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 **Electrocatalytic CO<sup>2</sup> reduction has the dual-promise of neutralizing carbon emissions in the near future, while providing a long-term pathway to create energy-dense chemicals and fuels from atmospheric CO2. The field has advanced immensely in recent years, taking significant strides towards commercial realization. Catalyst innovations have played a pivotal role in these advances, with a steady stream of new catalysts providing gains in CO<sup>2</sup> conversion efficiencies and selectivities of both C1 and C2 products. Comparatively few of these catalysts have been tested at commercially-relevant current densities (~200 mA/cm<sup>2</sup> ) due to transport limitations in traditional testing configurations and a research focus on fundamental catalyst kinetics, which are measured at substantially lower current densities. A catalyst's selectivity and activity, however, have been shown to be highly sensitive to the local reaction environment, which changes drastically as a function of reaction rate. As a consequence of this, the surface properties of many CO<sup>2</sup> reduction catalysts risk being optimized for the wrong operating conditions. The goal of this article is to communicate the substantial impact of reaction rate on catalytic behaviour and the CO<sup>2</sup> reduction reaction. In brief, this work motivates high current density catalyst testing as a necessary step to properly evaluate materials for electrochemical CO<sup>2</sup> reduction, and to accelerate the technology toward its envisioned application of neutralizing CO<sup>2</sup> emissions on a global scale.**

30 Under an applied potential and in the presence of an appropriate catalyst, carbon-dioxide 31 (CO<sub>2</sub>) and water can be electrocatalytically converted into syngas (CO + H<sub>2</sub>), ethylene (C<sub>2</sub>H<sub>4</sub>), 32 methane  $(CH_4)$ , ethanol  $(C_2H_5OH)$  and formate  $(HCOOH)$  among other products. The 33 collective market size of these reduction products is >500 Mton/year, indicating the potential 34 scale of a commercially competitive  $CO<sub>2</sub>$  electrolyzer;<sup>1</sup> in the process, and of utmost 35 importance and urgency, this process may aid in reducing fossil fuels by supplanting current  $36$  production routes. Excitingly,  $CO<sub>2</sub>$  electroreduction catalysts have shown enough promise that 37 we are beginning to see the first steps towards commercial application of the technology, 38 including more and more start-ups (see OPUS12, CERT, Dioxide Materials) and established 39 companies (Siemens) focusing on system design and engineering. As a result, researchers are now targeting lower overall cell potentials by improving other parts of the conversion unit,  $2^{-5}$ 40 41 while looking to more efficiently integrate electrochemical  $CO<sub>2</sub>$  conversion units with 42 upstream and downstream processes.<sup>6</sup> Future devices will also need to demonstrate stable 43 long-term operation ( $>20,000$  hours) at substantial current densities ( $>200$  mA/cm<sup>2</sup>) to 44 minimize the capital-expenditure of a conversion unit to economically-compelling levels.<sup>1,7,8</sup> 45 Due to the low solubility of  $CO_2$  in aqueous-fed systems that limits  $CO_2$  conversion to current 46 densities of  $\sim$ 35 mA/cm<sup>2</sup>,<sup>9–11</sup> researchers have turned to pressurized electrolytes and 47 gas-diffusion layer-based systems to supply enough  $CO<sub>2</sub>$  to the catalyst layer to sustain higher 48 current densities. Despite these capabilities, an overwhelming percentage  $(>95%)^{12,13}$  of 49 fundamental studies and catalytic materials are still developed, tested and characterized in 50 classical H-cell configurations, where current densities are limited. The local catalytic 51 environment, and subsequently the energetics of the reactions occurring on a catalyst's 52 surface, are known however to be highly sensitive to changes in reaction rate. Therefore a 53 fundamental question remains: how representative are the conclusions from aqueous-fed 54 systems that are constrained to  $\sim$ 35 mA/cm<sup>2</sup> when the goal is to achieve >200 mA/cm<sup>2</sup>?

 This article seeks to shed light on this question by summarizing how the local reaction environment is known to vary as a function of current density, and how these changes may impact reactions occurring on a catalyst's surface when pushed to commercial current densities. To aid in the analysis we draw upon recent literature findings from electrochemical experiments, transport phenomena and Density-Functional Theory (DFT) modelling.

 Due to the promise of electrochemical CO<sup>2</sup> reduction technology, and a lack of selective and efficient cathode materials, a large fraction of the field has undergone a global, multidisciplinary effort over the last decade to find new and better catalysts. The search is complicated by the large number of surface factors impacting activity including intermediate 64 binding energy,<sup>14,15</sup> (via coordination<sup>16,17</sup> and site availability<sup>18–20</sup>), packing,<sup>21,22</sup> kinetic supply 65 of reactants,<sup>23</sup> desorption of products,<sup>24</sup> adsorbate-adsorbate interactions,<sup>25</sup> etc. The urgency of these efforts is illustrated by the large number of material-centric review papers published 67 in the last year alone on catalyst development/optimization.<sup>10,26–30</sup> Here, we define the catalyst 68 as the surface on which  $CO<sub>2</sub>$  is reduced. As with any catalytic process, however, the local and system reaction environments play equally important roles in efficiently driving specific reactions, while suppressing unwanted competing ones. Many researchers have reported the 71 extreme sensitivity of the reaction to changes in local  $pH$ ,  $31-35$  electrolytes  $36,37$  and cations  $38-41$ 72 (easily illustrated by replacing  $K^+$  with Na<sup>+</sup>). The 'catalyst' that notably reduces the energy 73 barrier for  $CO<sub>2</sub>$  reduction processes is then very much a combined material and environmental effect, rather than that of the catalyst's surface (composition, coordination, nano/mesostructure) alone.

 The above distinction, while central to any catalytic process, warrants particular attention here due to the unique peculiarities of electrocatalytic  $CO<sub>2</sub>$  reduction in aqueous solvents. *Specifically, while the local environment directly influences reaction pathways and kinetics, the reduction reaction itself greatly disturbs the local environment*. At the root of this

80 reaction-driven sensitivity is the requirement for both  $CO<sub>2</sub>$  and protons (H<sup>+</sup>) to participate in 81 the  $CO<sub>2</sub>$  reduction process. The ever-present, and in many cases more thermodynamically 82 favourable, hydrogen evolution reaction (HER) then simultaneously competes with  $CO<sub>2</sub>$ 83 reduction for protons and electrons. At extremely low current densities  $(1 \text{ mA/cm}^2)$ , these 84 protons can be supplied to either reaction directly by hydronium contained within the local 85 electrolyte (Fig. 1a).<sup>42</sup> As hydronium is depleted, water reduction fills the role as a hydrogen 86 source while the unused hydroxide molecule generated as a by-product, rapidly increases the 87 local electrolyte pH (Fig. 1c).<sup>43,44</sup> At slightly more moderate  $CO_2$  reduction current densities 88 in aqueous-fed systems (~35 mA/cm<sup>2</sup> for C1 products, ~100 mA/cm<sup>2</sup> for C2 products<sup>32,36</sup>), 89 CO<sup>2</sup> ultimately becomes depleted by a combination of diffusion limitations from the bulk 90 electrolyte, and the now unfavourable bicarbonate-equilibrium conditions as a result of the



**Fig. 1**: The relative effect of current density on the reaction (a) proton source, (b) concentration of  $CO<sub>2</sub>$  and (c) pH at the surface of a  $CO<sub>2</sub>$  reduction catalyst.

91 increased local pH.<sup>45,46</sup> Thus, as the reaction proceeds from 0 mA/cm<sup>2</sup> to CO<sub>2</sub>-depletion (Fig. 1b), the surface coverage and binding energies of key intermediates on a catalyst's surface are 93 ultimately impacted through these changes in the local environment;<sup>44,47,48</sup> not dissimilar from the surface effects incurred by varying material composition, structure or morphology. The activity of a catalyst is then identified by the environment around it, as much as its physical make-up.

97 The inherent sensitivity of the reaction to changing local conditions is seen in literature to 98 directly and indirectly drive many of the experimental choices in electrolyte type and 99 concentration. Unsurprisingly, a catalyst can perform exceptionally well or poorly depending 100 on the medium in which it is tested. The importance of the electrolyte medium on catalytic 101 behaviour is most clearly displayed through the near ubiquitous use of low KHCO<sub>3</sub> 102 concentrations in reports of high selectivity C2 production on nanostructured<sup>49–51</sup> and oxide-103 derived  $Cu^{52-55}$  in H-cells. Here the poor buffering capacity of the electrolyte causes the pH 104 close to the electrode to quickly increase at low current densities  $(\leq 20 \text{ mA/cm}^2)$ , helping to 105 promote C2 products and suppress the competing CH<sub>4</sub> and H<sub>2</sub> reactions.<sup>31,56</sup> The morphology 106 of the catalyst can be used to provide similar cumulative effects,<sup>52</sup> which ultimately makes 107 properly separating the direct contributions of intrinsic catalytic activity and the local 108 environment even more difficult. To this point, the field has collectively learned to manipulate 109 both catalysts and local electrochemical conditions as needed to optimize  $CO<sub>2</sub>$  reduction 110 performance metrics at primarily indiscriminate current densities. Given this widely-111 implemented knowledge that the environment is critical to catalytic behaviour, and that these 112 conditions change as a function of current density, it is our perspective that the environment at 113 commercially-relevant current densities (>200 mA/cm<sup>2</sup>) should be used as the criterion for 114 assessing catalytic performance and suitability.

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116 Effect of cell configuration and reaction rate on  $CO<sub>2</sub>$  reduction environments

117 The number of  $CO<sub>2</sub>$  electroreduction experiments reported at elevated current densities is 118 rapidly increasing, owed in part to the maturity of the field as well as the observed 119 performance benefits. Recent work has reviewed various electrochemical architectures 120 capable of delivering enough  $CO_2$  to the catalyst to reach current densities  $>200$  mA/cm<sup>2</sup>,<sup>12,13</sup> 121 summarizing in detail the impacts of different components and configurations on system 122 performance. While we refer the reader to these publications for specific technical advances 123 in the field, we will briefly summarize several commonly-used architectures (Fig. 2) and 124 aspects of their operation to illustrate how the reaction environment around the catalyst layer 125 is influenced by elevated current densities.



**Fig. 2**: Comparative mass transport phenomena in commonly-used electrochemical  $CO<sub>2</sub>$  reduction configurations. (a) Cell view for an H-cell configuration with a catalyst deposited on a solid substrate, (b) Cell view for a catalyst deposited on a gas-diffusion layer with a flowing catholyte channel, (c) Cell view for a catalyst deposited on a gas-diffusion layer with a non-flowing catholyte, (d) species transport to and from a catalyst layer in which  $CO<sub>2</sub>$  is supplied via diffusion from the bulk electrolyte on the microscale ( $\sim$ 50 µm). (e) a CO<sub>2</sub> reduction catalyst layer deposited onto a hydrophobic substrate with CO<sub>2</sub> diffusion from a nearby gas-liquid interface ( $\sim$ 50 nm). Liquid species diffuse to the ionexchange membrane through either a bulk flowing electrolyte or a solid-supported electrolyte layer.

126 In each of the described configurations  $CO<sub>2</sub>$  is supplied to a catalyst layer that is fully or 127 partially immersed in a conductive electrolyte. This  $CO<sub>2</sub>$  can diffuse through the 128 hydrodynamic boundary layer of a saturated bulk electrolyte as in a standard H-cell 129 configuration (Fig. 2a and d),  $45,46,57$  or from a nearby gas-phase with a much shorter diffusion 130 pathway (Fig. 2b, c and e).<sup>58–61</sup> Configurations where  $CO_2$  is provided from the gas-phase use 131 a gas-diffusion layer to form a gas-liquid interface adjacent to the catalyst layer. 132 Electrochemical CO<sub>2</sub> reactors using gas-diffusion layers have historically been used in diverse 133 configurations,  $13,62-64$  but range primarily from a Kenis-type reactor with a flowing 134 catholyte<sup>58,65–73</sup> (Fig. 2b), to membrane electrode assemblies<sup>2,5,12,74,75</sup> which directly combine 135 a gas-diffusion layer, catalyst and ion exchange membrane into one unit (Fig. 2c). These latter 136 configurations are occasionally denoted as 'catholyte-free' or gas-phase electrolysis due to the 137 lack of a flowing electrolyte between the catalyst layer and ion-exchange membrane. Liquid 138 water, however, is reported to be present in the porous catalyst layer in the majority of cases. 139 Further, research has shown that without the direct presence of a solid-supported electrolyte,  $140$  CO<sub>2</sub> reduction selectivity can be heavily penalized.<sup>2,5,64</sup> The two cathode variations shown in 141 Fig. 2b and c then similarly involve the diffusion of  $CO<sub>2</sub>$  across a gas-liquid interface and 142 through a thin electrolyte to a porous catalyst layer (Fig. 2e), where evidence suggests that the 143 reaction occurs primarily in the aqueous phase rather than at a three-phase solid-liquid-gas 144 interface. Water management is essential to maintain a stable gas-liquid equilibrium as both 145 flooding of the gas-diffusion layer and evaporation of the catholyte will impact  $CO<sub>2</sub>$  transport 146 to the catalyst layer.<sup>5,70,76</sup> A catalyst can be applied to the gas-diffusion layer via drop-casting, 147 airbrushing, electrodeposition, compression, or incorporation into the porous layer itself.

148 The primary difference between these architectures is a roughly 3-order of magnitude 149 reduction in the CO<sub>2</sub> diffusion pathway to the surface of the catalyst: from  $\sim$ 50  $\mu$ m in an H-150 cell to ~50 nm using a gas-diffusion layer (Fig. 2b,c), which allows for the increased  maximum current densities reported in literature. Using a simple 1D reaction-diffusion model 152 developed previously,<sup>45,46,57–59</sup> we can also approximate the similarities and differences in the local catalytic environments as a function of reaction rate for both cases.

154 The first observation from these curves is that the  $CO<sub>2</sub>$  concentration and pH in the electrolyte at low current densities is relatively similar for both configurations (Fig. 3). This is to be expected as the decreased CO<sup>2</sup> diffusion pathway does not affect the maximum availability of  $CO<sub>2</sub>$  in an electrolyte, and OH<sup>-</sup> diffusion is moderated by the catholyte. In each case a sudden increase in local pH is observed for the weakly-buffered electrolytes (1 M KCl, 0.1 M KHCO3) as the hydroxide generated as a by-product of water-splitting cannot diffuse away fast enough or be immediately buffered by the solution (Fig. 3b and d). Shown here, and 161 in recent experimental work by the Koper group,<sup>42</sup> the electrode pH can in fact shift by as 162 much as 6 units within the first 1 - 2 mA/cm<sup>2</sup>. Not only could the reaction itself be altered by this shift, but large pH differences between the reference and working electrodes in this current density range complicate determination of the equilibrium potential, and subsequently, 165 product onset potentials and Tafel slopes. Furthermore, for slightly acidic  $CO<sub>2</sub>$ -saturated 166 electrolytes, the solvent itself can also act as the sole proton source (via  $H_3O^+$ ) at current 167 densities <1 mA/cm<sup>2</sup> until becoming depleted and replaced by water reduction (Fig. 1a). It is then entirely possible for a CO<sup>2</sup> reduction catalyst to be effective within the Tafel region but exhibit slower kinetics at higher potentials/current densities if the water reduction step to liberate protons becomes rate-determining. Within this low current density region, where the most important electrochemical characterizations of a material take place, the reaction environment is then extremely sensitive, complicating analysis of intrinsic catalyst behaviour and the reaction mechanisms at play.

174 In our reaction-diffusion model, the maximum predicted  $CO<sub>2</sub>$  reduction current densities in 175 the aqueous-fed system are again  $\leq$ 35 mA/cm<sup>2</sup> for two-electron reduction processes (Fig. 3b).

176 As shown here in Fig. 3d, and in previous gas-diffusion layer modelling work, we can see 177 however that the maximum current densities are much higher in the case of a gas-diffusion 178 layer as a result of the reduced  $CO<sub>2</sub>$  diffusion distance; here all electrolytes are capable of 179 sustaining current densities over the proposed 200 mA/cm<sup>2</sup> minimum. This agrees well with 180 experimental literature where current densities substantially higher than 200 mA/cm<sup>2</sup> have 181 been reported, including the first report using gas-diffusion layers for  $CO<sub>2</sub>$  reduction from Cook et al. in 1990.<sup>62</sup> In recent work by Dinh et al., for example, current densities of 1 A/cm<sup>2</sup> 182 183 were reached in 1 M KOH at 1 atm with an overall  $CO<sub>2</sub>$  reduction selectivity over 90%.<sup>70</sup> 184 While these current densities might not be desired economically due to the corresponding 185 increase in cell potential required,<sup>1,7</sup> it indicates that substantial  $CO<sub>2</sub>$  reduction reaction rates 186 are possible even if the  $CO<sub>2</sub>$  partial pressure is reduced. This is important for future large-187 scale devices  $(>100 \text{ cm}^2 \text{ catalyst areas})$  where  $CO_2$  partial pressure will decrease as it is 188 converted in the device. It is also worth noting that the proposed 200 mA/cm<sup>2</sup> minimum 189 current density is defined primarily for two-electron reduction products. For multi-carbon 190 products requiring more electrons per CO<sup>2</sup> molecule converted, this current density limit must 191 be higher to have the same molecular yield per unit area.

192 A final extremely important takeaway from Fig. 3 is that the pH near the electrode will be 193 inevitably high at commercially-viable current densities  $(>200 \text{ mA/cm}^2)$  in all of the most 194 commonly-used electrolytes, regardless of the choice of catalyst or electrolyte (Fig. 3d). Due 195 to the extremely large quantity of hydroxide generated as a by-product of water reduction and 196 limitations in transporting hydroxide away from the electrode, we predict the pH within the 197 catalyst layer will greater than 12, even for a 1 M KHCO<sub>3</sub> buffered electrolyte. While the use 198 of a 0.1 M KHCO<sub>3</sub> electrolyte can, and has, been used in an H-cell to approach the local pH 199 values reached at high current densities (Fig. 2b), these conditions are reached only when  $CO<sub>2</sub>$ 200 is largely depleted and over a small current density/potential range. It is worth noting that the



Fig. 3: Simplified predictions of the electrode concentration of CO<sub>2</sub> and pH for commonly-used electrolytes as a function of current density in an (a,b) H-cell with a 50  $\mu$ m CO<sub>2</sub> diffusion thickness and,  $(c,d)$  a gas-diffusion layer with a 50 nm  $CO<sub>2</sub>$  diffusion thickness and liquid diffusion layer of 200  $\mu$ m. A Faradaic efficiency of CO<sub>2</sub>-to-CO of 90% is assumed.

201 locally alkaline conditions could potentially be avoided by using an acidic electrolyte, but the 202 reaction kinetics for  $CO<sub>2</sub>$  would have to outweigh the heavily-favoured hydrogen evolution 203 rate in acidic media. In any of these cases all changes in local pH will also ultimately have to 204 be paid for in the overall cell potential, regardless of the locally corrected cathode potential. In 205 brief, the results presented in Fig. 3d show a convergence towards local conditions that have 206 far-reaching implications for not only catalytic activity, but the stability and maximum 207 efficiency of an entire  $CO<sub>2</sub>$  reduction system, as discussed in later sections.

 From existing knowledge about CO<sup>2</sup> reduction, we can infer that the thermodynamics and kinetics of reactions on a catalytic surface will be impacted by testing under these elevated reaction conditions. Further modelling and direct-measurement experimental studies of the local electrolyte environment are of course warranted, however, to even better understand  how various factors may influence the reaction (e.g. 2D/3D effects, morphology, partial 213 pressure of  $CO<sub>2</sub>$  in the gas-diffusion layer, etc.). A more detailed representation of  $CO<sub>2</sub>$  diffusion through a porous electrode structure, for instance, may provide further insight but 215 requires consideration of pore sizes, structures and additives, which are catalyst-specific and beyond the scope of this article. These studies are particularly needed for zero-gap membrane electrode assemblies where the extremely-low catholyte volume is expected to make the local reaction conditions more sensitive to the specific device configuration and the properties of the ion-exchange membrane.

### Impact of high current densities on CO<sup>2</sup> reduction catalyst testing

221 In the previous section we discussed the impact that both hydrogen evolution and  $CO<sub>2</sub>$  reduction have on the local environment up to commercially-relevant current densities. This 223 section discusses the important opposite side of the equation, how does access to surplus  $CO<sub>2</sub>$  and the predicted local environment at higher current densities impact the reactions occurring on the surface of the catalyst. More importantly, can we use this understanding to design even 226 better catalysts or conditions that may advance  $CO<sub>2</sub>$  electroreduction performance further.

 In catalyst design the surface of a material is altered as a means of modifying catalytic behaviour. By changing a surface's composition, nanostructure or even substrate, the binding energies of molecules to the surface and the reaction rate of different pathways can be tuned 230 to promote certain reactions, and hopefully, suppress unwanted ones. In electrochemical  $CO<sub>2</sub>$  reduction, the local environment can provide a similar function. Numerous experimental studies have particularly noted the tendency for higher local pH conditions to favour CO and 233 multi-carbon products while suppressing  $H_2$  and CH<sub>4</sub> on metals such as Ag and Cu.<sup>32,36</sup> As shown in Fig. 3d, when operating at higher current densities this effect is pushed to the extreme, even in highly buffered solutions. An important place to start is then to discuss the 236 effect of pH on the selectivity of both  $CO<sub>2</sub>$  reduction products and hydrogen evolution.

237 Due to its role as the primary competing reaction to  $CO<sub>2</sub>$  reduction, H<sub>2</sub> evolution is one of the most important products to consider. Under basic conditions the H<sup>2</sup> evolution reaction proceeds through direct water reduction and the Volmer-Tafel or Volmer-Heyrovsky steps (see EIS Fig. S2). For commonly-used metals such as Cu, Au and Ag, the Volmer step is particularly sluggish in basic conditions due to both poor water dissociation properties and weak \*H binding energies, which is pushed even further to the right and away from the peak 243 of the classical volcano plot under higher pH conditions.<sup>78,79</sup> Simultaneous  $CO_2$  reduction 244 occurring on a catalyst's surface also tends to further suppress  $H_2$  activity by weakening 245 hydrogen binding, occupying surface sites and consuming protons.<sup>25,80</sup> For catalysts on the left side of the hydrogen binding energy volcano curve, however, hydrogen evolution under locally basic conditions may increase for the same fundamental reasons.

248 For the most commonly-used set of materials, access to  $>200$  mA/cm<sup>2</sup> current densities can 249 then provide a secondary means of suppressing hydrogen evolution by weakening hydrogen 250 binding energies under higher local pH conditions. A secondary, non-material approach for 251 suppressing hydrogen is particularly important for multi-carbon product formation where, 252 despite achieving 100-fold C2:C1 ratios, many of the best catalysts when operated in an H-253 cell are constantly dogged by a persistent 20-30%  $H_2$  selectivity.<sup>62,63,68,69</sup> When these same 254 catalyst are operated under elevated current densities in the configurations and electrolytes 255 described here (Fig. 2 and 3), the selectivity towards target products could be increased purely 256 by penalizing hydrogen evolution, rather than necessarily promoting  $CO<sub>2</sub>$  reduction activity. 257 From Fig. 3 one can expect that any pH-dependent suppression of  $H_2$  would be a function of 258 current density and buffering strength, with the simultaneous requirement that the 259 overpotentials needed for  $CO<sub>2</sub>$  reduction are also competitive with  $H<sub>2</sub>$  evolution.

260 The local pH environment can also separately influence the energetics of different  $CO<sub>2</sub>$ 261 reduction products. For catalysts capable of producing only CO and  $H_2$ , the suppression of  $H_2$   can lead to high CO selectivities. On a Ag catalyst CO formation under alkaline conditions has been also been observed to be produced almost immediately following the equilibrium 264 potential of -0.11 V vs RHE<sup>58,67</sup>, indicating that the reaction itself is improved. The behaviour of CO formation on Cu also differs from that of a more neutral H-cell environment. In H-cell tests CO selectivities of >20% are observed on Cu and Cu-derivatives only at very low 267 current densities ( $\leq 5 \text{ mA/cm}^2$ ) before being supplanted by CO<sub>2</sub> reduction to methane, ethylene and ethanol. Under alkaline conditions performed in a gas-diffusion layer, high CO 269 selectivities appear over a much broader range  $(0{\text -}200 \text{ mA/cm}^2)^{70,73}$ . This suggests that the binding energy of CO on Cu may be weakened under alkaline conditions, promoting faster 271 desorption of the formed  $*$ CO intermediate more than under neutral conditions.<sup>70</sup> The selectivity towards CO does eventually decrease in favour of higher order products similar to what is observed in an H-cell, but at much higher overall current densities.

 Similar to H<sub>2</sub> evolution, methane formation on Cu has been shown to be suppressed by increased local pH on oxide-derived samples. If locally alkaline (pH>12) conditions are indeed unavoidable with the currently-used electrolytes, then these results suggest that an alternate reaction mechanism or catalyst may be needed to realize selective methane formation at elevated current densities. An interesting fundamental result would then be the demonstration of a catalyst capable of selective methane formation under alkaline or locally alkaline conditions. Inversely, for multi-carbon product formation on Cu, higher local pH 281 conditions have been experimentally demonstrated  $31,73,83$  to be an important factor for promoting carbon-carbon coupling. The higher observed activity toward multi-carbon species at lower potentials could be due to the imporved CO onset potentials, changes to the binding energy of \*CO, a direct effect of the local conditions on the energetics of the coupling step itself, or a cumulative effect of multiple factors. There does not appear to be any strong  correlations between pH and product distribution after C-C coupling, however, as most studies report similar alkane to alkene ratios as in lower current density H-cell experiments.

 While several studies have operated at elevated current densities using membrane electrode 289 assemblies or neutral-pH catholytes such as KCl and bicarbonate-based salts,<sup>2,5,12,13,73,84</sup> a larger number of gas-diffusion layer experiments have used KOH directly as a bulk 291 catholyte,  $58,65-68,70,71,85$  with much of the original CO<sub>2</sub> reduction research pioneered by the Kenis Group. By using an alkaline catholyte directly, the impact of a higher pH environment 293 on catalyst performance can be probed across both low and high current densities.  $65-68,85$  In a 1 M KOH environment, CO<sup>2</sup> reduction products have been observed on Cu, Au and Ag catalysts at earlier overall onset potentials than in neutral conditions, with current densities of >100 mA/cm<sup>2</sup> having been reached for CO, C<sub>2</sub>H<sub>4</sub> and ethanol at more anodic potentials 297 than -0.6 V vs. RHE and with  $\leq 10\%$  H<sub>2</sub> selectivities.<sup>61,65,67,70,86</sup> These experiments, however, do not pay the same overpotential price associated with the large local pH swing from neutral to alkaline conditions, which are not taken into account when cathode potential are reported versus a reversible hydrogen electrode (RHE). Additionally, the interaction between unreacted  $CO<sub>2</sub>$  and hydroxide is problematic for overall stability, as described in the following section. Using an alkaline electrolyte for testing and characterizing catalyst performance is however a promising means of mimicking the local environment of high current densities while being able to measure catalytic activity even at lower current densities.

 A final consideration for our prediction that many electrolytes will be forced towards high local pH conditions pertains to catalyst stability. Depending on the properties and composition of a given catalyst, such conditions may result in the dissolution of metals into solution or the removal of some species from the surface. While this has not been observed for many of the Cu and Ag catalysts tested in gas-diffusion layer configurations to date, it should be a consideration in the design of new catalysts.

311 A second important property of the local reaction environment at commercial-relevant current 312 densities is access to excess CO<sub>2</sub>. While we have imposed a current density of 200 mA/cm<sup>2</sup> as 313 a threshold to reach, from Fig. 3c we can see that additional unreacted  $CO_2$  surrounding the 314 catalyst provides the capacity for even higher current densities. An increased  $CO<sub>2</sub>$ 315 concentration, even at elevated current densities, helps to kinetically ensure that  $CO<sub>2</sub>$  rather 316 than protons are able to populate the reaction surface. More importantly, the reaction will not 317 be hindered by a deficit of  $CO_2$ , even at higher local pH conditions. While single-carbon  $CO_2$ 318 reduction products such as  $CO<sup>73</sup>$  HCOOH<sup>88,89</sup> and CH<sub>4</sub><sup>90</sup> can reach relatively high 319 selectivities even at lower current densities in an H-cell configuration, the highest Faradaic 320 efficiencies reported for multi-carbon products typically appear at current densities where  $321$  CO<sub>2</sub> is almost depleted. This is in part due to the necessity for multi-carbon products to follow 322 from \*CO (Fig. S2) and C-C coupling which requires both sufficient potentials and current 323 densities.<sup>48,86,91</sup> Testing novel catalysts at elevated current densities with less  $CO<sub>2</sub>$  limitations 324 would allow the surface coverage of the \*CO reaction intermediate to be maximized over a  $325$  wider current and potential range without being kinetically-limited by  $CO<sub>2</sub>$  availability. This 326 is in contrast to current H-cell environments where peak C2 selectivities are often observed 327 only at singular operating conditions (i.e. at a specific potential, current density and pH). 328 Access to a larger operating window then allows more attention to be placed on modifying 329 catalysts to specifically alter  $CO<sub>2</sub>$  reduction product selectivity between higher-order products 330 such as alkenes vs. alcohols and C2 vs C3 products. Finally, operating under an excess  $CO<sub>2</sub>$ 331 environment reduces the overpotential losses associated with transport limitations (sometimes 332 called concentration polarizations). As a result, plots of voltage versus log(j) have been 333 observed to remain linear even up to 300 mA/cm<sup>2</sup>, helping to remove one of the barriers to 334 gauging intrinsic catalyst activity.<sup>17</sup>

 While the exact implications of high current density catalyst testing will vary slightly with materials, we can assert that the local environment will differ greatly from the bulk electrolyte with a substantial chance of changing important surface kinetics and the observed catalytic activity. Tuning catalysts to optimize morphology or surface binding energies for low current density characterization may then risk optimizing the catalyst for the wrong environment unless higher current conditions can be appropriately mimicked. Performing such experiments adds an additional degree of complexity due to the need for researchers to adopt 342 either a pressurized system or a gas-diffusion layer to supply additional  $CO<sub>2</sub>$  (Fig. 2), in addition to developing new catalysts. We believe, however, that this to be an essential step to 344 make the best (highest activity, selectivity and stability)  $CO<sub>2</sub>$  reduction catalyst possible. Fortunately, the range of experimental reports already performed at higher current densities indicate that CO<sup>2</sup> reduction is typically improved versus operating in the same electrolyte at lower current densities, at least in part due to increased  $CO<sub>2</sub>$  availability and suppression of pH-independent products.

## Impact of high current densities on system design

 Up to this point we have discussed the impacts of configuration and reaction conditions on the CO<sup>2</sup> reduction reaction and vice versa. While understanding the CO<sup>2</sup> reduction reaction and catalyst over a range of conditions is important, our preferred choice of catalyst and catholyte will have implications and constraints for the system as a whole. Further catalyst testing in a more commercial-type reactor will help to bring operational issues to the forefront of the field and may result in new ingenious scientific and engineering solutions to these issues.

356 One such issue pertains to the twist of fate that the most efficient  $CO<sub>2</sub>$  reduction conditions appear to occur when a highly-alkaline electrolyte is used as a catholyte. While an alkaline catholyte may provide optimal cathode performance, it comes at the cost of system stability due to the interaction between unreacted  $CO<sub>2</sub>$  and hydroxide in the electrolyte, particularly at  current densities less than the CO<sub>2</sub> limiting case where higher concentrations of CO<sub>2</sub> exist in solution. Our reaction-diffusion model shows that this interaction can decrease the pH within the porous catalyst layer by 1-2 units at lower current densities depending on the 363 replenishment rate from a bulk liquid phase (Fig. 3d).<sup>17</sup> While this pH change can be accounted for when trying to ascertain the intrinsic activity of the catalyst, a portion of the CO<sub>2</sub> crossing the gas-liquid interface will be converted to bicarbonate upon interacting with hydroxide and then carbonate.<sup>61</sup> Not only does this decrease  $CO<sub>2</sub>$  utilization, but over a long enough operating time it will destroy the expensive KOH catholyte, itself energy-intensively produced through electrochemical reactions. At the moment there is no engineering solution to completely mitigate this effect even at small scales, let alone a more complex  $>100 \text{ cm}^2$  reactor design. We may then be resigned to the use of neutral-pH catholytes which to date would represent an increase in expected cathode overpotentials. Further, overall cell potentials will be higher due to the need for the oxygen evolution reaction to occur in a similar pH electrolyte, or by using a bipolar membrane to maintain an alkaline anolyte. While CO2- hydroxide interactions are typically only considered as a critical issue for alkaline catholytes such as KOH, systems using neutral electrolytes should also aim to balance the generated 376 hydroxide ions with protons generated by the anode reaction.<sup>92</sup> Even in a neutral-pH medium



**Fig. 4**: Expected ohmic losses as a function of current density for commonly-used electrolytes in an electrochemical cell with a combined 3 mm catholyte and anolyte thickness at 25 °C.

 the system's electrolyte balance would similarly be steadily shifted away from the initial condition due our  $CO<sub>2</sub>$  reagent that can influence pH; in this case, however, the electrolyte could be externally regenerated without additional energy input.

 Another cell design issue with using alkaline electrolytes is the need for anion exchange membranes, which have comparatively slower ion transport than proton exchange membranes and overall limited mobility for both bicarbonate and carbonate anions.<sup>11,81</sup> For these reasons 383 a large amount of research is being undertaken to improve OH,  $HCO_3$  and  $CO_3$ <sup>2</sup> transport through anion exchange membranes, with a fair amount of work done by Dioxide Materials' 385 and their Sustainion<sup>®</sup> membrane which has shown 1000's of hours of stability, albeit under 386 specific operating conditions.<sup>25,82</sup> Without sufficient bicarbonate/carbonate transport through the membrane, the concentration of buffering ions will increase over time, forcing co-ion transport through the membrane and resulting in electrolyte precipitation, destroying the membrane and/or the gas-diffusion layer. Without solutions to these issues it will be difficult for either membrane electrode assemblies or alkaline catholytes to be paired with anion exchange membranes in a practical  $CO<sub>2</sub>$  reduction device.

392 An additional reaction constraint brought on by the need for  $>$ 200 mA/cm<sup>2</sup> operation pertains to the practical choice of electrolytes, independent of their impact on catalytic activity. Using this minimum current density as a target threshold we can approximate the expected ohmic losses of commonly-used electrolytes at 25°C, regardless of the catalyst or substrate used. Assuming a combined catholyte and anolyte thickness of 3 mm, for example, it is clear that 397 certain electrolytes will cause prohibitive ohmic losses (Fig. 4). The 0.1 M KHCO<sub>3</sub> electrolyte 398 used in the majority of the highest selectivity  $C_2H_4$  studies, for instance, results in heating 399 losses of 6 V at 200 mA/cm<sup>2</sup>, five-fold larger than the thermodynamic cell potential when using an oxygen-evolving anode (Fig. S3). Such a low conductivity electrolyte can then never be used in a functioning system unless the electrolyte pathway between the anode and cathode

402 is eliminated or greatly reduced, as in the case of membrane electrode assemblies (Fig. 2c).<sup>2,5</sup> These ohmic drops also put into perspective how other cell losses may be more influential than further decreases to cathode overpotentials. It is worth noting that the result in Fig. 4 becomes even more pronounced when the presumed even higher current densities needed for 406 multi-carbon products such as  $C_2H_4$  are considered. Finally, separate from our discussion motivating the testing of catalysts at elevated current densities, this result highlights the need to test catalysts in higher conductivity electrolytes to see the effect that a higher concentration of supporting ions may or may not impact a catalyst's activity.

410 A final notable difference to performing  $CO<sub>2</sub>$  electroreduction in an H-cell versus a gas- diffusion layer configuration is subtler. As has been recently demonstrated, under high current 412 density operation the  $CO<sub>2</sub>$  reduction reaction is confined to a relatively small portion of a 413 porous catalyst layer and takes place on the backside of the material (Fig. 5a).<sup>70</sup> This is in 414 contrast to an H-cell where  $CO<sub>2</sub>$  diffuses to the catalyst layer from the front-side bulk electrolyte (Fig. 5a). Much like the effects of varying morphology and porosity in H-cell catalyst studies allowed for performance to be improved and varied, the reversed flow direction of CO<sup>2</sup> transport allows for unique gas-diffusion and catalyst layer engineering to take place. One recent example is placing an inactive material on top of the catalyst layer (Fig. 5a) to provide an additionally conductive layer. While this layer is used as a current collector, it may also help to prevent both catalyst restructuring that can change catalytic behaviour as well as the deposition of contaminants on the active catalyst surface. 422 Contaminants are a problem largely unique to  $CO<sub>2</sub>$  reduction due to the tendency for most electrolytes to contain minute concentrations of Ni, Fe or Co, metals capable of preferentially promoting hydrogen evolution even at low potentials and are a primary source of catalyst 425 deactivation.<sup>2,95,96</sup> One could further imagine layering catalyst structures on gas-diffusion layers for either unique catalyst designs or supportive layers that provide new functionalities.



Fig. 5: (a) Schematic of the directional change in  $CO<sub>2</sub>$  transport for fully-aqueous and gas-diffusion layer  $CO<sub>2</sub>$  reduction catalysts. (b) Potential advantages of a change in the  $CO<sub>2</sub>$  transport and reaction direction inside a catalyst layer. A buried catalyst layer may be inherently more stable and protected from both contaminants and restructuring while still having access to  $CO<sub>2</sub>$ .

427 While many possibilities have yet to be explored for  $CO<sub>2</sub>$  reduction, a gas-diffusion layer provides a porous electrode structure which fundamentally changes both reagent and product transport pathways compared to the impermeable supports traditionally used in fully-aqueous reactors. As adoption increases substantial opportunity then exists for further innovative catalyst-support integrations to improve either stability or performance. The subtle operational difference also means the traditionally described benefits of catalyst nanostructuring (for increased surface area, mass transport, facet exposure, etc.) have to be somewhat reassessed, which may be difficult as the primary active surface is no longer easily accessible to surface characterization techniques.

#### Conclusion

 In summary, in this article we have shown that the minimum current density requirements for 438 future commercial systems will ultimately drive  $CO<sub>2</sub>$  reduction away from the operating conditions where much of the cutting-edge catalyst research has been performed.

 Acknowledging these realities and testing state-of-the-art catalysts under these more realistic operating conditions will be important not only for further improving performance metrics such as selectivity, activity and stability, but to accelerate research towards commercial applications that are exceedingly needed sooner rather than later. It is encouraging that there has been a recent noticeable shift in literature towards more system-integrated testing 445 platforms for electrochemical  $CO<sub>2</sub>$  reduction, and we hope that this new perspective further motivates adoption and helps incite new discoveries.

#### **Conflicts of Interest**

There are no conflicts of interest to declare.

## **Acknowledgements**

- This work was supported by contributions from the European Research Council in the form of
- a ERC Starting Grant (WUTANG) provided to WAS. The authors greatly acknowledge the
- stimulating research conversations with Dr. Cao-Thang Dinh, Dr. Ali Seifitokaldani, Dr. Md
- Kibria, Dr. Recep Kas, Dr. Christine Gabardo, Dr. Nathan Nesbitt, Jonathan Edwards and
- Divya Bohra, as well as Dr. David Sinton and Dr. Edward Sargent, that over time have
- allowed this article to come to fruition.

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