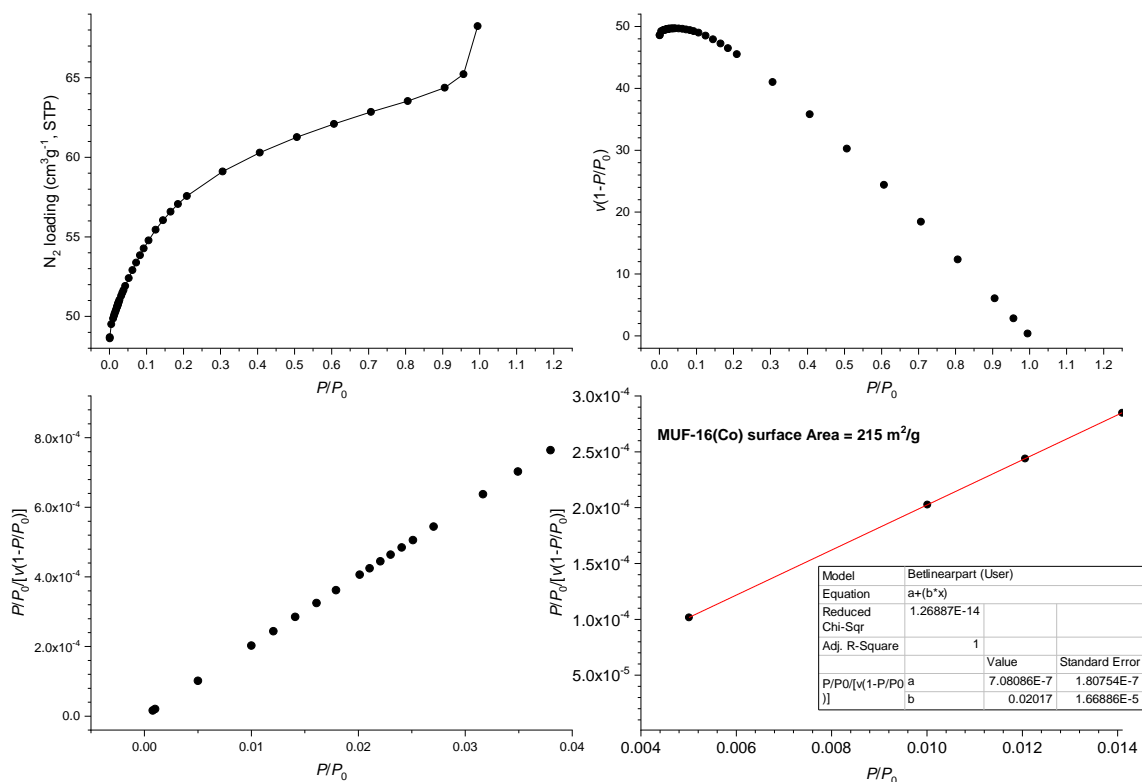


Figure S18. N₂ adsorption isotherm at 77 K and BET surface area plots for MUF-16.

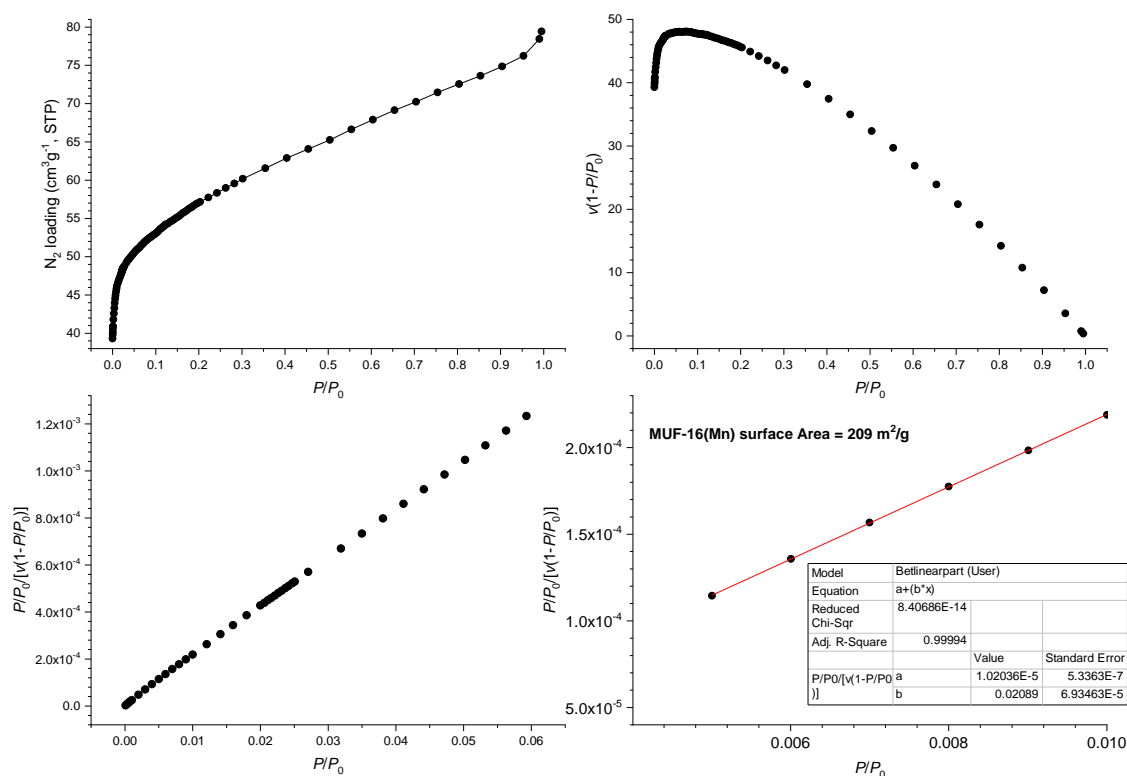


Figure S19. N₂ adsorption isotherm at 77 K and BET surface area plots for MUF-16(Mn).

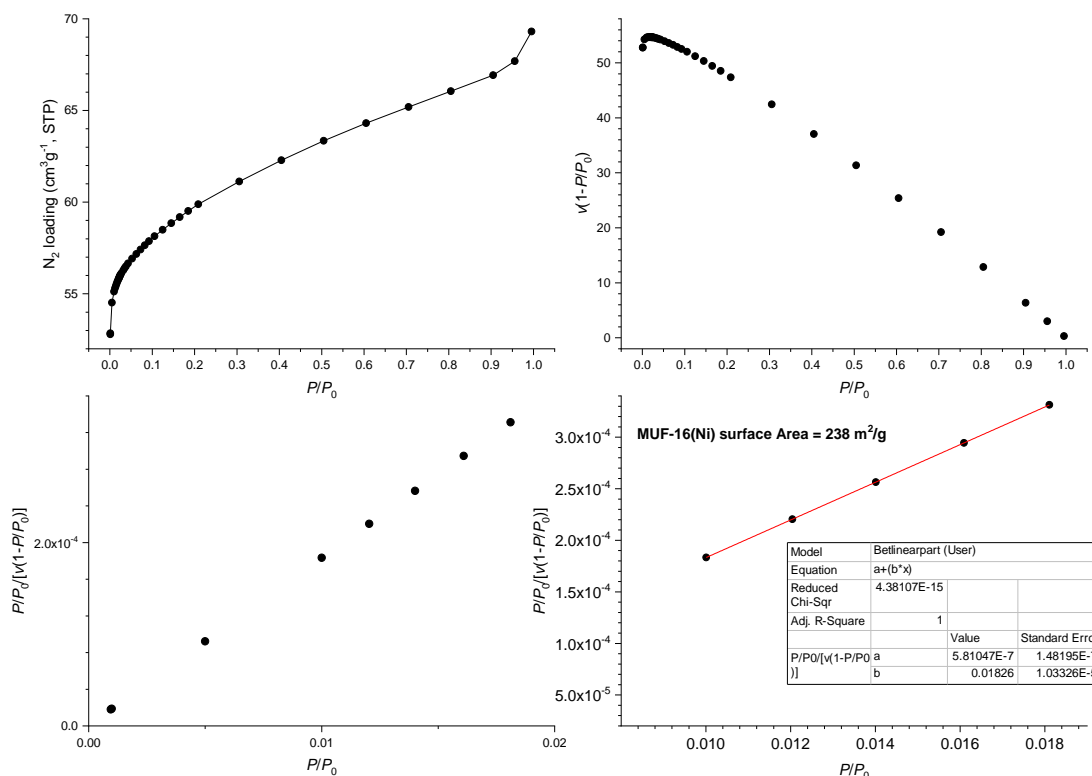


Figure S20. N₂ adsorption isotherm at 77 K and BET surface area plots for MUF-16(Ni).

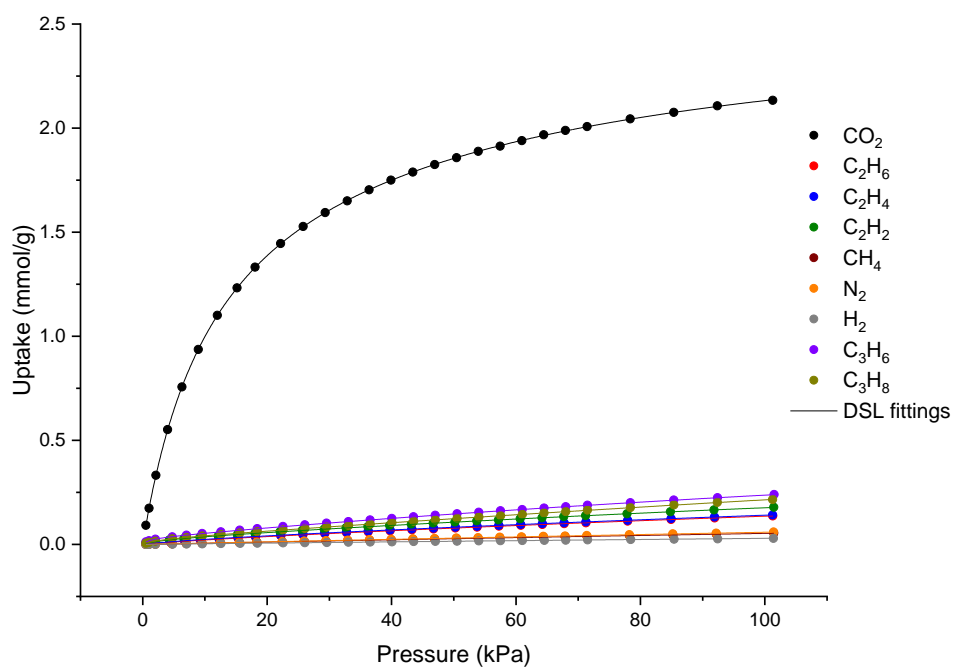
8. IAST calculations

Mixed gas adsorption isotherms and gas selectivities for different mixtures of CO₂/C₂H₂, CO₂/C₂H₄, CO₂/C₂H₆, CO₂/N₂, CO₂/CH₄ and CO₂/H₂ at 293 K were calculated based on the ideal adsorbed solution theory (IAST) proposed by Myers and Prausnitz⁸. The pyIAST package⁹ was used to perform the IAST calculations. In order to predict the sorption performance of MUF-16 toward the separation of binary mixed gases, the single-component adsorption isotherms were first fit to a Dual Site Langmuir or Dual Site Langmuir Freundlich model as below:

$$q = \frac{q_1 b_1 P}{1 + b_1 P} + \frac{q_2 b_2 P}{1 + b_2 P}$$

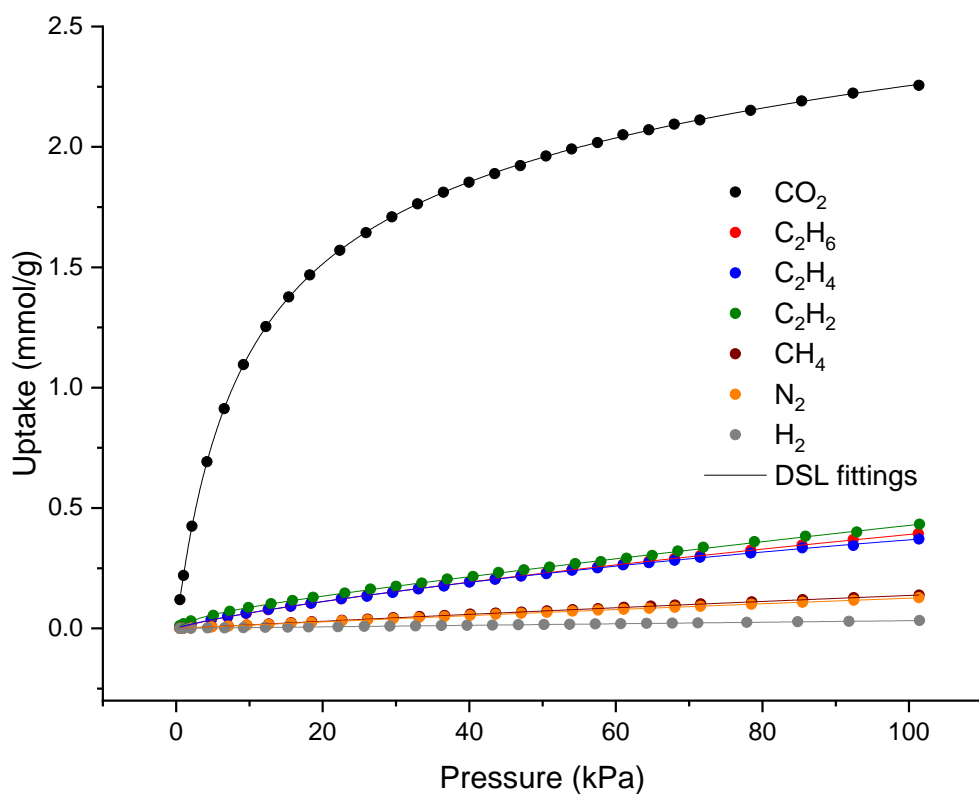
$$q = \frac{q_1 b_1 P^{1/t_1}}{1 + b_1 P^{1/t_1}} + \frac{q_2 b_2 P^{1/t_2}}{1 + b_2 P^{1/t_2}}$$

Where q is the uptake of a gas; P is the equilibrium pressure and q_1 , b_1 , t_1 , q_2 , b_2 and t_2 are constants. These parameters were used subsequently to carry out the IAST calculations.



Model	DSL (User)								
Equation	$q1 \cdot b1 \cdot x / (1 + b1 \cdot x) + q2 \cdot b2 \cdot x / (1 + b2 \cdot x)$								
Plot	CO2	C2H6	C2H4	C2H2	CH4	N2	H2	C3H6	C3H8
q1	1.92197 ± 0.03622	0.01903 ± 7.58427E-4	0.90455 ± 0.02194	0.84858 ± 0.02172	-1.37048E-4 ± 2.62012E-5	-1.30883E-4 ± 1.93944E-5	1.46115E-4 ± 1.23483E-4	0.92327 ± 0.02031	0.02582 ± 8.46918E-4
b1	0.09147 ± 0.00142	0.06919 ± 0.00295	0.00155 ± 4.83418E-5	0.00219 ± 7.32671E-5	2.40335 ± 2.41269	1.42902 ± 0.89123	1.47 ± 0	0.00289 ± 8.52827E-5	0.38985 ± 0.03262
q2	0.71591 ± 0.02029	0.91643 ± 0.02976	0.02077 ± 4.66874E-4	0.02486 ± 4.712E-4	0.63958 ± 0.01292	0.86986 ± 0.01365	0.4377 ± 0.00344	0.03023 ± 4.69954E-4	2.11273 ± 0.21651
b2	0.01264 ± 0.0014	0.00149 ± 6.32966E-5	0.09736 ± 0.00278	0.29065 ± 0.01171	9.04454E-4 ± 2.00076E-5	7.2231E-4 ± 1.22207E-5	7.1E-4 ± 0	0.92871 ± 0.04824	9.83565E-4 ± 1.13365E-4
Reduced Chi-Sqr	2.547E-6	4.27057E-9	4.09689E-9	3.87189E-8	1.11837E-9	4.7599E-10	1.0175E-7	1.63183E-7	2.34956E-7
R-Square (COD)	0.99999	1	1	0.99999	1	1	0.99871	0.99997	0.99994
Adj. R-Square	0.99999	1	1	0.99998	1	1	0.99866	0.99996	0.99994

Figure S21 Dual-site Langmuir fits of various adsorption isotherms for MUF-16 at 293 K.



Model	DSL (User)						
Equation	$q1 \cdot b1 \cdot x / (1 + b1 \cdot x) + q2 \cdot b2 \cdot x / (1 + b2 \cdot x)$						
Plot	CO2	C2H6	C2H4	C2H2	CH4	N2	H2
q1	1.94289 ± 0.0227	0.04806 ± 0.00391	1.11314 ± 0.0652	3.94913 ± 1.20449	1.20612 ± 0.06748	1.33778 ± 0.08483	13.5332 ± --
b1	0.12229 ± 0.00169	0.09141 ± 0.009	0.00448 ± 4.81593E-	0.00102 ± 3.53725E-	0.00129 ± 8.15601E-5	0.00103 ± 7.0371E-	2.3718E-5 ± -
q2	1.14216 ± 0.04571	2.04938 ± 0.09902	0.02464 ± 0.00777	0.06637 ± 0.00631	-8.32165E-4 ± 2.43966E	0 ± 0	0 ± 0
b2	0.0067 ± 8.46612E-	0.00204 ± 1.38007E-	0.20141 ± 0.10616	0.24669 ± 0.04921	10.03567 ± 38.12063	0 ± 0	0 ± 0
Reduced Chi-Sq	6.81414E-6	2.15657E-7	3.7049E-6	6.09794E-6	1.33437E-7	2.12406E-7	1.0589E-8
R-Square (COD)	0.99998	0.99999	0.99973	0.99963	0.99993	0.99987	0.9999
Adj. R-Square	0.99998	0.99998	0.99969	0.99958	0.99992	0.99985	0.99988

Figure S22. Dual-site Langmuir fits of various adsorption isotherms for MUF-16(Mn) at 293 K.

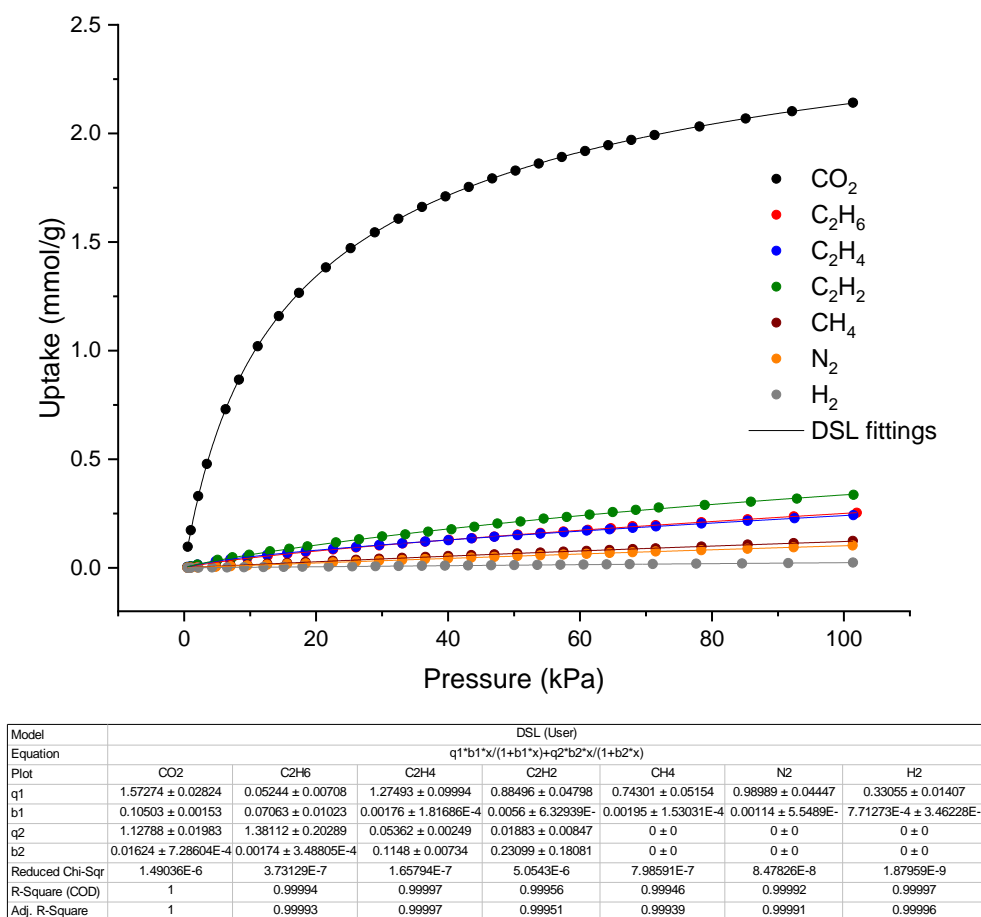


Figure S23. Dual-site Langmuir fits of various adsorption isotherms for MUF-16(Ni) at 293 K.

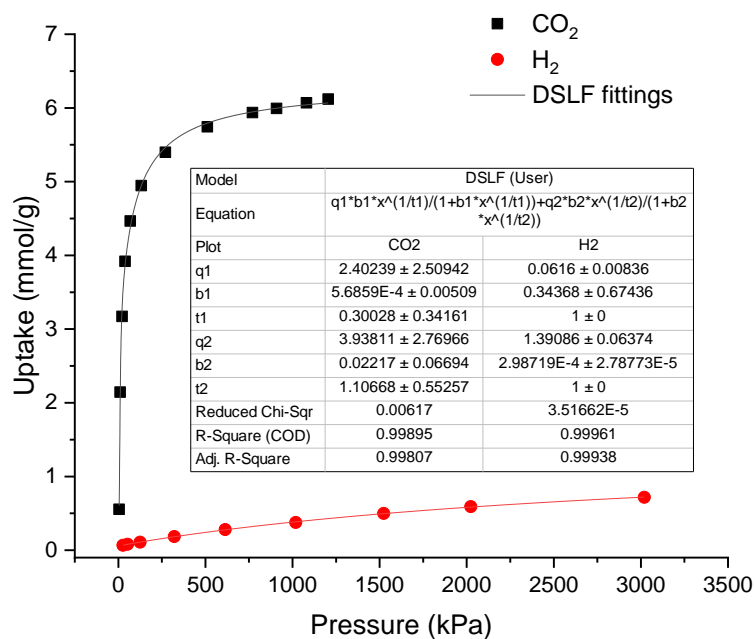


Figure S24. Dual-site Langmuir Freundlich fits for Zeolite 13X at 313 K. Isotherm data were taken from ¹⁰.

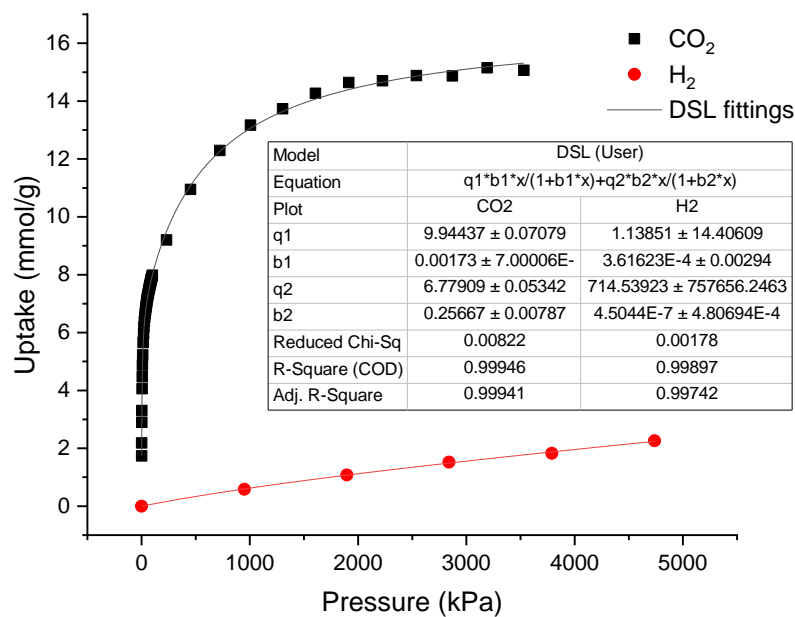


Figure S25. Dual-site Langmuir Freundlich fits for Mg-dobdc at 313 K. Isotherm data were taken from ¹¹.

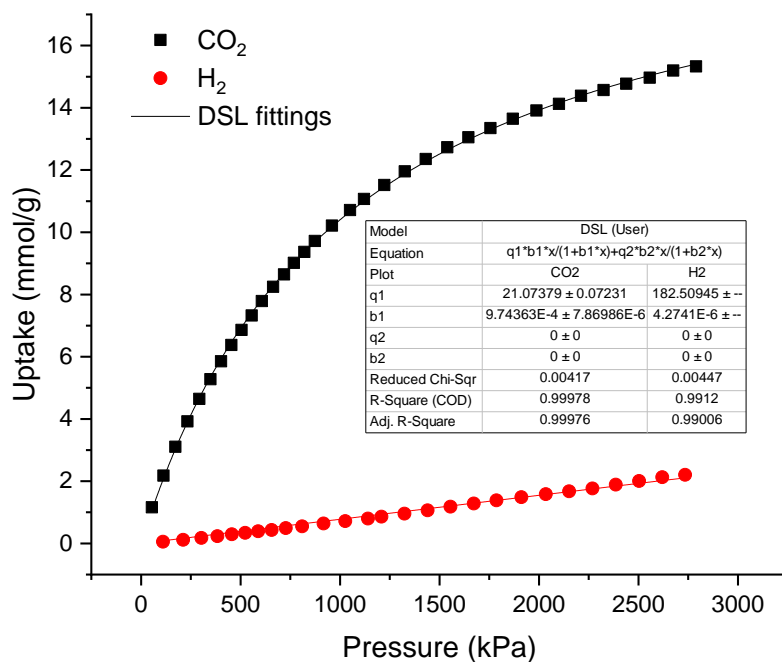


Figure S26. Dual-site Langmuir Freundlich fits for Cu-BTtri at 313 K. Isotherm data were taken from ¹¹.

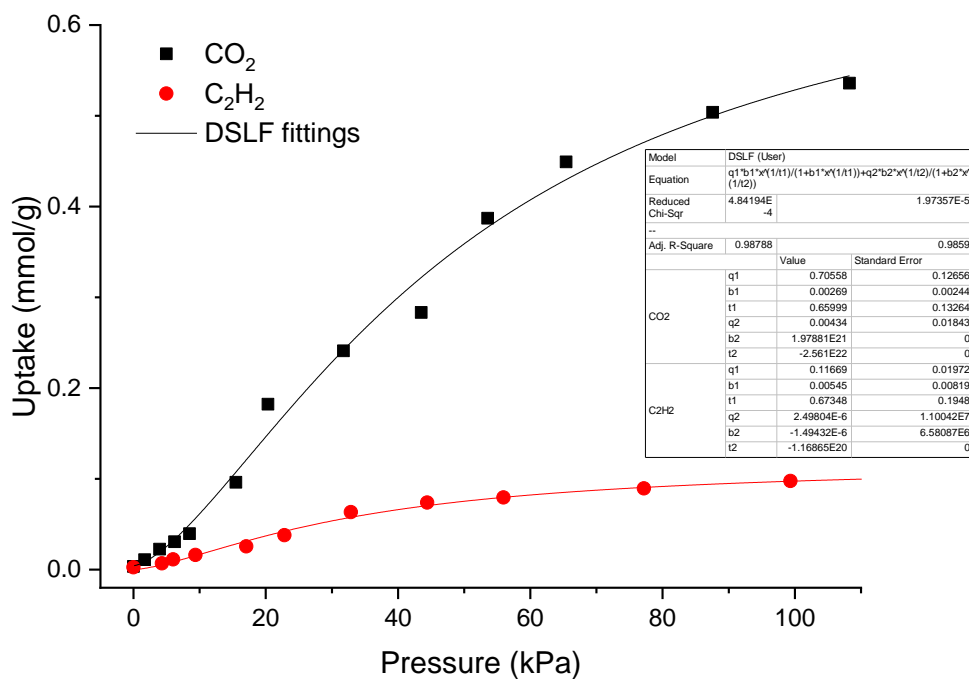


Figure S27. Dual-site Langmuir Freundlich fits for $K_2[Cr_3O(OOCH)_6(4\text{-ethylpyridine})_3]_2[\alpha\text{-SiW}_{12}O_{40}]$ at 278 K. Isotherm data were extracted from ⁴ using a digitizer software.

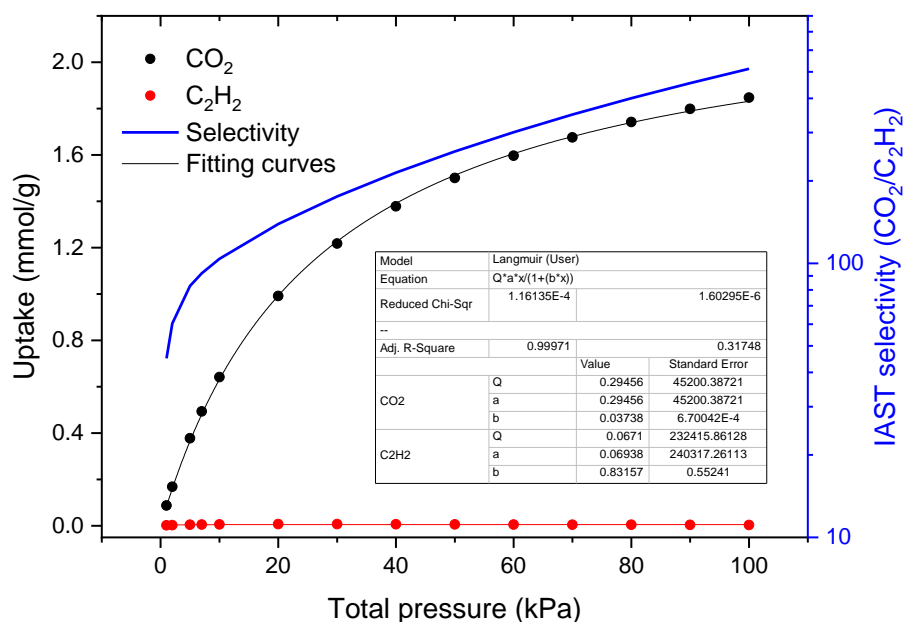


Figure S28. Mixed-gas isotherms and selectivity of MUF-16 predicted by IAST for a mixture of 50/50 CO_2/C_2H_2 at 293 K.

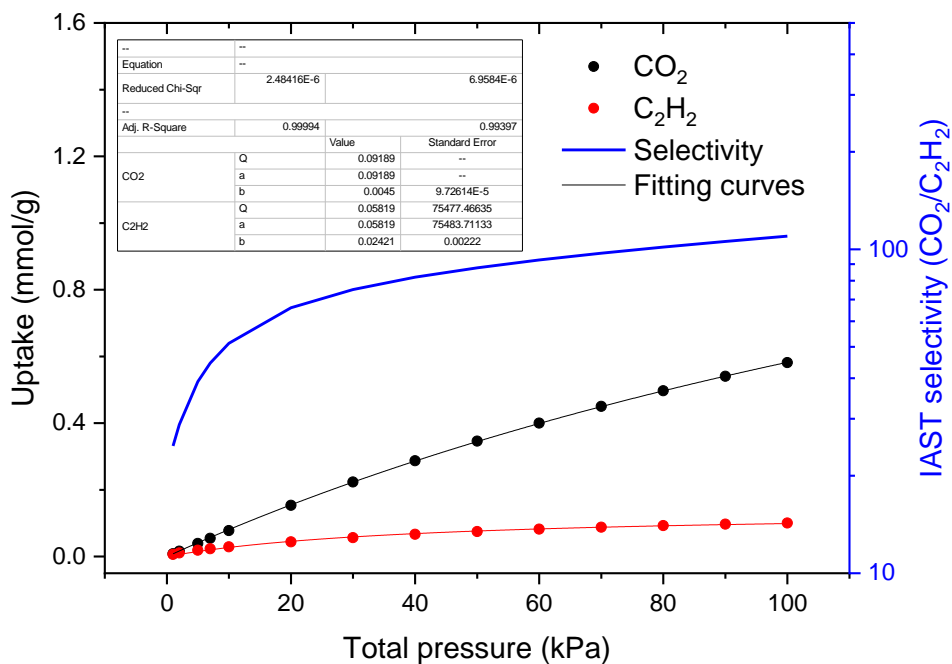


Figure S29. Mixed-gas isotherms and selectivity of MUF-16 predicted by IAST for a mixture of 5/95 CO₂/C₂H₂ at 293 K.

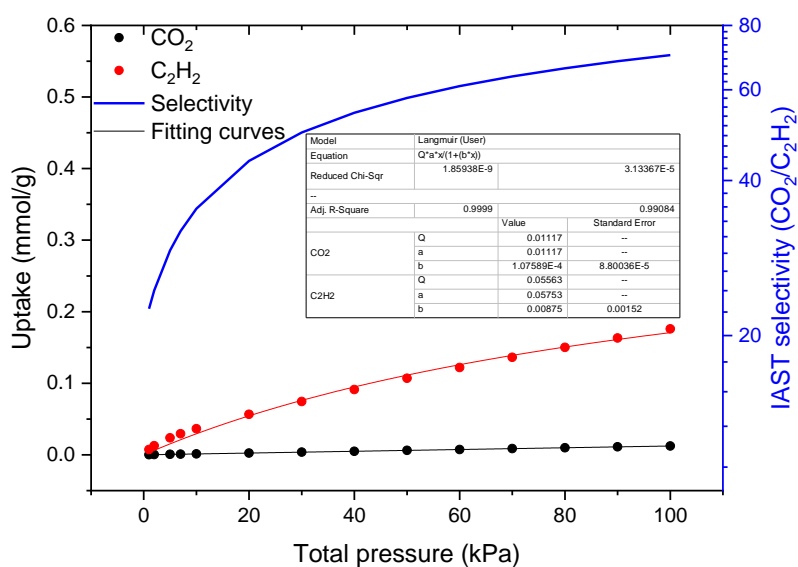


Figure S30. Mixed-gas isotherms and selectivity of MUF-16 predicted by IAST for a mixture of 0.1/99.9 CO₂/C₂H₂ at 293 K.

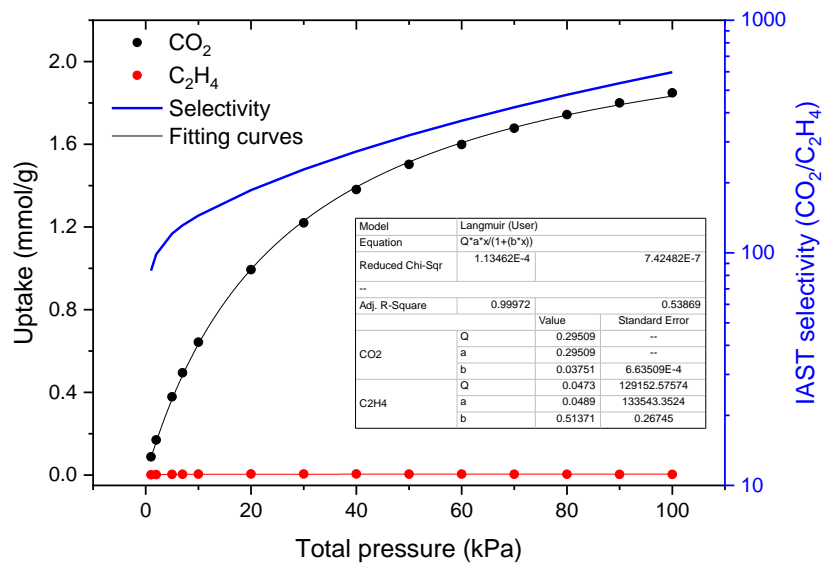


Figure S31. Mixed-gas isotherms and selectivity of MUF-16 predicted by IAST for a mixture of 50/50 $\text{CO}_2/\text{C}_2\text{H}_4$ at 293 K.

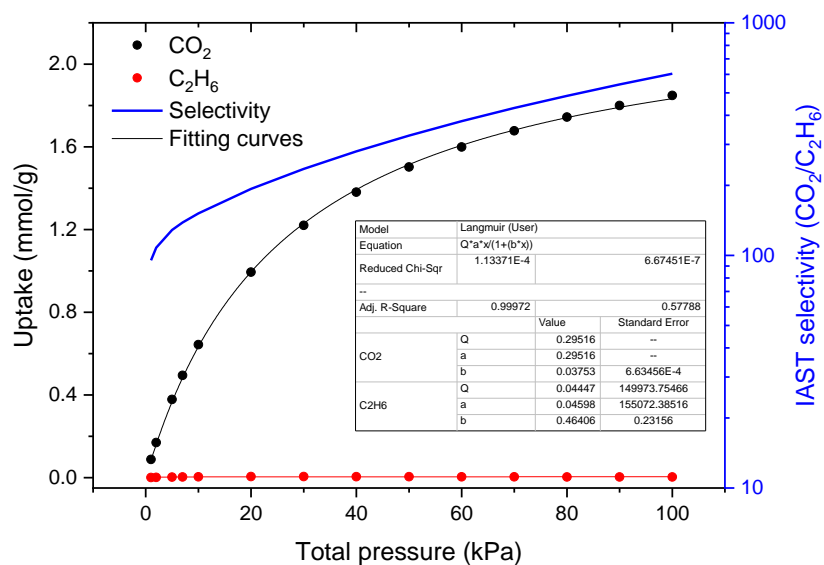


Figure S32. Mixed-gas isotherms and selectivity of MUF-16 predicted by IAST for a mixture of 50/50 $\text{CO}_2/\text{C}_2\text{H}_6$ at 293 K.

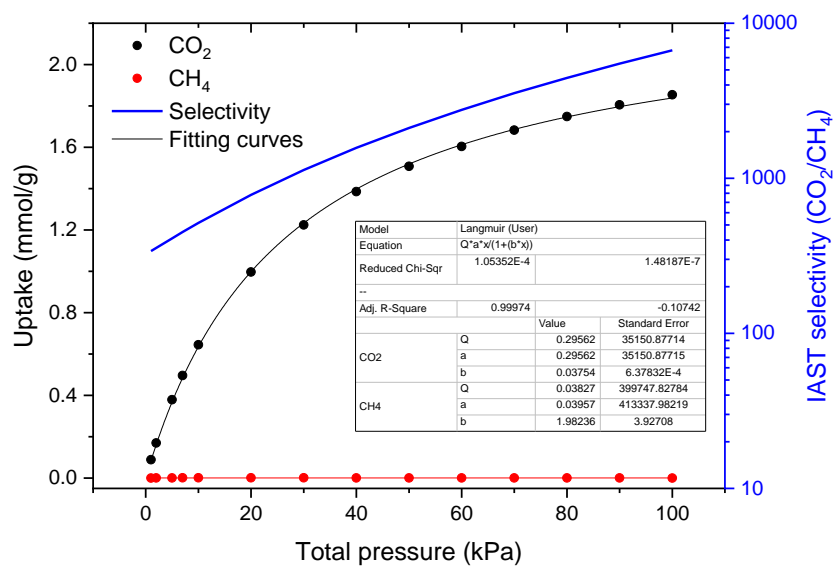


Figure S33. Mixed-gas isotherms and selectivity of MUF-16 predicted by IAST for a mixture of 50/50 CO₂/CH₄ at 293 K.

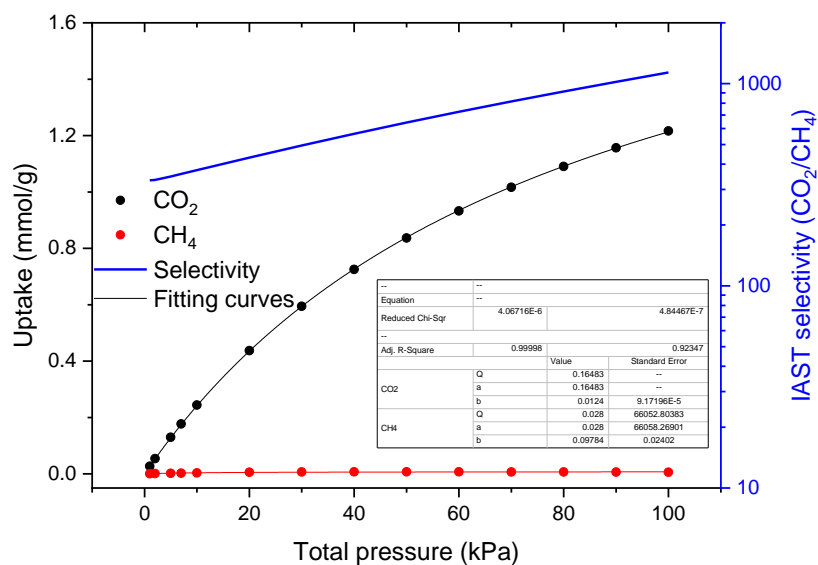


Figure S34. Mixed-gas isotherms and selectivity of MUF-16 predicted by IAST for a mixture of 15/85 CO₂/CH₄ at 293 K.

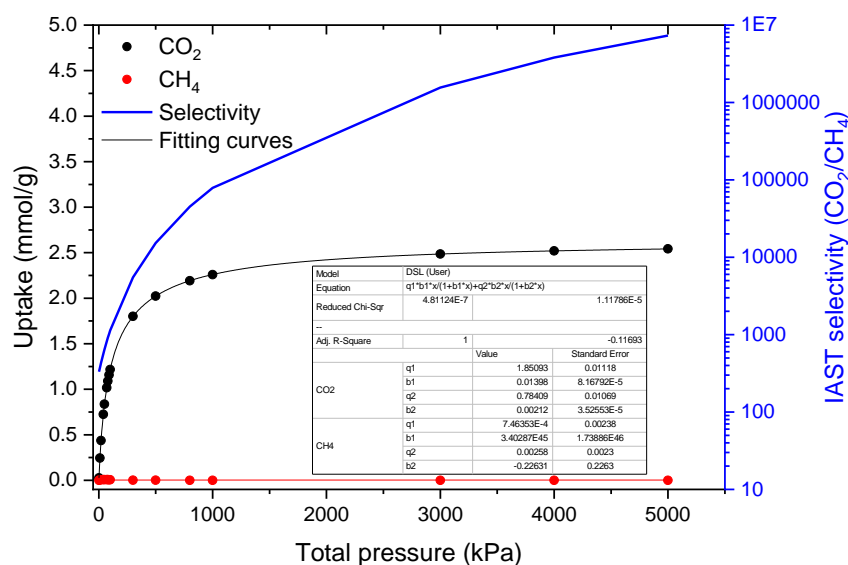


Figure S35. Mixed-gas isotherms and selectivity of MUF-16 predicted by IAST for a mixture of 15/85 CO₂/CH₄ at 293 K up to 50 bar.

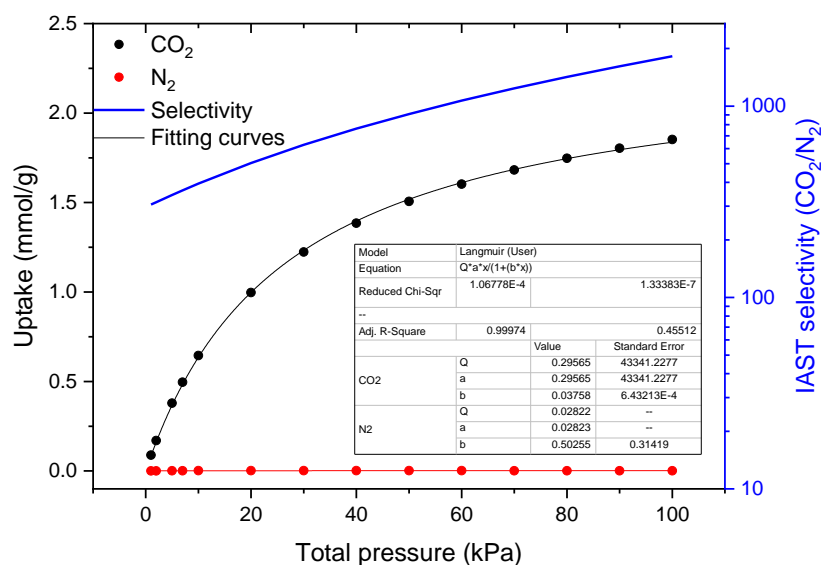


Figure S36. Mixed-gas isotherms and selectivity of MUF-16 predicted by IAST for a mixture of 50/50 CO₂/N₂ at 293 K.

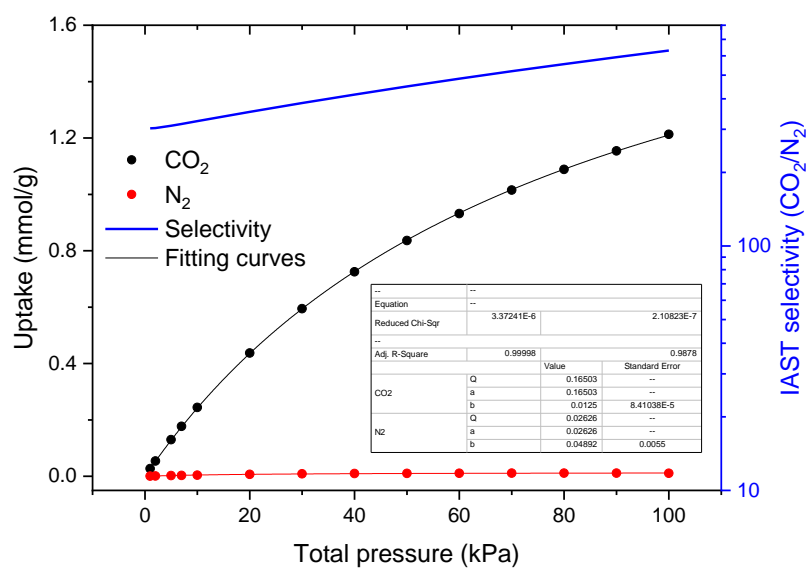


Figure S37. Mixed-gas isotherms and selectivity of MUF-16 predicted by IAST for a mixture of 15/85 CO_2/N_2 at 293 K.

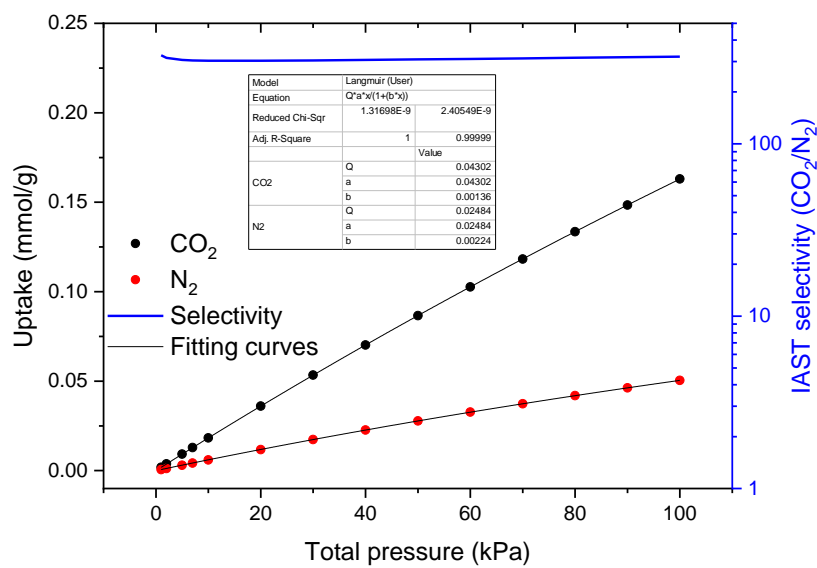


Figure S38. Mixed-gas isotherms and selectivity of MUF-16 predicted by IAST for a mixture of 1/99 CO_2/N_2 at 293 K.

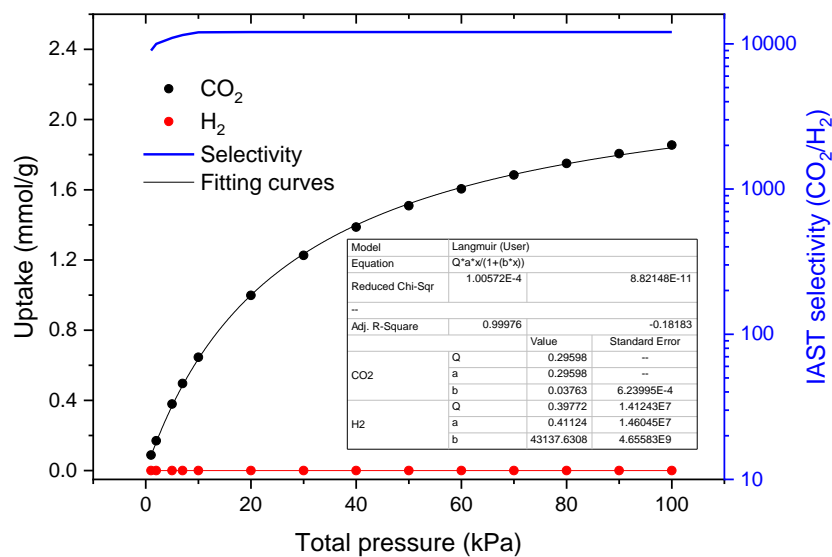


Figure S39. Mixed-gas isotherms and selectivity of MUF-16 predicted by IAST for a mixture of 50/50 CO₂/H₂ at 293 K.

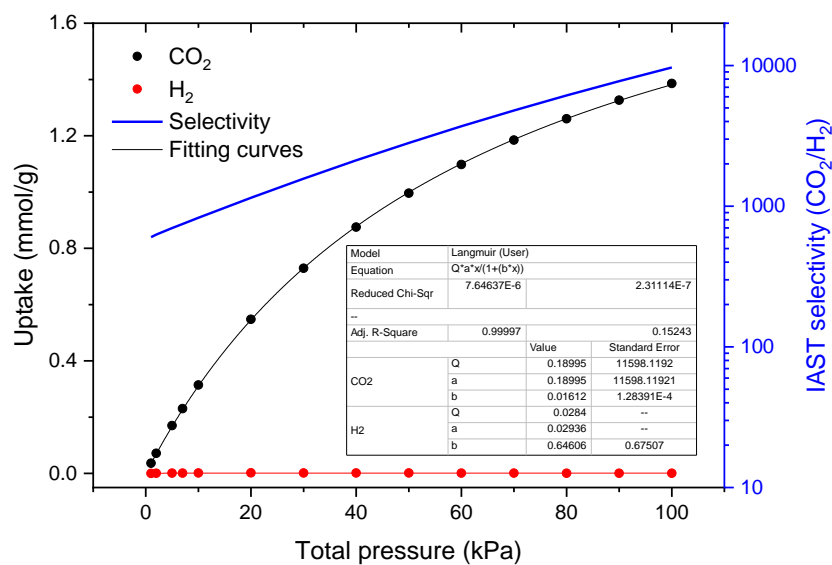


Figure S40. Mixed-gas isotherms and selectivity of MUF-16 predicted by IAST for a mixture of 20/80 CO₂/H₂ at 293 K.

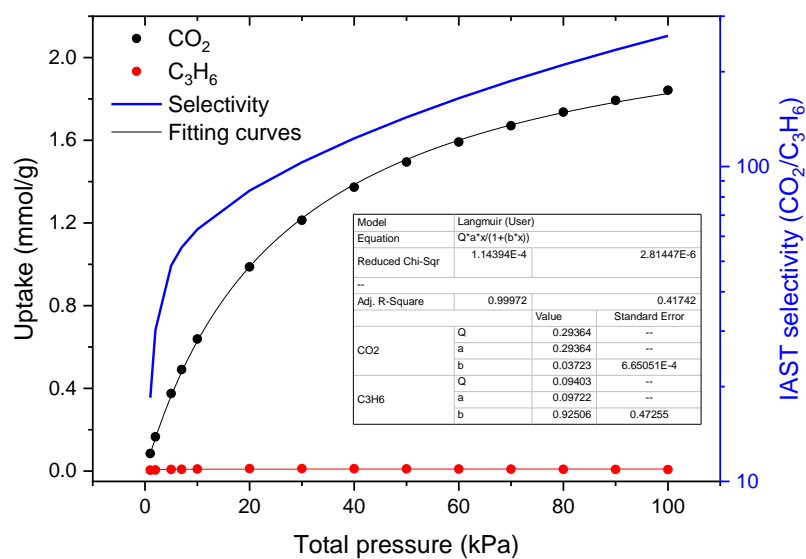


Figure S41. Mixed-gas isotherms and selectivity of MUF-16 predicted by IAST for a mixture of 50/50 $\text{CO}_2/\text{C}_3\text{H}_6$ at 293 K.

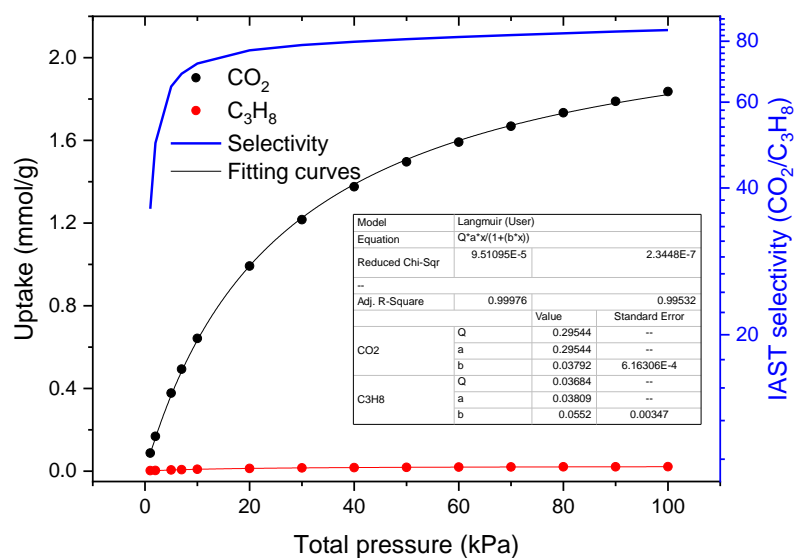


Figure S42. Mixed-gas isotherms and selectivity of MUF-16 predicted by IAST for a mixture of 50/50 $\text{CO}_2/\text{C}_3\text{H}_8$ at 293 K.

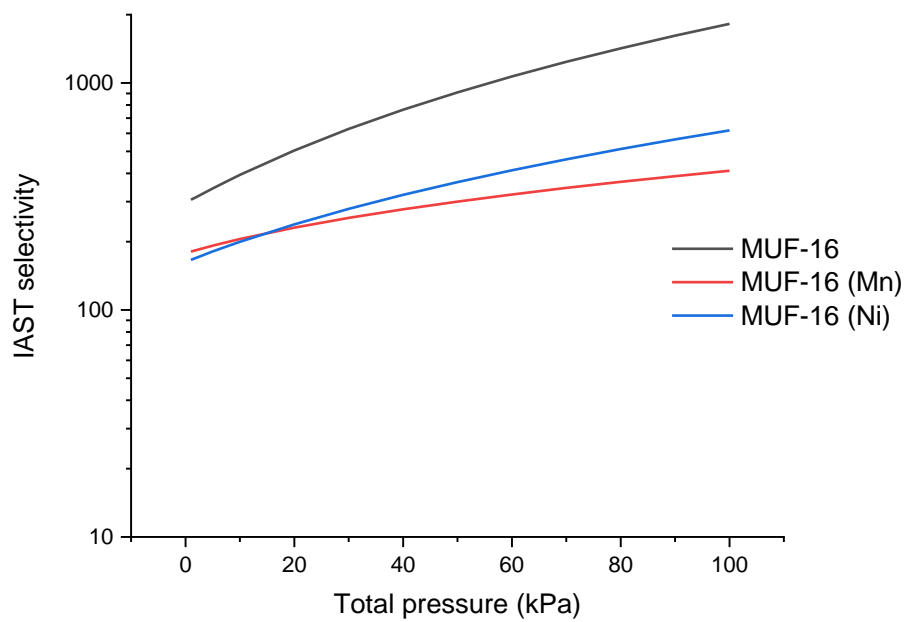


Figure S43. IAST selectivity for a 50/50 mixture of CO₂/N₂ at 293 K for the MUF-16 family.

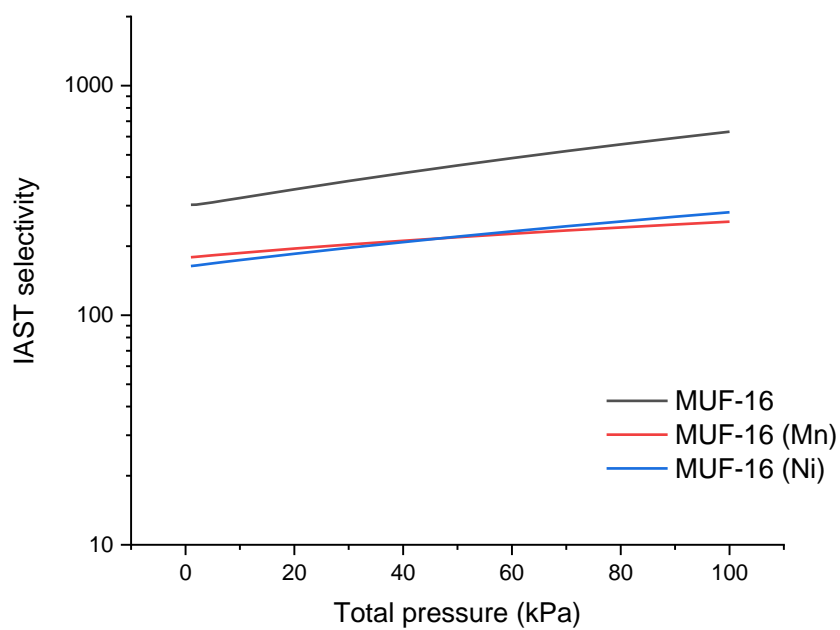


Figure S44. IAST selectivity for a 15/85 mixture of CO₂/N₂ at 293 K for the MUF-16 family.

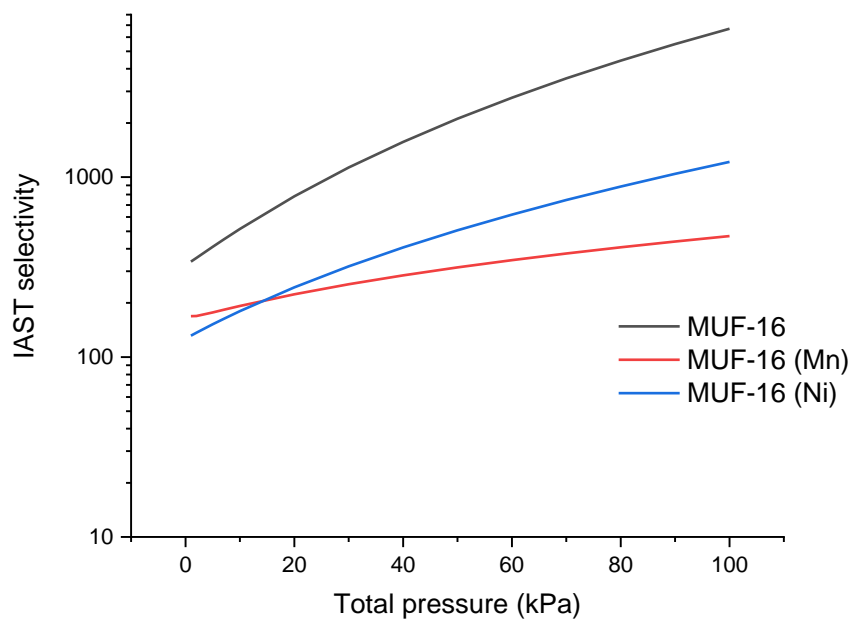


Figure S45. IAST selectivity for a 50/50 mixture of CO₂/CH₄ at 293 K for the MUF-16 family.

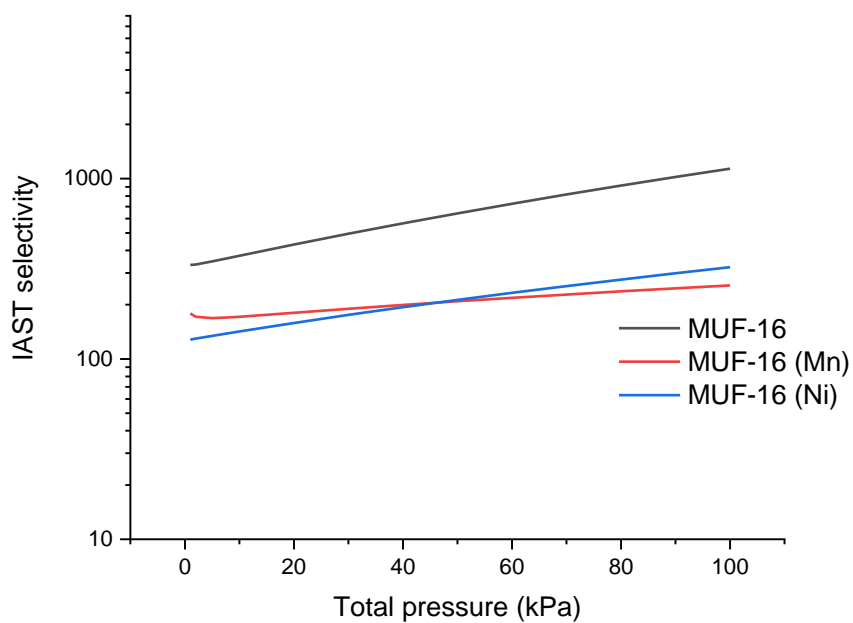


Figure S46. IAST selectivity for a 15/85 mixture of CO₂/N₂ at 293 K for the MUF-16 family.

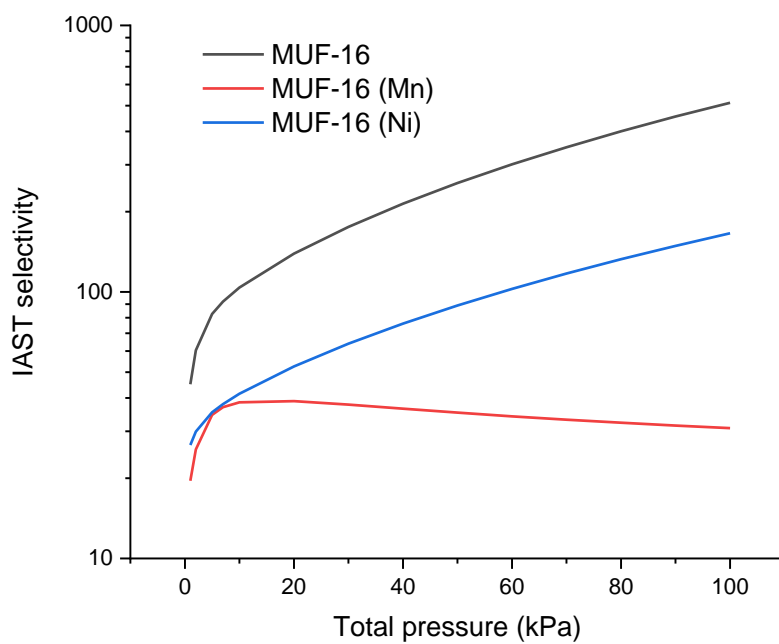


Figure S47. IAST selectivity for a 50/50 mixture of $\text{CO}_2/\text{C}_2\text{H}_2$ at 293 K for the MUF-16 family.

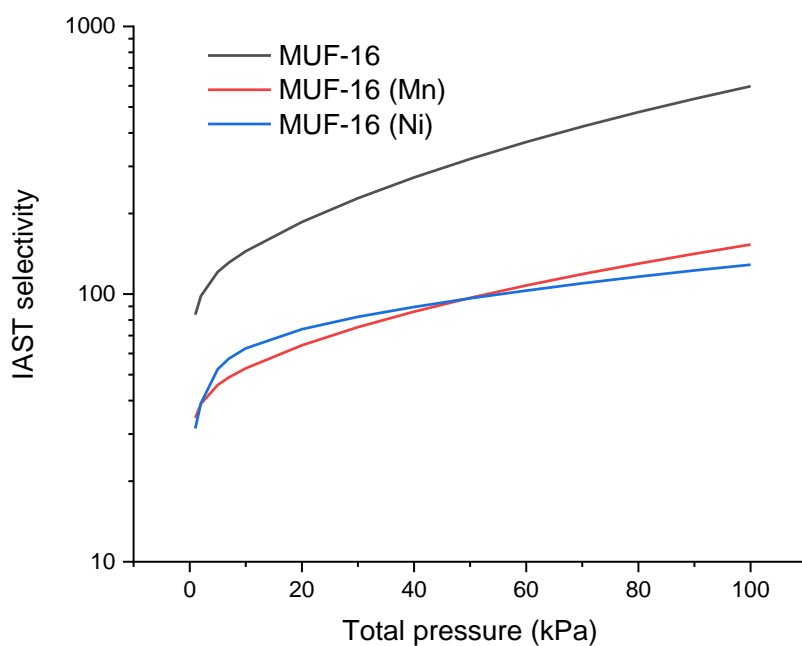


Figure S48. IAST selectivity for a 50/50 mixture of $\text{CO}_2/\text{C}_2\text{H}_4$ at 293 K for the MUF-16 family.

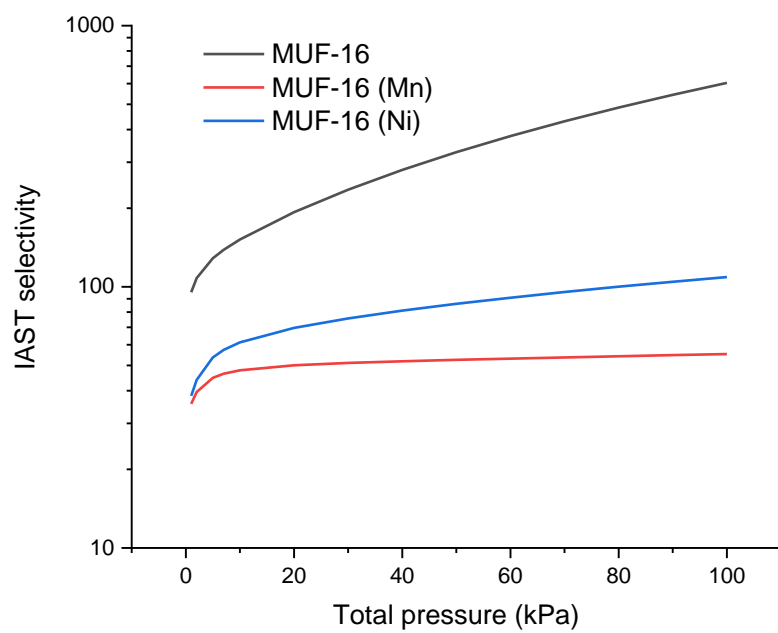


Figure S49. IAST selectivity for a 50/50 mixture of $\text{CO}_2/\text{C}_2\text{H}_6$ at 293 K for the MUF-16 family.

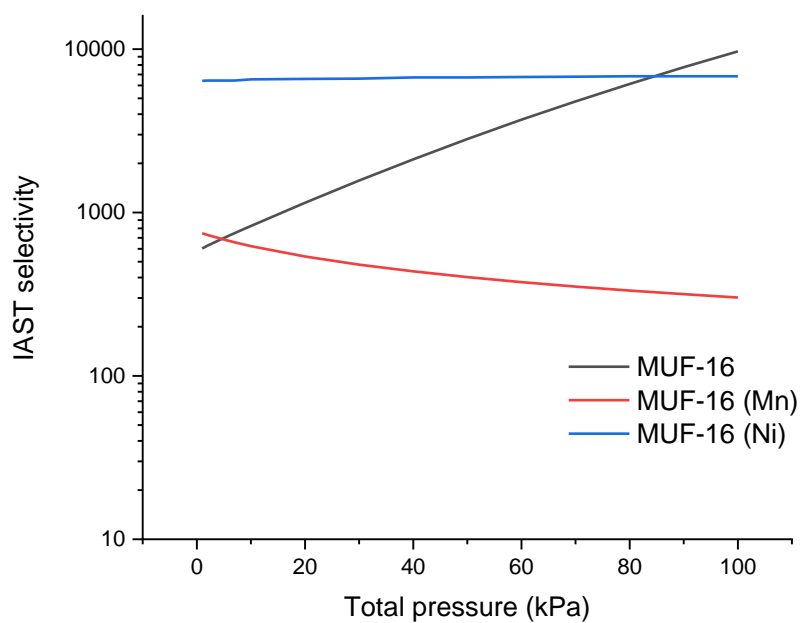


Figure S50. IAST selectivity for a 50/50 mixture of CO_2/H_2 at 293 K for the MUF-16 family.

9. Breakthrough separation experiments and simulations

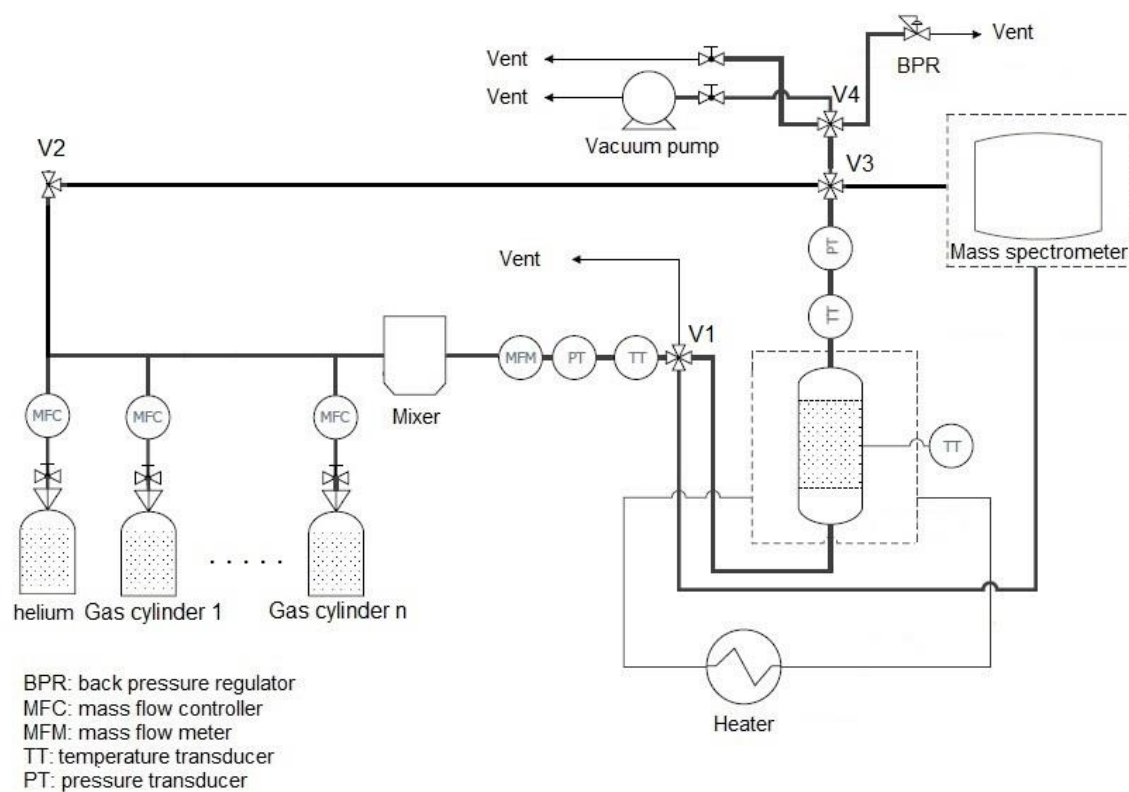


Figure S51. A schematic of the experimental column breakthrough setup.

Table S7. Summary of inlet gas feed streams, outlet compositions and associated data for experimental breakthrough tests using a MUF-16 adsorbent bed.

Gas mixture	Total pressure (bar)	Inlet CO ₂ partial pressure (bar)	Flowrate (mL _N /min)	Upper limit for CO ₂ concentration in effluent (ppmv)	Breakthrough point of CO ₂ (min)	CO ₂ concentration in effluent at breakthrough point (ppmv)	Dynamic adsorption capacity (mmol/g)	Equilibrium adsorption capacity (mmol/g)
CO ₂ /N ₂ (50/50)	1	0.5	6	500	10.6	600	1.57	1.85
CO ₂ /N ₂ (15/85)	1	0.15	6	520	24.1	600	1.08	1.23
CO ₂ /N ₂ (1/99)	1	0.01	6	530	40.7	600	0.12	0.17
CO ₂ /N ₂ (0.4/99.6)	1	0.004	10	500	28.5	600	0.06	0.09
CO ₂ /CH ₄ (50/50)	1	0.5	6	500	10.6	600	1.53	1.85
CO ₂ /CH ₄ (15/85)	1	0.15	6	520	25.6	600	1.13	1.23
CO ₂ /CH ₄ (15/85)	9	0.15	6	360	44.8	600	2.01	-
CO ₂ /CH ₄ +C ₂ H ₆ +C ₃ H ₈ (15/80/4/1)	1	0.15	6	520	24.6	600	1.09	1.23
CO ₂ /CH ₄ +C ₂ H ₆ +C ₃ H ₈ (15/80/4/1)	9	0.15	6	390	42.5	600	1.93	-
CO ₂ /C ₂ H ₂ (50/50)*	1	0.33	6	500	12.3	600	1.23	1.64
CO ₂ /C ₂ H ₂ (5/95)	1	0.035	6.85	540	15.1	600	0.18	0.46
CO ₂ /C ₂ H ₄ (50/50)*	1	0.33	6	500	11.9	600	1.19	1.64
CO ₂ /C ₂ H ₆ (50/50)*	1	0.33	6	500	12.2	600	1.22	1.64
CO ₂ /H ₂ (50/50)	1	0.5	6	500	10.8	600	1.62	1.85
CO ₂ /H ₂ (15/85)	1	0.5	6	510	24.4	600	1.11	1.85

9.1 CO₂/N₂, CO₂/CH₄, CO₂/H₂ and CO₂/CH₄+C₂H₆+C₃H₈ breakthrough separations

In a typical breakthrough experiment, activated MUF-16 (0.9 g) was placed in an adsorption column (6.4 mm in diameter \times 11 cm in length) to form a fixed bed. The adsorbent was activated at 130 °C under high vacuum for 7 hours and then the column was left under vacuum for another 3 hours while being cooled to 20 °C. The column was then purged under a 20 mL_N/min flow of He gas for 1 hr at 1.1 bar prior to the breakthrough experiment. A gas mixture containing different mixture of CO₂/N₂, CO₂/CH₄, CO₂/H₂ and CO₂/CH₄+C₂H₆+C₃H₈ was introduced to the column at 1.1 bar (and 9 bar for CO₂/CH₄ and CO₂/CH₄+C₂H₆+C₃H₈) and 20 °C. A feed flowrate of 6 mL_N/min (10 mL_N/min for 0.4/99.6 CO₂/N₂ mixture) was set. The operating pressure was controlled at 1.1 or 9 bar with a back-pressure regulator. The outlet composition was continuously monitored by a SRS UGA200 mass spectrometer. The CO₂ was deemed to have broken through from the column when its concentration reached 600 ppmv.

Regeneration experiment

The adsorbates (primarily CO₂) were stripped from the column to regenerate the adsorbent by purging with dry air at ambient temperature (20 °C) and a flow rate of 20 mL_N/min at 1.1 bar. The effluent from the adsorption bed was monitored by mass spectrometry to show that all of the CO₂ was removed at 20 °C over a period of around 25 minutes, with no further loss of CO₂ observed at 40, 60, 80 or 130 °C. For the recycling experiments, the adsorption bed was subsequently used to separate CO₂/N₂ 15/85 (6 mL/min) before being regenerated again with a flow of air. This process was repeated 200 times.

Alternatively, the adsorption bed could be regenerated under a dynamic vacuum (turbomolecular pump) for around 15-20 mins at room temperature, but this procedure was not typically employed.

9.1.1. Separation of CO₂/N₂

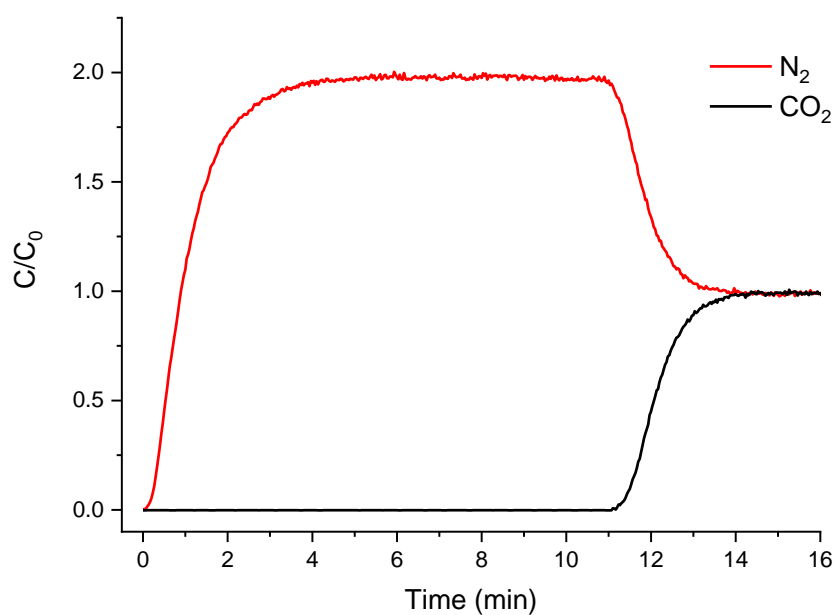


Figure S52. Experimental breakthrough curves for a mixture of 50/50 CO₂/N₂ at 1.1 bar and 293 K in an adsorption column packed with MUF-16.

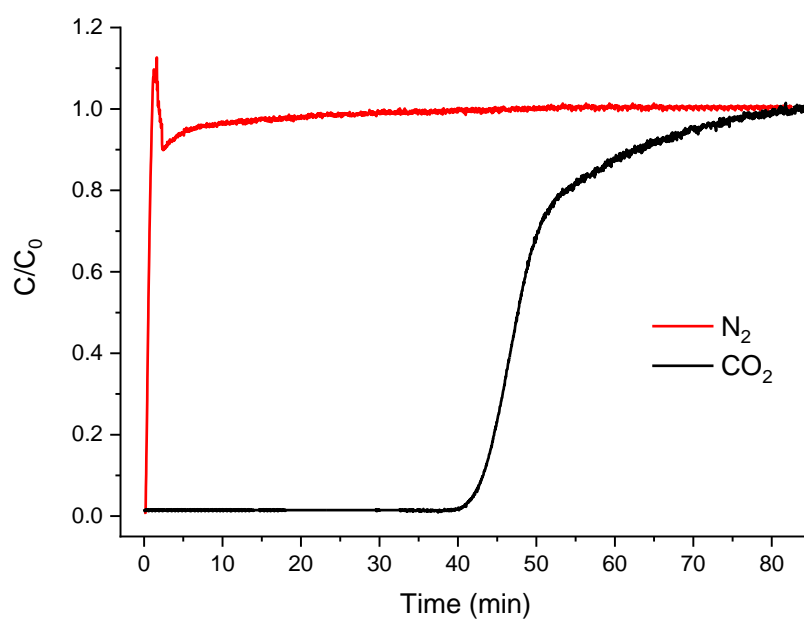


Figure S53. Experimental breakthrough curves for a mixture of 1/99 CO₂/N₂ at 1.1 bar and 293 K in an adsorption column packed with MUF-16.

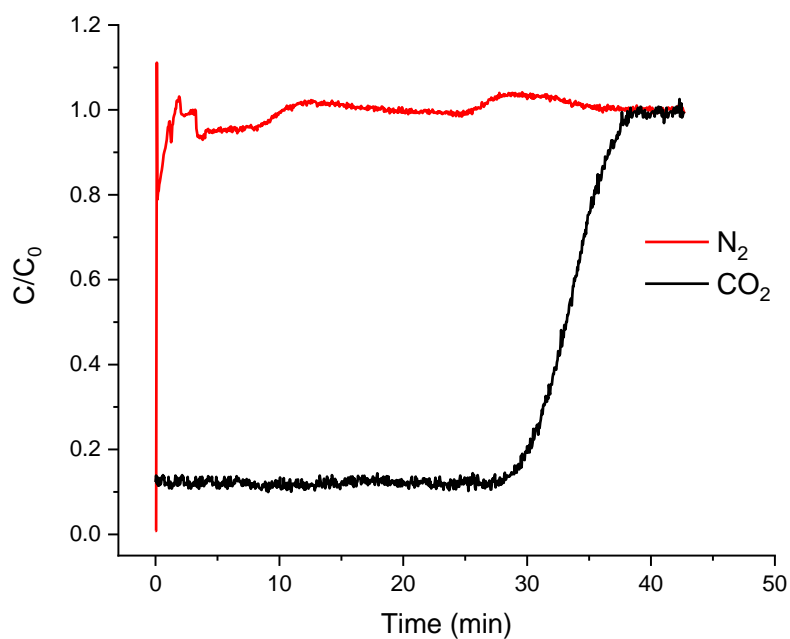


Figure S54. Experimental breakthrough curves for a mixture of 0.4/99.6 CO₂/N₂ at 1.1 bar and 293 K in an adsorption column packed with MUF-16.

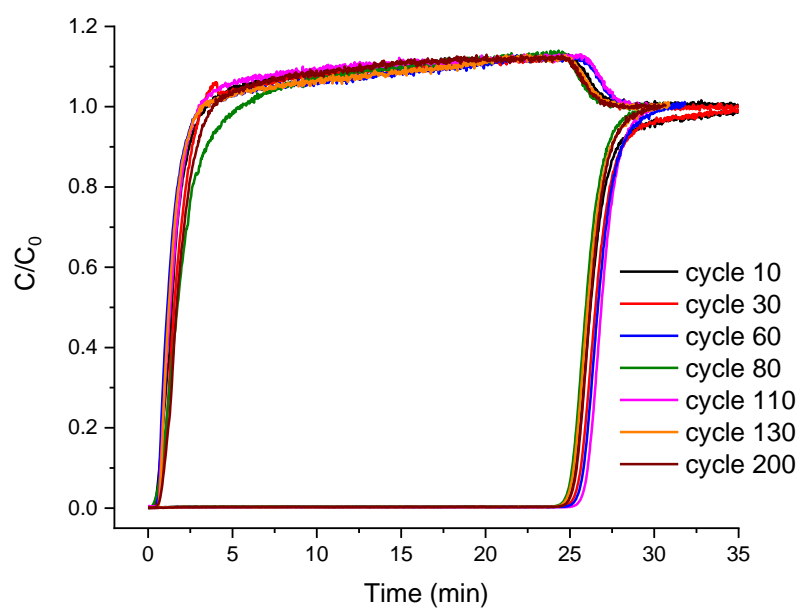


Figure S55. Breakthrough curves of CO₂/N₂ (15/85) mixture at different cycles at 293 K and 1.1 bar for MUF-16.

9.1.2. Separation of CO₂/H₂

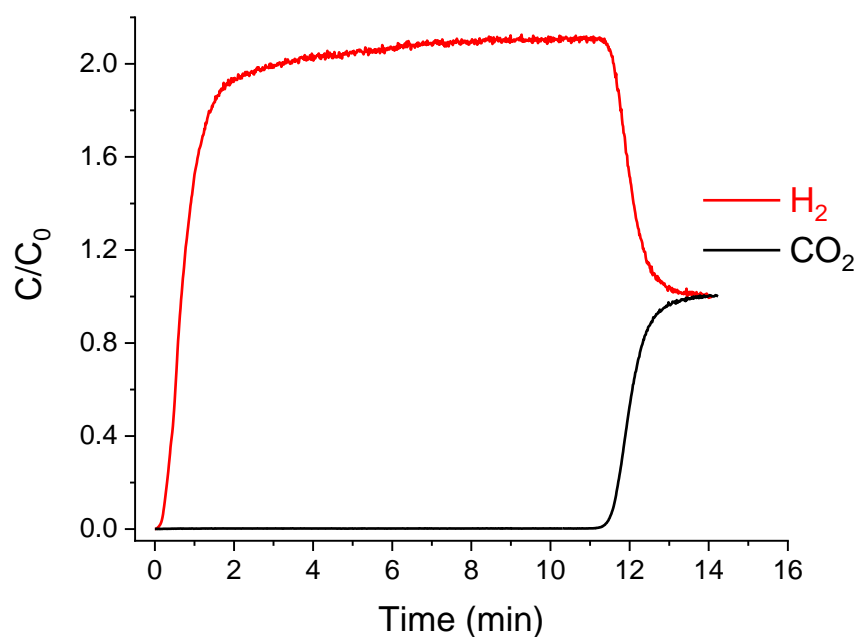


Figure S56. Experimental breakthrough curves for a mixture of 50/50 CO₂/H₂ at 1.1 bar and 293 K in an adsorption column packed with MUF-16.

9.1.3 Separation of CO₂/CH₄ and CO₂/CH₄+C₂H₆+C₃H₈

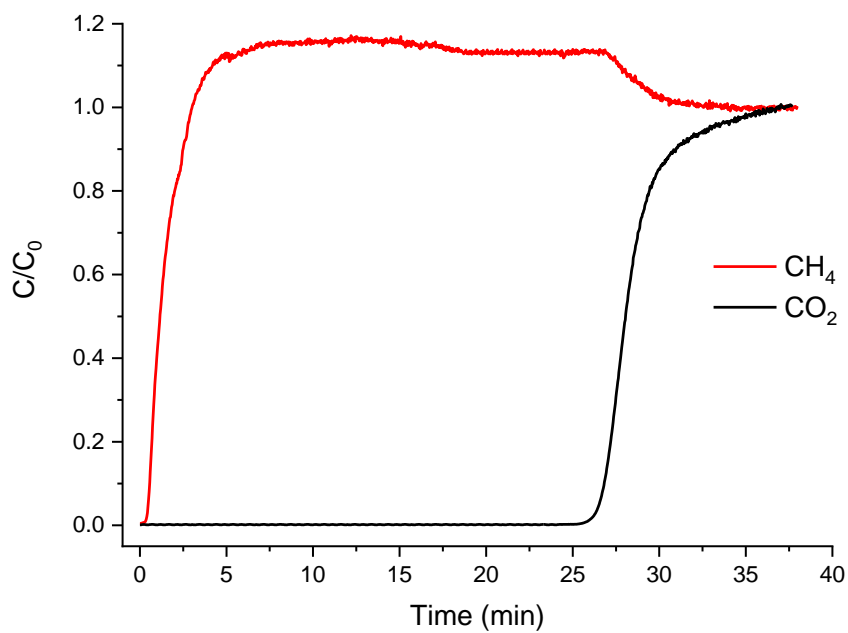


Figure S57. Experimental breakthrough curves for a mixture of 15/85 CO₂/CH₄ at 1.1 bar and 293 K in an adsorption column packed with MUF-16.

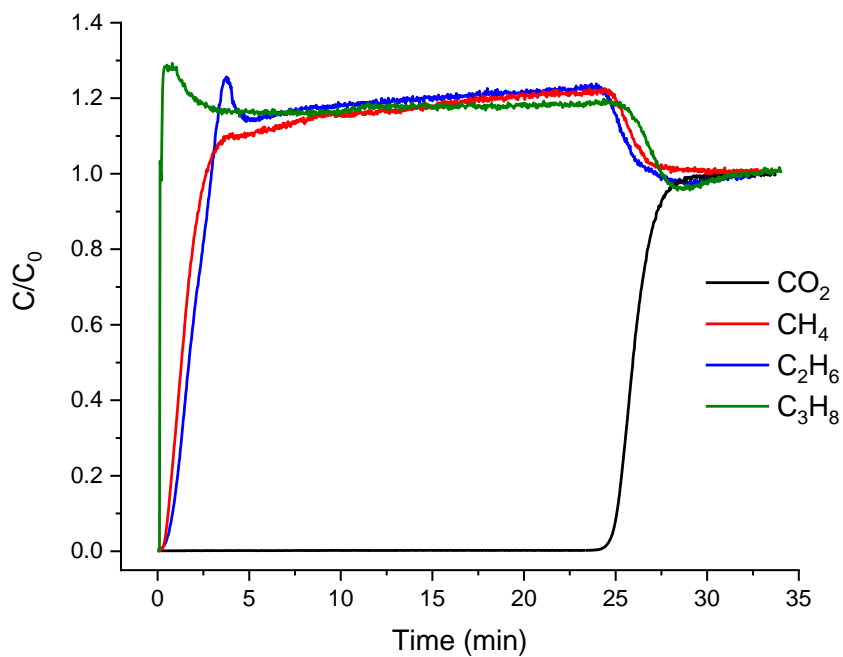


Figure S58. Experimental breakthrough curves for a mixture of 15/80/4/1 $\text{CO}_2/\text{CH}_4/\text{C}_2\text{H}_6/\text{C}_3\text{H}_8$ at 1.1 bar and 293 K in an adsorption column packed with MUF-16.

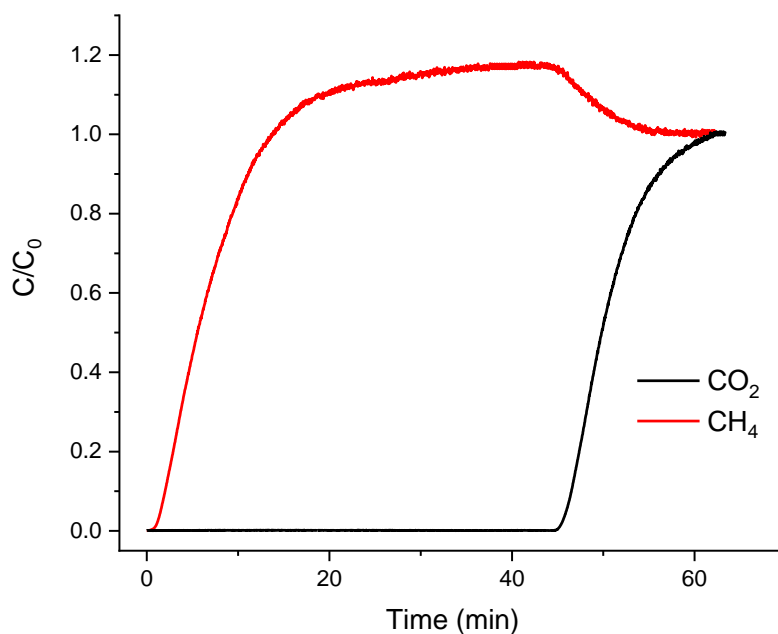


Figure S59. Experimental breakthrough curves for a mixture of 15/85 CO_2/CH_4 at 9 bar and 293 K in an adsorption column packed with MUF-16.

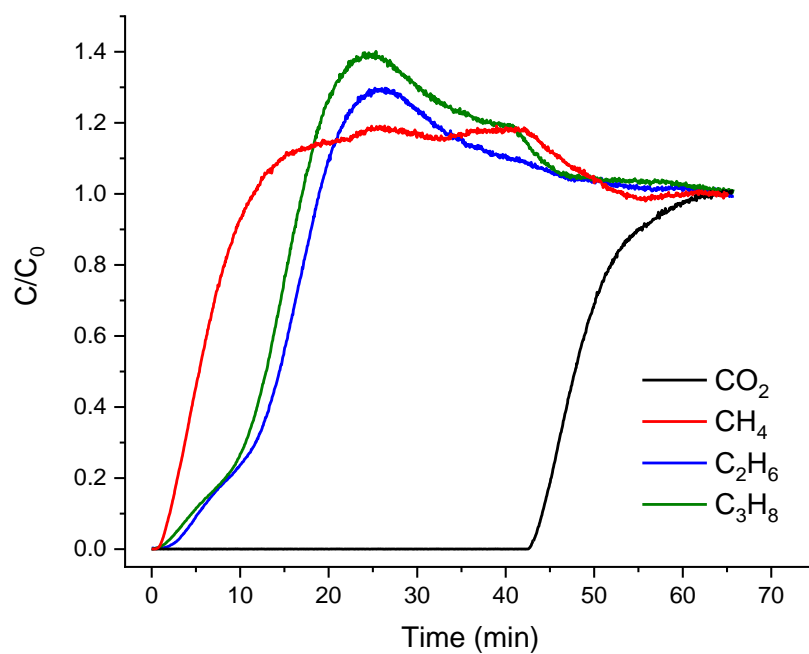


Figure S60. Experimental breakthrough curves for a mixture of 15/80/4/1 CO₂/CH₄/C₂H₆/C₃H₈ at 9 bar and 293 K in an adsorption column packed with MUF-16.

9.1.4. Simulations of CO₂/CH₄ breakthrough curves

The simulation of breakthrough curves was carried out using a previously reported method.¹²⁻¹³ A value for the mass transfer coefficient (k) was obtained by empirical tuning the steepness of the predicted breakthrough curves to match the experimental curve. The mass transfer coefficient tuned in this way was later used to predict breakthrough curves for other feed mixtures and operating pressures. A summary of adsorption column parameters and feed characterizations are presented in Table S8.

Table S8. Adsorption column parameters and feed characterizations used for the simulations for MUF-16.

Adsorption bed	Feed
Length: 110 mm	Flow rate: 6 mL _N /min
Diameter: 6.4 mm	Temperature: 293 K
Amount of adsorbent in the bed: 0.9 g	Pressure: 1.1 bar
Adsorbent density: 1.674 g/cm ³	Carrier gas flow rate: No carrier gas was used
Adsorbent average radius: 0.2 mm	
k_{CO_2} : 0.029 s ⁻¹	
k_{CH_4} : 0.00021 s ⁻¹	

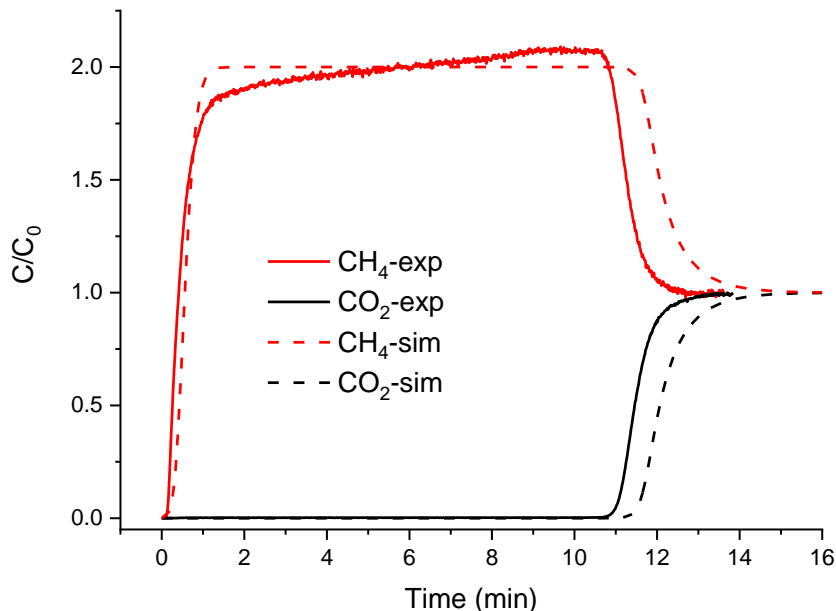


Figure S61. Experimental breakthrough curves in comparison to simulated one for a mixture of 50/50 CO₂/CH₄ at 1.1 bar and 293 K in an adsorption column packed with MUF-16.

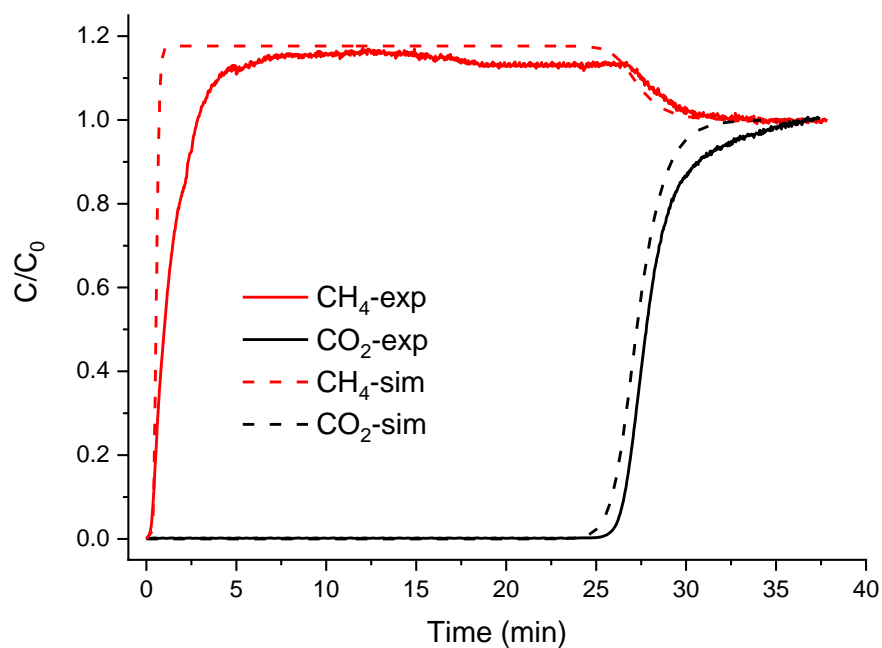


Figure S62. Experimental breakthrough curves in comparison to simulated one for a mixture of 15/85 CO₂/CH₄ at 1.1 bar and 293 K in an adsorption column packed with MUF-16.

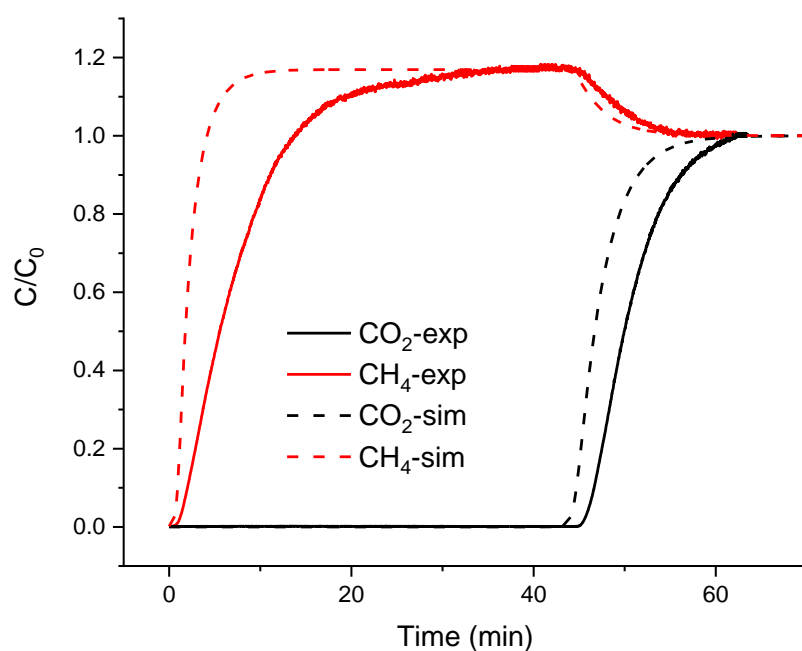


Figure S63. Experimental breakthrough curves in comparison to simulated one for a mixture of 15/85 CO₂/CH₄ at 9 bar and 293 K in an adsorption column packed with MUF-16.

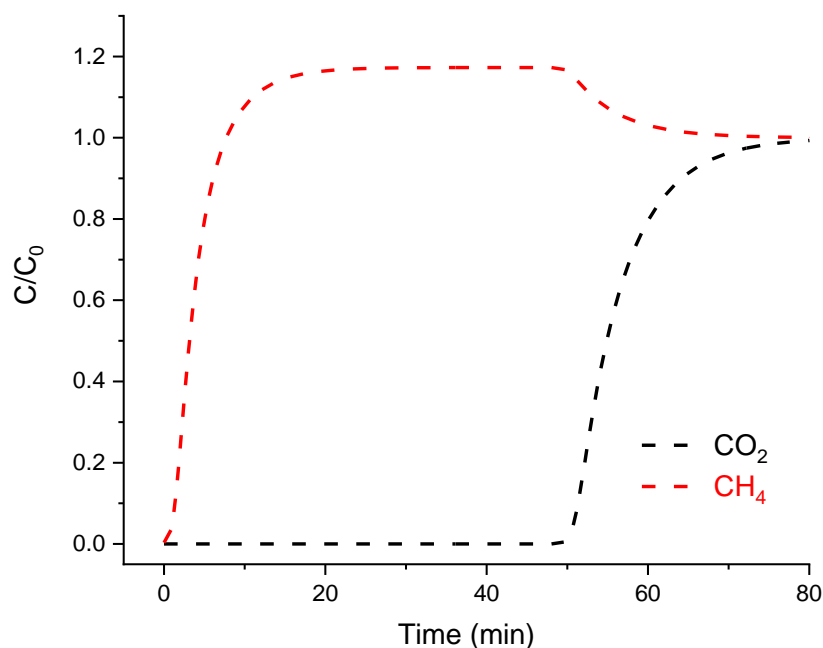


Figure S64. Simulated breakthrough curves for a mixture of 15/85 CO₂/CH₄ at 50 bar and 293 K in an adsorption column packed with MUF-16.

9.2 CO₂/C₂ hydrocarbon separations

In a typical breakthrough experiment, 0.9 g of activated MUF-16 was placed in an adsorption column (6.4 mm in diameter \times 11 cm in length) to form a fixed bed. The adsorbent was activated at 130 °C under high vacuum for 7 hours and then the column was left under vacuum for another 3 hours while being cooled to 20 °C. The column was then purged under a 20 mL_N/min flow of He gas for 1 hr at 1.1 bar prior to the breakthrough experiment. A gas mixture containing different gas pairs of CO₂ and C₂H₂, C₂H₆ or C₂H₄ along with He as a carrier gas was introduced to the column at 1.1 bar and 20 °C. A feed flowrate of 6.0 or 6.85 mL_N/min (including helium) was set for the experiments with 50/50 and 5/95 mixture of gases, respectively, and the flowrate of He in the feed was kept constant at 2 mL_N/min for all the experiments. The operating pressure was controlled at 1.1 bar with a back-pressure regulator. The outlet composition was continuously monitored by a SRS UGA200 mass spectrometer. The CO₂ was deemed to have broken through from the column when its concentration reached 600 ppmv.

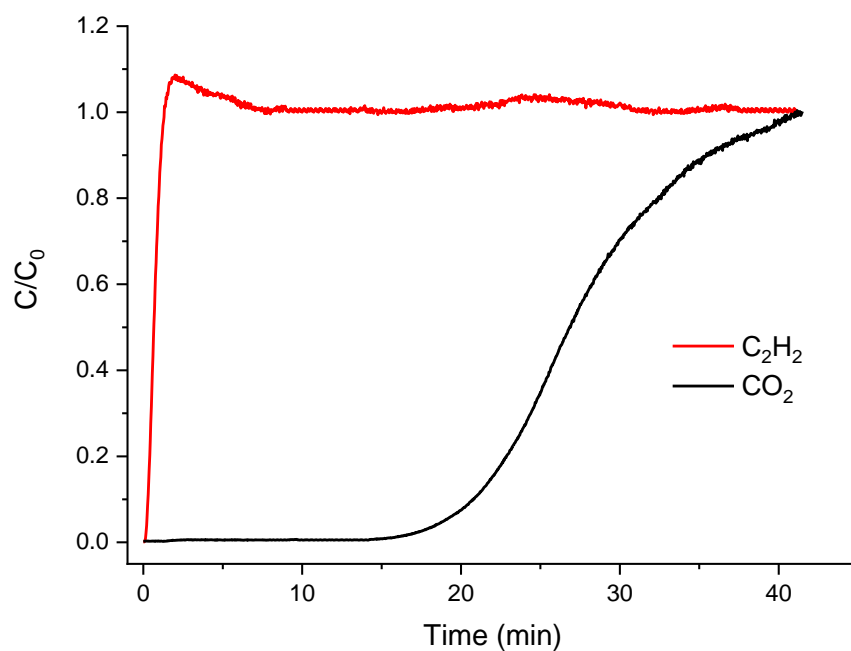


Figure S65. Experimental breakthrough curves for a mixture of 5/95 $\text{CO}_2/\text{C}_2\text{H}_2$ at 1.1 bar and 293 K in an adsorption column packed with MUF-16.

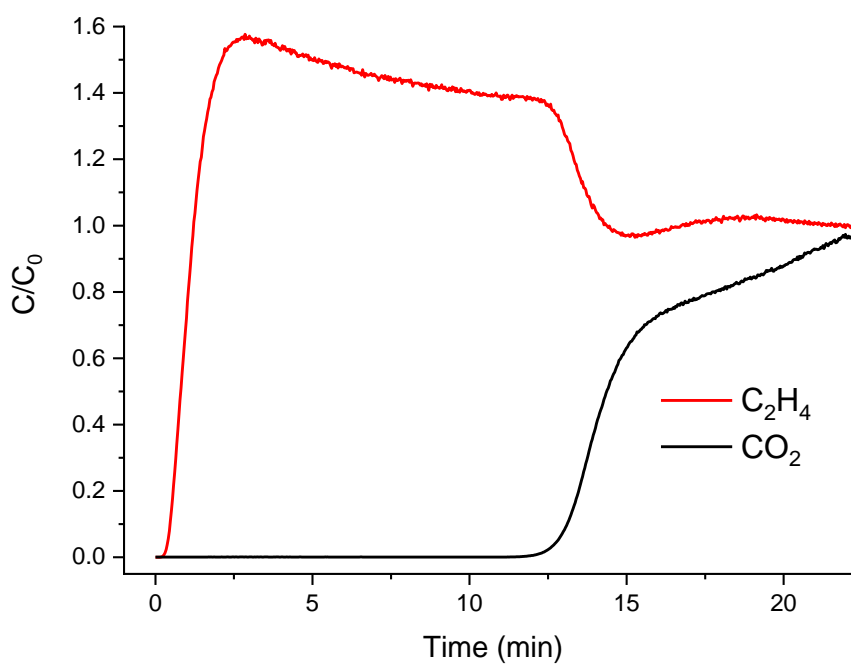


Figure S66. Experimental breakthrough curves for a mixture of 50/50 $\text{CO}_2/\text{C}_2\text{H}_4$ at 1.1 bar and 293 K in an adsorption column packed with MUF-16.

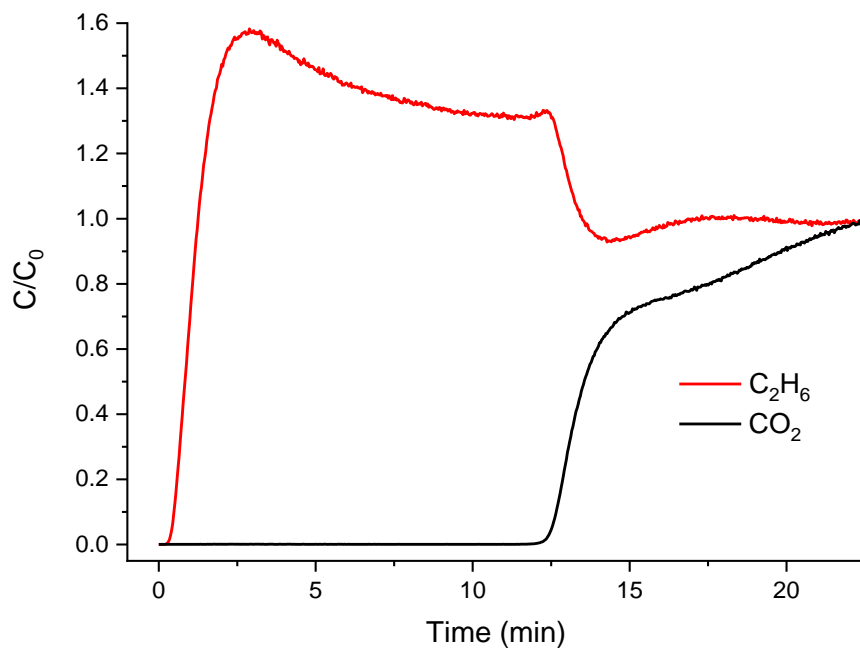


Figure S67. Experimental breakthrough curves for a mixture of 50/50 CO₂/C₂H₆ at 1.1 bar and 293 K in an adsorption column packed with MUF-16.

9.2.1. Simulations of CO₂/C₂H₂ breakthrough curves

The simulation of breakthrough curves for CO₂/C₂ hydrocarbons was carried out using the method reported above. A summary of adsorption column parameters and feed characterizations are presented in Table S9.

Table S9. Adsorption column parameters and feed characterizations used for the simulations for MUF-16.

<i>Adsorption bed</i>	<i>Feed</i>
Length: 110 mm	Flow rates:
Diameter: 6.4 mm	6 mL _N /min for equimolar and 0.1/99.9 mixtures, and 6.85
Amount of adsorbent in the bed: 0.9 g	mL _N /min for the 5/95 mixture.
Bed voidage: 0.84	Temperature: 293 K
Adsorbent average radius: 0.2 mm	Pressure: 1.1 bar
k _{CO2} : 0.021 s ⁻¹	Carrier gas (He) flow rate: 2 mL _N /min.
k _{C2H2} : 0.024 s ⁻¹	

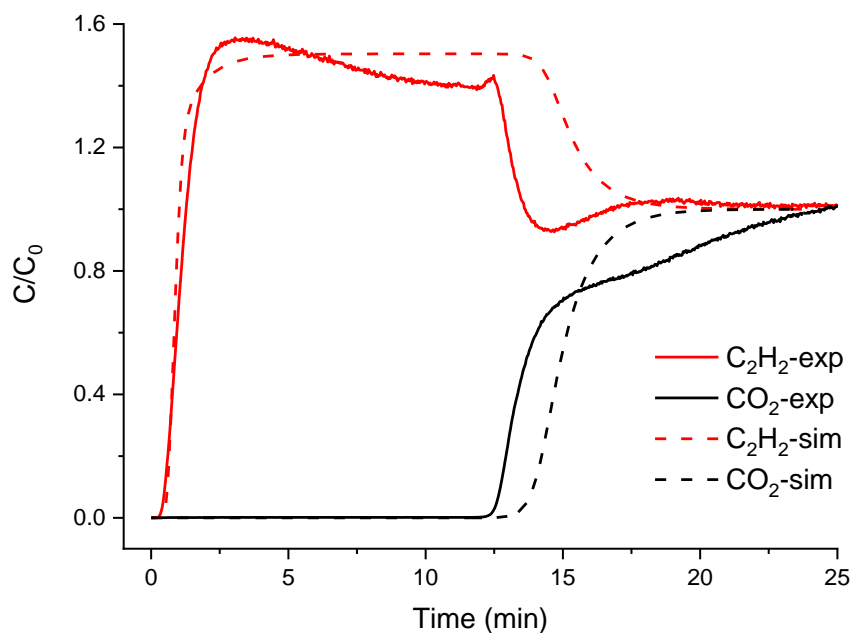


Figure S68. Experimental breakthrough curves in comparison to simulated one for a mixture of 50/50 $\text{CO}_2/\text{C}_2\text{H}_2$ at 1.1 bar and 293 K in an adsorption column packed with MUF-16.

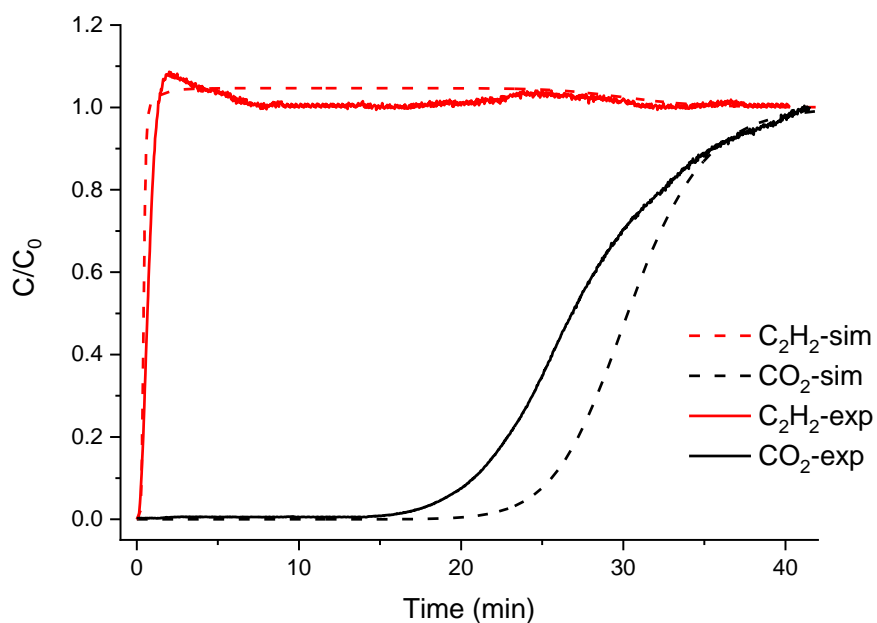


Figure S69. Experimental breakthrough curves in comparison to simulated one for a mixture of 5/95 $\text{CO}_2/\text{C}_2\text{H}_2$ at 1.1 bar and 293 K in an adsorption column packed with MUF-16.

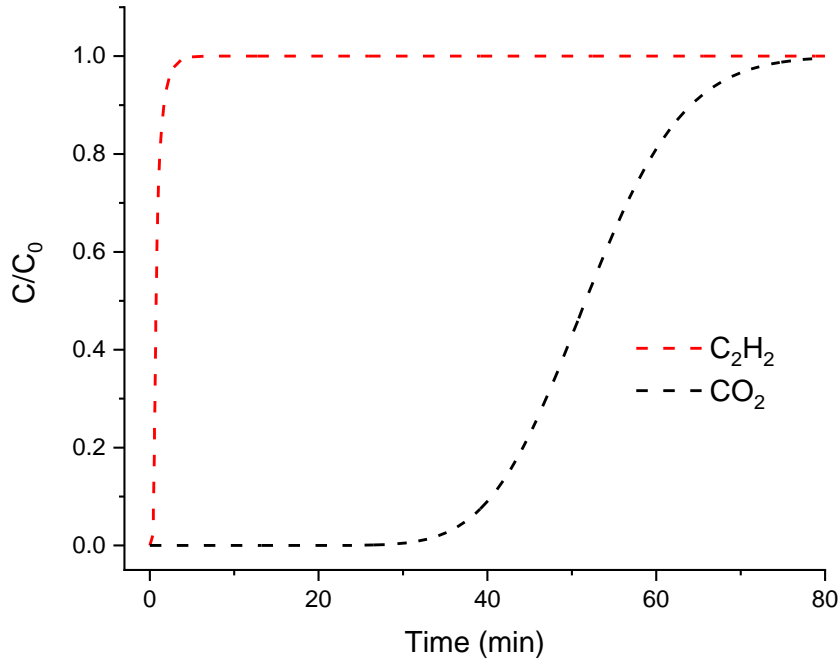


Figure S70. Simulated breakthrough curves for a mixture of 0.1/99.9 CO₂/C₂H₂ at 1.1 bar and 293 K in an adsorption column packed with MUF-16.

10. Heat of adsorption

Isosteric heat of adsorption (Q_{st})¹⁴ values were calculated from isotherms measured at 293K, 298K and 303 K for CO₂. The isotherms were first fit to a virial equation:

$$\ln P = \ln N + \frac{1}{T} \sum_{i=0}^m a_i N^i + \sum_{i=0}^n b_i N^i$$

Where N is the amount of gas adsorbed at the pressure P , a and b are virial coefficients, m and n are the number of coefficients require to adequately describe the isotherm. To calculate Q_{st} , the fitting parameters from the above equation were used for the following equation:

$$Q_{st} = -R \sum_{i=0}^m a_i N^i$$

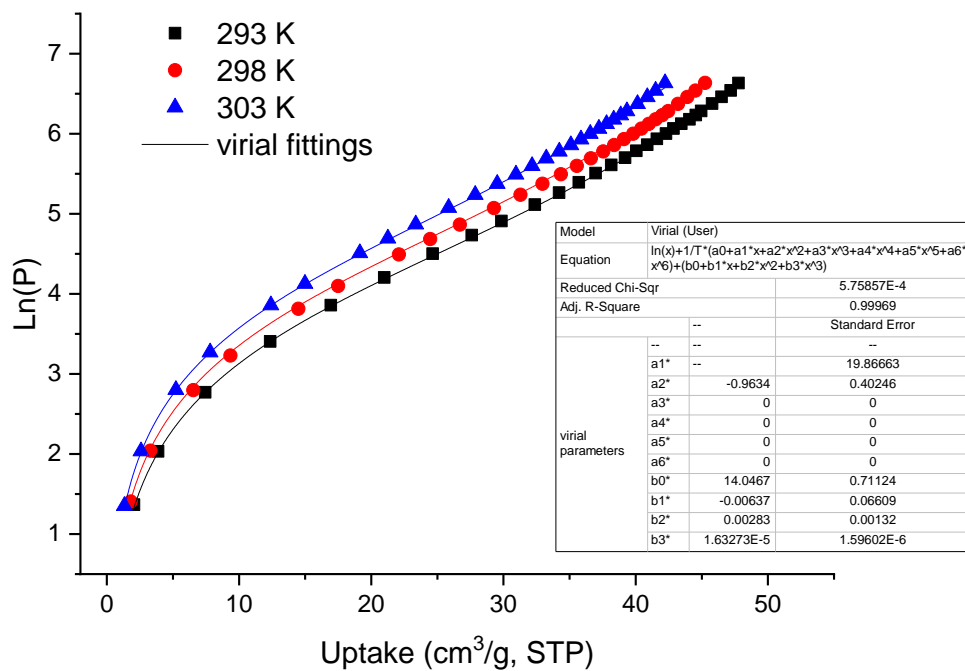


Figure S71. Virial equation fits for CO₂ adsorption isotherms of MUF-16.

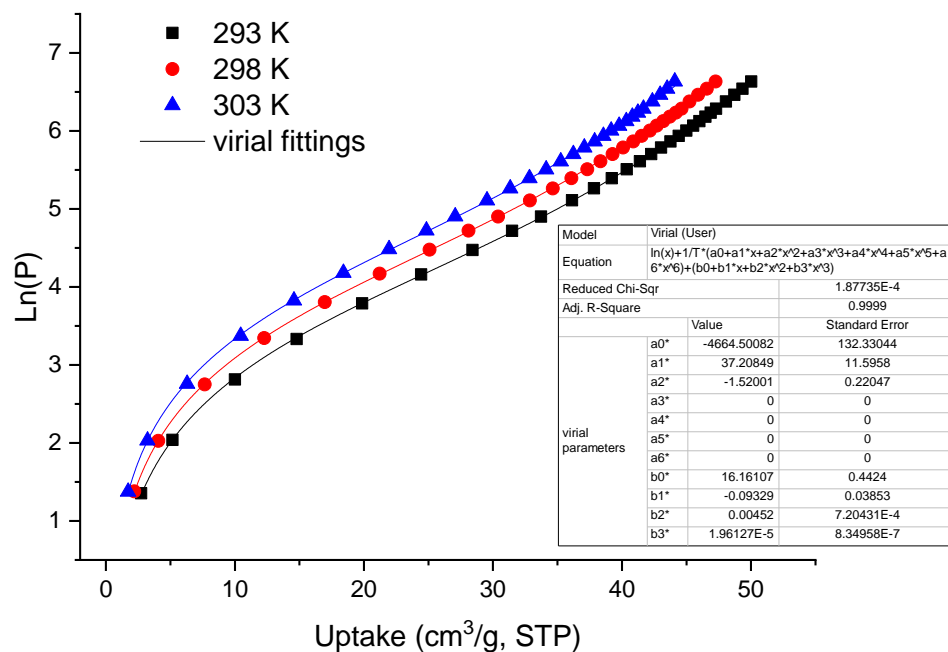


Figure S72. Virial equation fits for CO₂ adsorption isotherms of MUF-16(Mn).

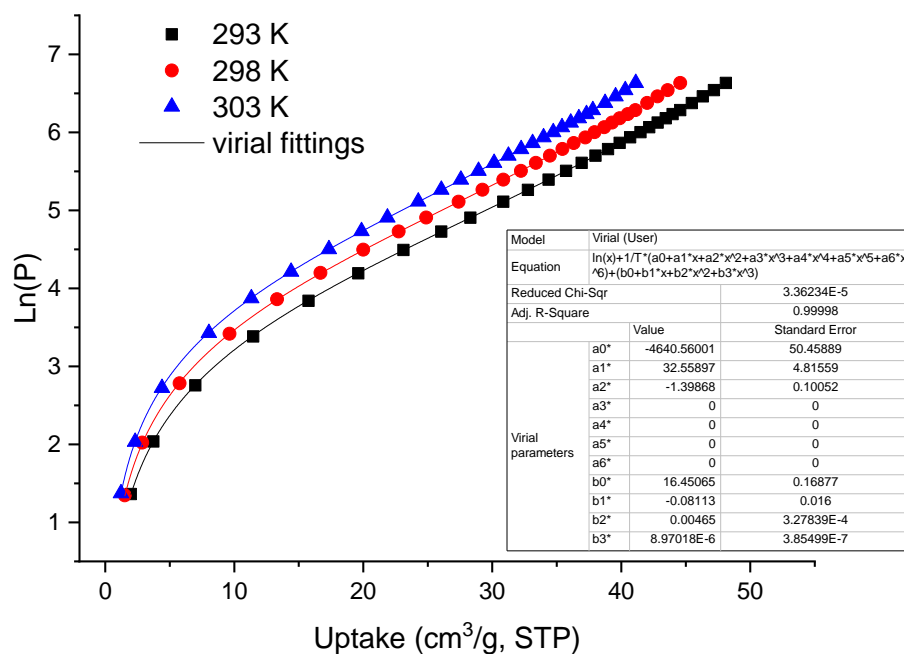


Figure S73. Virial equation fits for CO₂ adsorption isotherms of MUF-16(Ni).

11. Pelletization

MOF pellets were fabricated based on the following procedure:

1. MUF-16 (~1 g) was gently ground using mortar and pestle.
2. The ground sample was transferred to a 20 mL vial and 1 mL of DMF was added. A viscous suspension was obtained after sonicating for half an hour. The suspension was stirred for another 30 mins.
3. PVDF powder (50 mg) was gradually added over the course of 1 hour and the mixture was stirred overnight to make a viscous paste.
4. The paste was transferred into a plastic syringe and squeezed it out into a thin noodle on a glass slide.
5. The noodle was cut into small pellets and dried under vacuum at 140 °C for 6 hours.



Figure S74. A photograph of MUF-16/PVDF pellets.

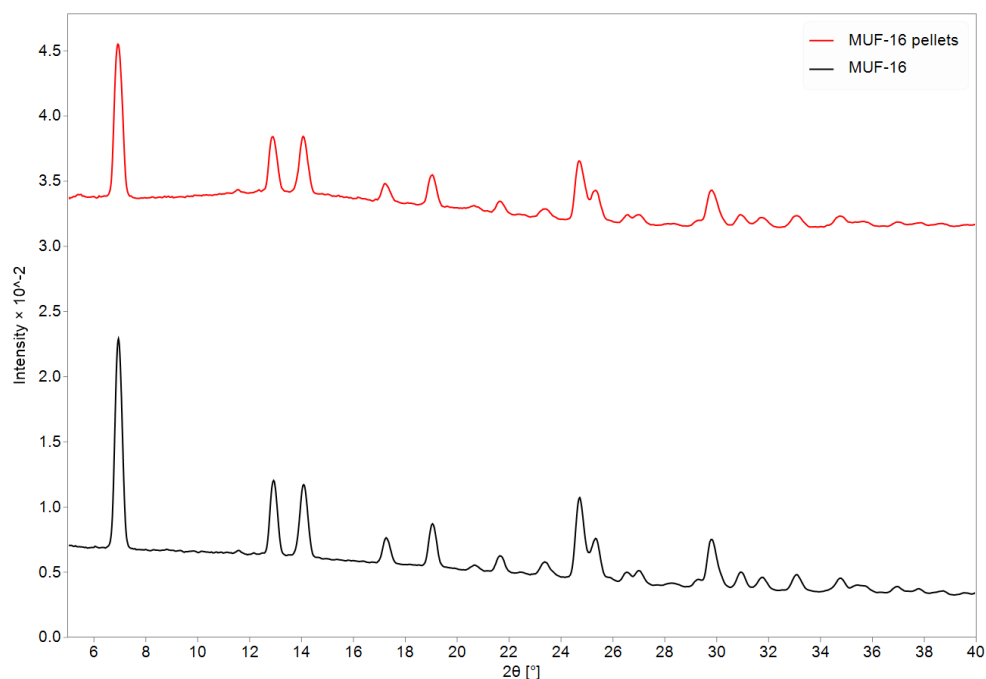


Figure S75. PXRD patterns of MUF-16 showing that its structure remains unchanged after making it into pellet with a PVDF binder.

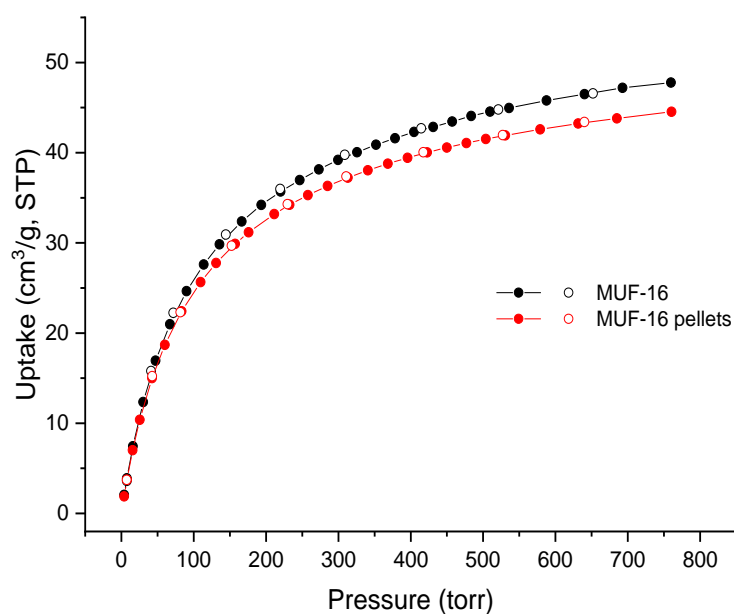


Figure S76. CO₂ adsorption isotherm of MUF-16 at 293 K showing that the inherent adsorption performance of the MOF toward CO₂ remains unchanged after making it into pellet with a PVDF binder. The observed drop in capacity for the pellets arises from the 5 wt% PVDF, which is non-adsorbing.

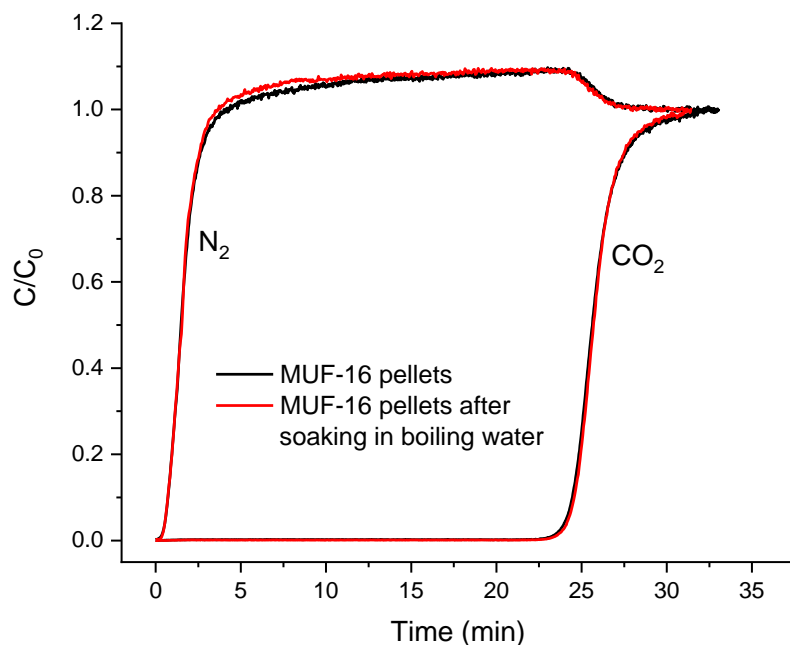


Figure S77. Experimental breakthrough curves for a mixture of CO₂/N₂ 15/85 at 293 K and 1.1 bar in an adsorption column packed with MUF-16/PVDF pellets before and after being soaked in boiling water.

12. Tabulated separation metrics

The CO₂/N₂, CO₂/CH₄, CO₂/H₂ and CO₂/C₂H₂ separation parameters of MUF-16 in comparison to top-performing MOFs are presented in Table S10 and S11. IAST selectivities are presented for a 15/85 mixture of CO₂/N₂, 50/50 CO₂/CH₄, 20/80 CO₂/H₂ and 50/50 CO₂/C₂H₂ at 1 bar, unless otherwise stated. Q_{st} values are reported at low loading, unless otherwise stated. Uptake ratios are calculated by dividing the uptake of CO₂ by that of N₂, CH₄ or C₂H₂ (all at 1 bar and the specified temperature in the Table S10 and S11). These were taken from either a direct statement of relevant details in the manuscript or were extracted from figures by a digitizer software.

Table S10. Metrics relevant to CO₂/N₂/CH₄ separations for MUF-16 in comparison to other top-performing materials reported in the literature.

	Material	T (°C)	P (bar)	CO ₂ N ₂ CH ₄ uptakes (cc/g)	Q _{st} (CO ₂) (kJ/mol)	Uptake ratio		IAST selectivity		
						CO ₂ /N ₂	CO ₂ /CH ₄	CO ₂ /N ₂ (15/85)	CO ₂ /CH ₄ (50/50)	CO ₂ /H ₂ (20/80)
This work	MUF-16	20	1	47.8 1.3 1.2	33	36.2	39.8	631	6686	9695
	MUF-16(Mn)	20	1	50.5 2.9 3.1	38	17.6	16.3	256	470	301
	MUF-16(Ni)	20	1	48.0 2.3 2.8	37	20.8	17.3	281	1215	6828
Commercial adsorbents and zeolites	Zeolite 13X ¹⁵⁻¹⁶	25	1	112 6.0 13	44-54	18.7	8.6	420 [#]	103	250 ^{##}
	Zeolite 5A ¹⁷⁻¹⁸	30	1	75.5 5.2 11.8	23 ^c	14.5	6.4	n/a	n/a	n/a
	Zeolite 4A ¹⁹⁻²⁰	30-32	1	105.3 7.4 15	39	14.2	7	n/a	n/a	n/a
	BPL Activated carbon ²¹⁻²²	25	1	46.2 6.5 20.2	21 ^c	7.1	2.3	23 [*]	4	n/a
	SIFSIX-3-Cu ²³	25	1	58 4.3 n/a	54	13.5	n/a	15500 [#]	n/a	n/a
	SGU-29 ²⁴	25	1	79.2 n/a n/a	50	n/a	n/a	3510 [#]	n/a	n/a
	IISERP-MOF2 ²⁵	30	1	88.5 5.1 n/a	33	17.3	n/a	1860	n/a	n/a
	SIFSIX-3-Zn ¹⁶	25	1	57 5.1 17.6	45	11.2	3.2	1820 [#]	230	n/a
	[Cd ₂ L(H ₂ O)] ₂ .5H ₂ O ²⁶	20	1	47.2 1.3 1.1	37	36.3	42.9	n/a	n/a	n/a
	UTSA-120 ²⁷	23	1	112 5.6 20.8	27	20.0	5.4	600	96	n/a
	[Cu(bc ppm)H ₂ O] ²⁸	20	1	33.6 1.5 n/a	29	22.4	n/a	590	n/a	n/a
	bio-MOF-11 ²⁹	25	1	92 2.9 n/a	45	31.7	n/a	75 ^b	n/a	n/a
	PPN-6-CH ₂ DETA ³⁰	22	1	98.6 0.7 n/a	63	140.0	n/a	442	n/a	n/a
	Cu-BTtri	40	1	n/a n/a n/a	n/a	n/a	n/a	n/a	n/a	25 ^{##}
	mmen-Cu-BTtri ³¹	25	1	90 2.35 n/a	96	38.3	n/a	330 [*]	n/a	n/a
	Ni-4PyC ³²	40	1	n/a n/a n/a	n/a	n/a	n/a	n/a	n/a	190
	UTSA-16 ³³⁻³⁴	23	1	96 4.5 13.2	33	21.3	7.3	314	38	n/a
	en-Mg-dobdc ³⁵	25	1	103 2.2 n/a	50	47.0	n/a	230 ^a	n/a	n/a
	HKUST-1 ^{34, 36-37}	25	1	103 4.5 18.7	35 ^c	n/a	7.4	23	5.5	n/a
	Mg-dobdc ^{11, 16, 34, 38}	23	1	190 24.6 25	47-52	7.7	7.6	180	130	1530 ^{##}
	IITKGP-5a ³⁹	22	1	49 4 13.6	23	12.3	3.6	150	24	n/a
	DICRO-3-Cu-i ⁴⁰	20	1	40.3 0.51 n/a	37	79.0	n/a	150 ^a	n/a	n/a
	DICRO-3-Ni-i ⁴⁰	20	1	49.8 1.95 n/a	37	25.5	n/a	79 ^a	n/a	n/a
	WOFOUR-1-Ni ⁴¹	25	1	52 3.5 11.5	66	14.8	4.5	180 [#]	26 [#]	n/a
	SIFSIX-2-Cu-i ¹⁶	25	1	121.2 3.4 10.5	32	35.6	11.5	140 [#]	33	n/a
	CAU-1 ⁴²	0	1	165 5.6 27	48	29.5	6.1	100 ^b	28 ^b	n/a
	NbOFFIVE-Ni ⁴³	25	1	51.7 n/a 2.2	54	n/a	23.1	n/a	370	n/a
	TIFSIX-3-Ni ⁴³	25	1	48.6 n/a 4.8	50	n/a	10.2	n/a	160	n/a
	SIFSIX-3-Ni ⁴³	25	1	59 n/a 6.6	45	n/a	8.9	n/a	130	n/a
	SIFSIX-14-Cu-i ⁴⁴	25	1	109 n/a 1.1	38	n/a	116.0	n/a	n/a	n/a
	mmen-Mg-dobdc ⁴⁵	25	1	86.3 2.35 n/a	71 ^c	36.7	n/a	n/a	n/a	n/a

Values were generally taken from either a direct statement in the manuscript or were extracted from relevant figures by a digitizer software.^a Selectivity is calculated from the uptake/partial pressure ratio. ^b Selectivity is calculated from the slope of isotherms at low pressures (Henry constants). ^c Heat of adsorption averaged over CO₂ uptakes. ^{*}IAST is

calculated for a 15/75 mixture (10% other gases assumed). [#]IAST is calculated for a 10/90 mixture. [&]IAST is calculated for a 15/85 mixture. [¥]Molecular sieving mechanism. ^{##}Isotherm data were taken from the literature for zeolite 13X¹⁰ and other materials¹¹ to calculate IAST selectivities at 1 bar and 313 K (see IAST calculation section for fitting parameters).

Table S11. Separation metrics relevant to C₂H₂/CO₂ separations for MUF-16 in comparison to other top-performing materials reported in the literature.

MOF	T (°C)	P (bar)	CO ₂ uptake (mmol/g)	C ₂ H ₂ uptake (mmol/g)	Q _{st} of CO ₂ ^a (kJ/mol)	Q _{st} of C ₂ H ₂ ^a (kJ/mol)	Uptake ratio*	IAST selectivity (50/50)*
CO ₂ -selective MOFs								
MUF-16	20	1	2.14	0.18	34	¥	12.0	510
[Mn(bdc)(dpe)] ⁴⁶	0	1	2.08	0.32	29.5	27.8	6.4	9.0
SIFSIX-3-Ni ⁴⁷	25	1	2.80	3.30	51	36.5	0.8	7.5 ^{&}
K ₂ [Cr ₃ O(OOCH) ₆] ⁴	5	1	0.50	0.10	38	30	4.5	5.6 ^{##}
CD-MOF-1 ⁴⁸	25	1	2.87	2.23	41	17	1.3	3.4 ^{&}
CD-MOF-2 ⁴⁸	25	1	2.67	2.03	67.5	25	1.3	6.1 ^{&}
C ₂ H ₂ -selective MOFs								
UTSA-300a ⁴⁹	25	1	0.15	3.10	-	57	20.6	700
NKMOF-1-Ni ⁵⁰	25	1	2.27	2.67	41	60	1.2	22
HOF-3a ⁵¹	23	1	0.93	2.14	42	19.5	2.3	21
[Ni ₃ (HCOO) ₆] ⁵²	25	1	3.00	4.20	24.5	41	1.4	21
SNNU-45 ⁵³	25	1	4.34	5.98	27.1	40	1.37	4.5
ZJU-196a ⁵⁴	25	1	0.35	3.70	-	39	10.6	18
JCM-1 ⁵⁵	25	1	1.69	3.34	33	36.5	2.0	14
DICRO-4-Ni-i ⁵⁶	25	1	1.02	1.91	34	38	1.9	13.5
UTSA-74a ⁵⁷	25	1	3.00	4.80	25.5	31.5	1.6	8
TIFSIX-2-Cu-i ⁴⁷	25	1	4.20	4.10	36	46	0.97	6
Cu-BTC ^{34, 51, 58}	25	1	5.10	8.90	26.9	30	1.7	5.5
MAF-2 ⁵⁹	25	1	0.82	3.90	27	33	4.7	5
UTSA-50a ⁵¹	23	1	3.10	4.10	27.8	32	1.3	5
FJU-90a ⁶⁰	25	1	4.92	8.03	21	25	1.6	4.3
ZJU-60a ⁶¹	23	1	3.12	6.69	15.5	17.5	2.1	4
ZJU-10a ⁶²	25	1	3.66	7.58	26	39	2.1	4
MFM-188 ⁶³	25	1	5.35	10.20	20.8	32.5	1.9	3.7

Values were taken from either a direct statement in the manuscript or were extracted from relevant figures by a digitizer software. ^a Q_{st} at low coverage. * Uptake ratios and IAST selectivities are given with respect to the ratio of the highly adsorbed component to the weakly adsorbed component from an equimolar mixture. [&] Fitting parameters were taken from the literature for SIFSIX-3-Ni⁴⁷ and for CD-MOFs⁴⁸ and to calculate IAST selectivity for an equimolar mixture. ^{##} Isotherm data were extracted from ⁴ using a digitizer software and so we could calculate IAST selectivity for an equimolar mixture. [¥] Adsorption amount is too low to reliably calculate Q_{st}

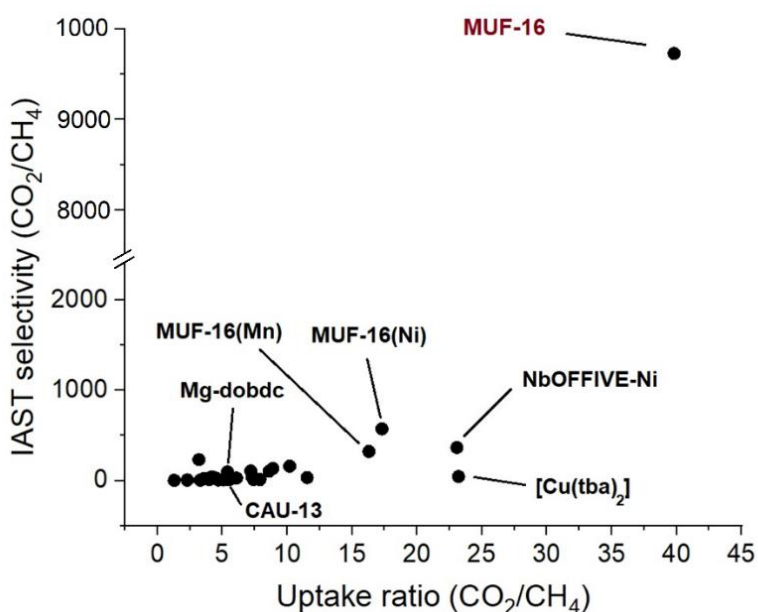


Figure S78. IAST selectivity of MUF-16 family for an equimolar mixture of CO_2/CH_4 in comparison to top top-performing MOFs at 1 bar and ambient temperature versus their uptake ratio at 1 bar.

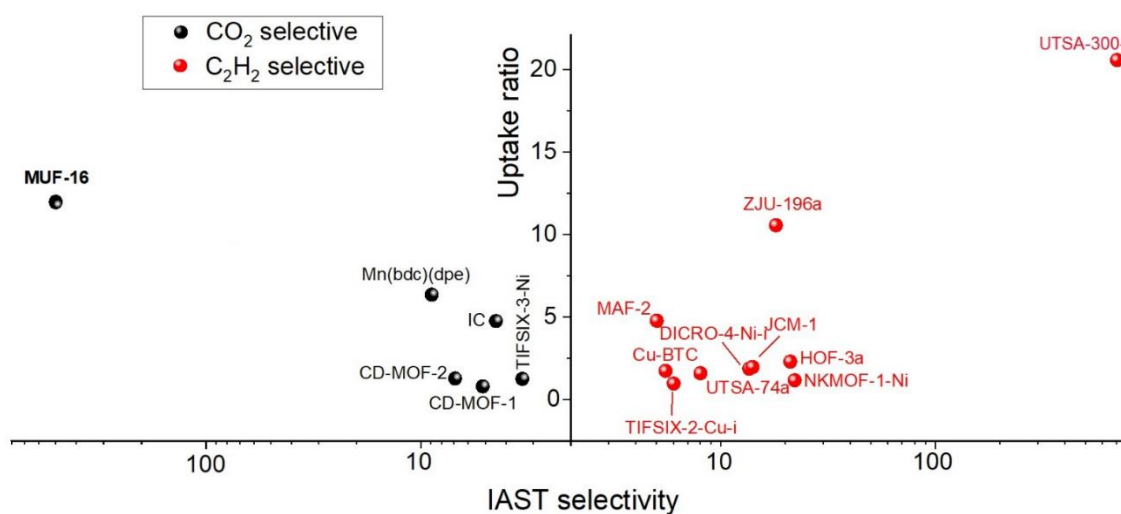


Figure S79. Predicted IAST selectivity (log scale) from an equimolar mixture of $\text{CO}_2/\text{C}_2\text{H}_2$ plotted against uptake ratio at 1 bar and 293-298 K (except for IC (278 K) and $[\text{Mn}(\text{bdc})(\text{dpe})]$ (273 K)) for MUF-16 in comparison to the best materials reported to date. Selectivity and uptake ratios are defined as $\text{CO}_2/\text{C}_2\text{H}_2$ and $\text{C}_2\text{H}_2/\text{CO}_2$ for CO_2 -selective and C_2H_2 -selective materials, respectively.

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