Decomposition Kinetics of Perfluorinated Sulfonic Acids

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¹ Abstract

Perfluorooctanesulfonic acid (PFOS) is a widespread and persistent pollutant of concern to human 2 health and the environment. Although incineration is often used to treat material contaminated 3 with PFOS and related per- and polyfluoroalkyl substances (PFAS), little is known about the 4 precise chemical mechanism for the thermal decomposition of these substances of concern. Here, 5 we present the first study of the thermal decomposition kinetics of PFOS and related perfluori-6 nated acids, using computational chemistry and reaction rate theory methods. We discovered that 7 preferred channel for PFOS decomposition is via an α -sultone that spontaneously decomposes to 8 form perfluorooctanal and SO₂. At 1000 K the halflife for PFOS is predicted to be 0.2 s; decreasing 9 sharply as temperature increases further. These results show that the acid headgroup in PFOS can 10 be efficiently destroyed in incinerators operating at relatively modest temperatures. Understand-11 ing the exact decomposition mechanism and kinetics of PFOS will help to improve remediation 12 technologies actively under development. 13

14 Keywords

¹⁵ Perfluorinated substances, Decomposition kinetics, Incineration, PFOS, PFOA, PFAS, Density
¹⁶ functional theory, Transition state theory

17 INTRODUCTION

Perfluorooctanesulfonate (PFOS) and perfluorooctanoic acid (PFOA) are anthropogenic contaminants belonging to a large family of per- and polyfluoroalkyl substances (PFAS). These substances have been manufactured in large quantities mainly by electrochemical fluorination [1] and, due to their unique physicochemical properties, they had been used in a variety of consumer products and for a range of industrial applications [2]. The atmospheric, biologic, and aquatic degradation of some PFAS also produces PFOS [3–5] and other PFAS [6–8].

In the early 2000s, the primary American and European manufacturers ceased the production

of PFOS after it was globally detected in the human population, wildlife, soil and water [9]. The 1 U.S. Environmental Protection Agency has established a health advisory level at 70 ng/L for the 2 combined concentration of PFOS and PFOA in drinking water [10]. Human exposure to PFOS and 3 PFOS-related products has been linked to cancer, kidney diseases, obesity, immune suppression, 4 elevated cholesterol, and hormone disruption [11–13]. Because of the high energy of C–F bonds 5 in PFAS, they resist physical, chemical, and biological degradation under standard atmospheric 6 conditions, hence posing a persistent and bioaccumulative chronic threat to human health and 7 wildlife. [14]. 8

PFAS remediation methods can be classified into the following treatment groups: oxidative, 9 reductive, and thermal [14–16]. Advanced Oxidation Processes (AOP) which utilize atomic oxy-10 gen, ozone, or hydroxyl radicals are viable solutions for the decomposition of recalcitrant organ-11 ics. However, AOP have shown insufficient degradation efficiency for PFAS waste because highly 12 electronegative fluorine atoms surround the carbon chain in these compounds. Furthermore, in-13 complete mineralisation identified in several AOP studies has indicated the formation of harmful 14 intermediates [17]. To increase the degradation efficiency, conventional AOP are used in conjunc-15 tion with at least one of the following reagents including Fenton's agent [17], sub- and supercritical 16 water [18], zero-valent metal [19], and activated persulfate [20, 21]. Various reductive decompo-17 sition processes have been demonstrated to be useful for the defluorination of PFAS, including 18 aqueous electrons, hydrated electrons, iron, alkaline 2-propanol, and UV-irradiated iodide, or -19 sulfites [22]. For example, ionising radiation via electron beams or gamma rays is promising for 20 PFOS reduction [23]. Recently, sonochemical treatment of PFOS waste has reported complete 21 mineralisation of fluorine [24]. 22

While new PFAS degradation methods are still improving regarding operational cost and scalability [25], incineration and pyrolysis remain the most well-established destruction strategies for solid waste treatment. Incineration involves heating a waste to high temperatures with a typical residence time of several seconds. Laboratory scale analyses have shown PFOS to be more than 99% decomposed at 600 °C [14, 26]. In the incineration of PFOS and perfluorosulfonamides [26], Liquid Chromatography-Mass Spectrometry (LC/MS) measurements have not detected any traces

of PFOS in the reactor effluent implying that thermal treatment could be successfully used for the 1 decomposition of these wastes. It was also demonstrated that perfluorosulfonamide incineration 2 is not a potential source of PFOS to the environment and the presence of SO_2 in the exhaust 3 stream suggests that this is the dominant sink for sulfur. Wang et al. [27] examined hydrated lime 4 (Ca(OH)₂) promoted incineration of PFOS sludge at low temperature (350 °C). The lime treatment 5 of PFOS sludge between 350 °C to 900 °C releases fluorine (defluorination) which subsequently 6 reacts to form CaF_2 and $Ca_5(PO_4)_3F$ phases along with the following gas fragments; $\cdot CF$, $\cdot CHF_2$, 7 $\cdot CF_3$, and $\cdot C_3F_5$. It was also noted that between 600 to 900 °C, an increase in the retention time, 8 temperature or both declines the gaseous CaF_2 content possibly due to the reaction with SiO_2 , 9 H_2O , and $Ca(OH)_2$ [28]. The mechanism of PFOS decomposition is fundamental to understand 10 and improve thermal treatment methods. 11

Some product identification based experimental studies have been carried out, in an effort to 12 elucidate the PFOS combustion mechanism [19, 26, 29, 30]. The terminal functional groups (-SO₃H, 13 -COOH, -SO₂NH₂, etc.) have been observed to be mostly detached during PFAS incineration. For 14 example, in a review article by Vecitis et al. a mechanism for PFOS pyrolysis was reported, where 15 it was proposed that thermolysis begins with breaking of the C-S bond, leading to the formation 16 of SO₃, HF, CF₂, and perfluoroalkene [29]. While CF₂, CF₃, C₂F₆, C₂F₄, SO_x and HF are the 17 observed lighter end-products of PFOS pyrolysis, of which the carbonaceous products transform 18 into CO_x in the presence of oxidizing media (water and/or air) [18, 26]. In the $Ca(OH)_2$ promoted 19 thermal treatment of PFOS, Wang et al. [30] have demonstrated a slightly different mechanism for 20 PFOS decomposition. A hydrodefluorination (conversion of C–F to C–H bonds) [31] mechanism 21 is proposed that initiates with the elimination of fluorine which subsequently reacts with $Ca(OH)_2$ 22 and forms CaF_2 . The above mechanisms suggest different initiation pathways for decomposition 23 of a potassium salt of PFOS; the former states direct C-S bond dissociation while the latter 24 proposed fluorine elimination. Also, the reported mechanisms of PFOS decomposition have not 25 included SO_2 which has been reported as the major sink of sulfur [7, 18, 26]. Analogous to PFOS, 26 the combustion of PFOA also starts at the carboxylate terminal group; Krusic et al. [32] have 27 suggested the elimination of HF and CO_2 at the α -position to produce perfluoroalkene as the initial 28

¹ step for PFOA thermolysis.

The above experimental studies provide a broad overview of PFOS pyrolysis mechanisms, 2 however, they provide limited information about the elementary decomposition pathways nor do 3 they report kinetic parameters. Moreover, they fail to explain the formation of SO_2 in PFOS 4 decomposition; SO_2 has been reported as the dominant sink for sulfur [7, 18, 26]. To develop and 5 optimize thermal treatment technology for PFOS we must have a fundamental understanding of the 6 elementary reaction mechanisms and kinetics. The present study provides the first detailed analysis 7 of the thermal decomposition chemistry and kinetics of PFOS, using computational chemistry 8 and statistical reaction rate theory techniques. This work identifies the likely products of the 9 initial stages of PFOS decomposition and the rate at which these products will form as a function 10 of temperature. Not only will this knowledge advance PFOS incineration techniques, but the 11 understanding of the thermal behaviour of PFOS is also important for the development of advanced 12 oxidation processes and other PFOS remediation methods because thermal treatment is one of the 13 fundamental pre-treatment steps in most of them. 14

15 METHODS

Quantum chemistry calculations were carried out with the Gaussian 16 program suite [33]. The 16 initial stage of work aimed to establish a reaction mechanism for PFOS using the model com-17 pounds perfluoromethanesulfonic acid (PFMS) and perfluoroethanesulfonic acid (PFES). These 18 small model compounds allow us to identify computationally efficient theoretical model chemistries 19 that are accurate for fluorinated sulfonic acids, in addition to establishing their mechanism. For 20 the model compounds (PFMS, PFES), the geometries of reactants, products, intermediates, and 21 transition states were optimized by employing different density functionals and basis sets (Supple-22 mentary Information). The equilibrium structures thus obtained were subsequently re-optimized 23 a the M06-2X/6-31G(2df,p) level of theory and utilized in high-level composite G3X-K energy cal-24 culations [34]. For the full PFOS structure, the most accurate DFT calculations identified on the 25 model compounds were applied. Intrinsic reaction coordinate (IRC) calculations have also been 26 carried out to verify transition state connectivity. Rate coefficient calculations have been performed 27

using canonical transition state theory in the Multiwell-2016 collection of programs [35, 36]. All
input parameters required for the rate coefficient calculations are provided in the Supplementary
Information. The reaction rate coefficients and halflife are studied in the temperature range of
300-2000 K.

5 RESULTS AND DISCUSSION

6 PFMS Model Compound

The decomposition mechanism identified for PFMS on the basis of high-level G3X-K theory calcu-7 lations is depicted in Fig. 1. The lowest energy direct bond-breaking reaction was found to be C–S 8 cleavage, leading to the CF₃ and HSO₃ radicals. Terminal bond breaking has also been implicated 9 in numerous experimental studies of long chain perfluorinated compounds [19, 26, 29]. This reac-10 tion does not proceed via a transition state (TS) and requires a barrier height of 72.8 kcal/mol. 11 All other bond breaking reactions were found to be considerably higher in energy and are depicted 12 in the Supplementary Information (Figure S2). Elimination of SO₃ via a H-shift reaction (TS2M) 13 can also take place, forming HCF_3 (transition state structure shown in Fig. 3b). This is a known 14 decomposition mechanism in sulfonic acids [15] and requires a barrier approximately equivalent to 15 that for C-S bond cleavage. Slightly lower in energy than both of these conventional mechanisms 16 is an isomerization process to yield the PFMS isomer $CF_3OS(O)OH$ (ISOPFMS, Fig. 3h). This 17 reaction proceeds via TS3M, with barrier height of 68.4 kcal/mol. Although CF₃OS(O)OH sits 18 lower in energy than PFMS, it appears to be thermally unstable, with low-barrier decomposition 19 channels available for SO_2 loss (TS5M and TS6M). 20

²¹ The lowest-energy decomposition mechanism for PFMS, by a considerable margin, involves HF ²² elimination via TS1M (the transition state geometry represented in Fig. 3a). The energetic barrier ²³ here is calculated to be 45.3 kcal/mol, and this process will dominate the decomposition kinetics. ²⁴ Loss of HF leads to formation of the three-membered ring compound called diffuoromethyl α -²⁵ sultone (DFMS, Fig. 3g). Previously in the synthesis of γ -sultone [37], Morimoto et al. [38] ²⁶ have also suggested α -sultone as an unstable reaction intermediate. The potential surface energy



Figure 1: Thermal decomposition mechanism for PFMS. Energies are 0 K enthalpies in kcal/mol calculated at the G3X-K level of theory.

- ¹ diagram shown in Fig. 2 also reveals that DFMS is a highly labile compound that spontaneously
- ² decomposes to CF_2O and SO_2 with an almost negligible barrier of 5.4 kcal/mol. The elimination
- $_{3}$ of SO₂ takes place through transition state TS1MS1 (shown as an inset to Fig. 2).



Figure 2: Thermal decomposition of DFMS. Energies are 0 K enthalpies in kcal/mol calculated at the G3X-K level of theory.

The optimized geometries of PFMS, transition states and intermediates in the dissociation process of PFMS are shown in Fig. 3. The lowest-energy decomposition of PFMS (Fig. 3a) proceeds via a transition state resulting in the formation of DFMS. The major structural feature of this transition state involves the elimination of HF and the creation of a new bond between the
terminal oxygen and carbon. At the BMK/6-31++G(2df, p) level of theory, the C–S bond length
and CSO bond angle are changed to 1.80 Å and 75.61° respectively in the transition state as
compared to 1.87 Å and 107.19° in the ground state PFMS (Fig. 3i).



Figure 3: PFMS optimized transition state geometries (a-e) and ground state structure of (g) DFMS, (h) ISOPFMS, (f) PFMS at the BMK/6-31++G(2df,p) level of theory

Having established a decomposition mechanism for PFMS, attention turns to identifying model
chemistries of reduced computational cost that can accurately reproduce the main features observed
in this mechanism. Numerous density functional theory (DFT) methods were trialled in combination with different basis sets (Table S1 in the Supplementary Information). For all methods, the
addition of diffuse basis functions dramatically improved accuracy for only a modest increase in
computational cost. Extending basis set size from double-zeta to triple-zeta, on the other hand,
resulted in only small improvements in accuracy for a significant extra cost. Accordingly, the aug-

¹ mented double-zeta basis set 6-31++G(2df,p) was selected. Of the different DFT methods, the ² BMK and M06 functionals predicted the barrier height for HF elimination to similar precision, ³ with BMK proving to be significantly more accurate for the other transition state energies. Ac-⁴ cordingly, the BMK/6-31++G(2df,p) model chemistry [39] was adopted for the subsequent PFES ⁵ and PFOS calculations.

6 PFES Model Compound

A mechanism illustrating the key features in the thermal decomposition of PFES is shown in 7 Fig. 4. In this diagram, energies are included at the G3X-K and BMK/6-31++G(2df,p) levels of 8 theory. The conventional sulfonic acid decomposition mechanisms leading to the HSO₃ radical and 9 SO_3 proceed with similar energetics to their PFMS counterparts. The lowest-barrier decomposition 10 reaction is still for HF elimination via TS1E to yield a tetrafluoroethyl α -sultone (TFES), although 11 the G3X-K barrier height has increased from 45.3 to 55.8 kcal/mol. Note that the BMK model 12 chemistry over-predicts this reaction barrier by almost 3 kcal/mol, in both the PFMS and PFES 13 cases. Finally, a new HF elimination reaction is seen for PFES, leading to the products $CF_2 = CF_2$ 14 and SO_3 (TS3E). The transition state energy is slightly higher than for TS1E, although it is likely 15 to be a competitive side-reaction in PFES decomposition. The optimized PFES and transition 16 state geometries are displayed in Fig. 5. 17

Transition state theory has been used to calculate rate coefficients for PFES decomposition to the product sets $CF_3CFO + HF + SO_2$ and $CF_2CF_2 + HF + SO_3$, and to predict the PFES halflife as a function of temperature. An Arrhenius plot of the calculated rate coefficients is shown in Fig. 6, demonstrating that the acid head-group predominantly decomposes via initial elimination of HF, with subsequent dissociation to SO_2 and CF_3CFO is assumed to be instantaneous. The competing direct process of HF loss with CF_2CF_2 and SO_3 formation is a minor channel, even at very high temperatures.

²⁵ Calculated halflife values for PFES are shown in the Supplementary Information Figure S3.
²⁶ Even at the relatively low incineration temperature of 800 K (527 °C) PFES is predicted to de²⁷ compose rapidly, with a halflife of 2.4 seconds. At 1000 K the PFES halflife is only 2.5 ms. After



Figure 4: Simplified thermal decomposition mechanism for PFES. Energies are 0 K enthalpies in kcal/mol calculated at the G3X-K (BMK/6-31++G(2df,p)) levels of theory.

- ¹ identifying two least resistive (TS1E, TS3E) routes for PFES decomposition, we next consider the
- ² thermolysis of the full PFOS molecule via these novel pathways.



Figure 5: PFES optimized transition state geometries (a-c) and ground state structure of PFES (d)

¹ PFOS Decomposition

Following the preliminary calculations on the smaller PFMS and PFES model compounds, the 2 BMK/6-31++G(2df,p) model chemistry was extended to PFOS itself for the two most important 3 identified reaction channels. A potential energy surface is shown in Fig. 7 and the optimized 4 geometries are represented in Fig. 8. Compared to PFES, the barrier (TSO1) for HF elimination 5 to produce a PFOS derived α -sultone intermediate (C₈F₁₆SO₃) is very similar, at 57.5 kcal/mol 6 (compared to 58.7 kcal/mol at the same level of theory, Fig. 4). In experimental study Song et 7 al. (2013) have also reported that the photochemical decomposition of PFOA initiates with the 8 elimination of fluorine atom at α -position of the terminal group [21]. As discussed, the BMK 9 calculations are expected to somewhat over-predict this barrier height, and the calculated rate 10 coefficients based on these energies may, therefore, be slight under-predictions. As with the model 11 compounds, the α -sultone resulting from HF loss can readily dissociate with barrier height 8.5 12 $\rm kcal/mol$ to yield SO₂ and perfluorooctanal (C₇F₁₅CFO) via TSO12 transition state (Fig. 7b) The 13 energies presented in Fig. 7b are calculated based on the α -sultone intermediate. 14



Figure 6: Arrhenius plot of calculated rate coefficients, k (s⁻¹), for thermal decomposition of PFES.

The competing decomposition channel for simultaneous HF and SO₃ loss was also considered, 1 producing perfluorooct-1-ene (TSO2). The barrier height here was calculated to be 63.5 kcal/mol, 2 considerably higher than that of TSO1. The formation of perfluoroolefin has also documented 3 in the pyrolysis mechanism of PFOS which is based on an experimental study [29]. Further, the 4 previous studies suggest that the decomposition proceeding from perfluorooctene-1 follows the 5 chain shortening pathway and leads to the formation of CF_2 , CF_3 , C_2F_6 , C_2F_4 and HF, among 6 these the carbonaceous compounds transform into CO_x in the presence of oxidizing media (water 7 and/or air) [40-43]. 8



Figure 7: Thermal decomposition mechanism for PFOS and PFOS derived α -sultone intermediate. Energies are 0 K enthalpies in kcal/mol calculated at the BMK/6-31++G(2df,p) level of theory

The potential energy surface outlined in Fig. 7 was used to calculate rate coefficients for PFOS 1 decomposition, according to transition state theory. Calculated rate coefficients and halflife for the 2 two pathways considered are shown in Fig. 9 and Fig. 10 respectively at temperatures between 3 300 and 2000 K. Across all temperatures, HF loss to form SO_2 and the perfluorinated aldehyde 4 is the dominant reaction channel. Rate coefficients for this reaction can be accurately reproduced 5 using the Arrhenius parameters $A = 2.18 \times 10^{13} \text{ s}^{-1}$ and $E_a = 58.4 \text{ kcal/mol}$. As we can see from 6 Fig. 10 that the PFOS halflife drops to below 1 s at 1000 K, which is again a relatively modest 7 incineration temperature. 8





Figure 8: PFOS optimized transition state geometries (a-c) and ground state structure of PFOS (d)



Figure 9: Arrhenius plot of calculated rate coefficients, k (s⁻¹), for thermal decomposition of PFOS.



Figure 10: Calculated halflife (ms) for thermal decomposition of PFES.

This work suggests that perfluorooctanal will be the dominant initial fluorinated product of 1 PFOS incineration, and the fate of fluorinated aldehydes in these systems therefore also needs to 2 be considered. These compounds are known to be rapidly hydrolyzed to perfluorocarboxylic acids 3 [29, 44], which is likely to be an important fate in the presence of water. Perfluorocarboxylic acids 4 are chemical of concern in their own right, although laboratory scale studies on their incineration 5 have demonstrated that they are up to 99 % decomposed in incinerators operating at 300 °C – 350 6 C [32, 45]. Further work is required, however, to identify the ways in which oxygenated PFAS 7 compounds break down during pyrolysis. 8

In summary, this work has identified that PFOS will undergo relatively rapid thermal decom-9 position, via a novel chemical mechanism. Moreover, our thermolysis mechanism explains the 10 formation of SO_2 which has been detected in PFOS incineration effluent. We have also shown 11 that SO₃ cannot only be produced via direct C–S bond dissociation but could also be formed via 12 unimolecular elimination (transition state TSO2). We believe that the results of the present study 13 not only provides a theoretical background for the PFOS thermal decomposition but would also 14 help to: i) improve the current incineration technology by providing better-operating conditions; 15 and ii) assist in the set up of new treatment facilities. 16

¹ CONCLUSION

The thermal decomposition kinetics of PFOS and model compounds (PFMS and PFES) have been 2 theoretically investigated by employing DFT and transition state theory. The C–S bond cleavage 3 has been found to be the lowest energy direct bond-breaking reaction. However, the lowest-4 barrier decomposition for the model compounds and PFOS is HF elimination to yield α -sultone 5 intermediate. Our findings demonstrate the α -sultone is an unstable compound that spontaneously 6 releases SO_2 . In addition, HF could also be eliminated leading to the formation of perfluoro-1-7 ene and SO_3 , and this step could be the competitive reaction channels in thermolysis processes. 8 Calculated rate coefficients and halflifes confirm that HF loss to form SO_2 and a perfluorinated 9 aldehyde is the dominant reaction pathway at all temperatures. In summary, this study provides 10 a better understanding of PFOS decomposition kinetics that will be used as a guide for improving 11 and developing both current and new PFOS treatment facilities. 12

¹³ Conflicts of interest

¹⁴ The authors report no conflict of interest.

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