1	Enhancing electrocatalytic CO ₂ reduction using a system-integrated
2	approach to catalyst discovery
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(*) Correspondence and requests for materials can be addressed to Thomas Burdyny 9 (t.e.burdyny@tudelft.nl) and Wilson A. Smith (W.smith@tudelft.nl) 10 11 12 Electrocatalytic CO₂ reduction has the dual-promise of neutralizing carbon emissions in 13 the near future, while providing a long-term pathway to create energy-dense chemicals 14 and fuels from atmospheric CO₂. The field has advanced immensely in recent years, taking significant strides towards commercial realization. Catalyst innovations have 15 16 played a pivotal role in these advances, with a steady stream of new catalysts providing 17 gains in CO₂ conversion efficiencies and selectivities of both C1 and C2 products. 18 Comparatively few of these catalysts have been tested at commercially-relevant current 19 densities (~200 mA/cm²) due to transport limitations in traditional testing configurations 20 and a research focus on fundamental catalyst kinetics, which are measured at 21 substantially lower current densities. A catalyst's selectivity and activity, however, have 22 been shown to be highly sensitive to the local reaction environment, which changes 23 drastically as a function of reaction rate. As a consequence of this, the surface properties 24 of many CO₂ reduction catalysts risk being optimized for the wrong operating 25 conditions. The goal of this article is to communicate the substantial impact of reaction 26 rate on catalytic behaviour and the CO₂ reduction reaction. In brief, this work motivates 27 high current density catalyst testing as a necessary step to properly evaluate materials 28 for electrochemical CO₂ reduction, and to accelerate the technology toward its 29 envisioned application of neutralizing CO₂ emissions on a global scale.

Under an applied potential and in the presence of an appropriate catalyst, carbon-dioxide 30 (CO_2) and water can be electrocatalytically converted into syngas $(CO + H_2)$, ethylene (C_2H_4) , 31 32 methane (CH₄), ethanol (C₂H₅OH) and formate (HCOOH) among other products. The 33 collective market size of these reduction products is >500 Mton/year, indicating the potential 34 scale of a commercially competitive CO_2 electrolyzer;¹ in the process, and of utmost importance and urgency, this process may aid in reducing fossil fuels by supplanting current 35 36 production routes. Excitingly, CO₂ electroreduction catalysts have shown enough promise that 37 we are beginning to see the first steps towards commercial application of the technology, including more and more start-ups (see OPUS12, CERT, Dioxide Materials) and established 38 companies (Siemens) focusing on system design and engineering. As a result, researchers are 39 now targeting lower overall cell potentials by improving other parts of the conversion unit,²⁻⁵ 40 while looking to more efficiently integrate electrochemical CO₂ conversion units with 41 upstream and downstream processes.⁶ Future devices will also need to demonstrate stable 42 long-term operation (>20,000 hours) at substantial current densities (>200 mA/cm²) to 43 minimize the capital-expenditure of a conversion unit to economically-compelling levels.^{1,7,8} 44 45 Due to the low solubility of CO₂ in aqueous-fed systems that limits CO₂ conversion to current densities of ~35 mA/cm²,⁹⁻¹¹ researchers have turned to pressurized electrolytes and 46 47 gas-diffusion layer-based systems to supply enough CO₂ to the catalyst layer to sustain higher current densities. Despite these capabilities, an overwhelming percentage (>95%)^{12,13} of 48 49 fundamental studies and catalytic materials are still developed, tested and characterized in 50 classical H-cell configurations, where current densities are limited. The local catalytic 51 environment, and subsequently the energetics of the reactions occurring on a catalyst's surface, are known however to be highly sensitive to changes in reaction rate. Therefore a 52 53 fundamental question remains: how representative are the conclusions from aqueous-fed systems that are constrained to \sim 35 mA/cm² when the goal is to achieve >200 mA/cm²? 54

55 This article seeks to shed light on this question by summarizing how the local reaction 56 environment is known to vary as a function of current density, and how these changes may 57 impact reactions occurring on a catalyst's surface when pushed to commercial current 58 densities. To aid in the analysis we draw upon recent literature findings from electrochemical 59 experiments, transport phenomena and Density-Functional Theory (DFT) modelling.

Due to the promise of electrochemical CO₂ reduction technology, and a lack of selective and 60 efficient cathode materials, a large fraction of the field has undergone a global, 61 62 multidisciplinary effort over the last decade to find new and better catalysts. The search is complicated by the large number of surface factors impacting activity including intermediate 63 binding energy,^{14,15} (via coordination^{16,17} and site availability^{18–20}), packing,^{21,22} kinetic supply 64 of reactants,²³ desorption of products,²⁴ adsorbate-adsorbate interactions,²⁵ etc. The urgency 65 of these efforts is illustrated by the large number of material-centric review papers published 66 in the last year alone on catalyst development/optimization.^{10,26–30} Here, we define the catalyst 67 68 as the surface on which CO₂ is reduced. As with any catalytic process, however, the local and 69 system reaction environments play equally important roles in efficiently driving specific 70 reactions, while suppressing unwanted competing ones. Many researchers have reported the extreme sensitivity of the reaction to changes in local pH,³¹⁻³⁵ electrolytes^{36,37} and cations³⁸⁻⁴¹ 71 (easily illustrated by replacing K^+ with Na⁺). The 'catalyst' that notably reduces the energy 72 73 barrier for CO₂ reduction processes is then very much a combined material and environmental 74 that of the catalyst's surface effect, rather than (composition, coordination, 75 nano/mesostructure) alone.

The above distinction, while central to any catalytic process, warrants particular attention here due to the unique peculiarities of electrocatalytic CO₂ reduction in aqueous solvents. *Specifically, while the local environment directly influences reaction pathways and kinetics, the reduction reaction itself greatly disturbs the local environment.* At the root of this 80 reaction-driven sensitivity is the requirement for both CO₂ and protons (H⁺) to participate in 81 the CO₂ reduction process. The ever-present, and in many cases more thermodynamically favourable, hydrogen evolution reaction (HER) then simultaneously competes with CO2 82 83 reduction for protons and electrons. At extremely low current densities (<1 mA/cm²), these protons can be supplied to either reaction directly by hydronium contained within the local 84 electrolyte (Fig. 1a).⁴² As hydronium is depleted, water reduction fills the role as a hydrogen 85 source while the unused hydroxide molecule generated as a by-product, rapidly increases the 86 87 local electrolyte pH (Fig. 1c).^{43,44} At slightly more moderate CO₂ reduction current densities in aqueous-fed systems (~35 mA/cm² for C1 products, ~100 mA/cm² for C2 products^{32,36}), 88 89 CO₂ ultimately becomes depleted by a combination of diffusion limitations from the bulk 90 electrolyte, and the now unfavourable bicarbonate-equilibrium conditions as a result of the



Fig. 1: The relative effect of current density on the reaction (a) proton source, (b) concentration of CO_2 and (c) pH at the surface of a CO_2 reduction catalyst.

91 increased local pH.^{45,46} Thus, as the reaction proceeds from 0 mA/cm² to CO₂-depletion (Fig.
92 1b), the surface coverage and binding energies of key intermediates on a catalyst's surface are
93 ultimately impacted through these changes in the local environment;^{44,47,48} not dissimilar from
94 the surface effects incurred by varying material composition, structure or morphology. The
95 activity of a catalyst is then identified by the environment around it, as much as its physical
96 make-up.

The inherent sensitivity of the reaction to changing local conditions is seen in literature to 97 98 directly and indirectly drive many of the experimental choices in electrolyte type and 99 concentration. Unsurprisingly, a catalyst can perform exceptionally well or poorly depending 100 on the medium in which it is tested. The importance of the electrolyte medium on catalytic 101 behaviour is most clearly displayed through the near ubiquitous use of low KHCO₃ concentrations in reports of high selectivity C2 production on nanostructured⁴⁹⁻⁵¹ and oxide-102 derived Cu⁵²⁻⁵⁵ in H-cells. Here the poor buffering capacity of the electrolyte causes the pH 103 104 close to the electrode to quickly increase at low current densities (<20 mA/cm²), helping to promote C2 products and suppress the competing CH₄ and H₂ reactions.^{31,56} The morphology 105 of the catalyst can be used to provide similar cumulative effects,⁵² which ultimately makes 106 107 properly separating the direct contributions of intrinsic catalytic activity and the local 108 environment even more difficult. To this point, the field has collectively learned to manipulate 109 both catalysts and local electrochemical conditions as needed to optimize CO₂ reduction 110 performance metrics at primarily indiscriminate current densities. Given this widely-111 implemented knowledge that the environment is critical to catalytic behaviour, and that these 112 conditions change as a function of current density, it is our perspective that the environment at 113 commercially-relevant current densities (>200 mA/cm²) should be used as the criterion for 114 assessing catalytic performance and suitability.

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116 Effect of cell configuration and reaction rate on CO₂ reduction environments

117 The number of CO_2 electroreduction experiments reported at elevated current densities is 118 rapidly increasing, owed in part to the maturity of the field as well as the observed 119 performance benefits. Recent work has reviewed various electrochemical architectures capable of delivering enough CO₂ to the catalyst to reach current densities $>200 \text{ mA/cm}^2$,^{12,13} 120 summarizing in detail the impacts of different components and configurations on system 121 122 performance. While we refer the reader to these publications for specific technical advances 123 in the field, we will briefly summarize several commonly-used architectures (Fig. 2) and 124 aspects of their operation to illustrate how the reaction environment around the catalyst layer is influenced by elevated current densities. 125



Fig. 2: Comparative mass transport phenomena in commonly-used electrochemical CO₂ reduction configurations. (a) Cell view for an H-cell configuration with a catalyst deposited on a solid substrate, (b) Cell view for a catalyst deposited on a gas-diffusion layer with a flowing catholyte channel, (c) Cell view for a catalyst deposited on a gas-diffusion layer with a non-flowing catholyte, (d) species transport to and from a catalyst layer in which CO₂ is supplied via diffusion from the bulk electrolyte on the microscale (~50 μ m). (e) a CO₂ reduction catalyst layer deposited onto a hydrophobic substrate with CO₂ diffusion from a nearby gas-liquid interface (~50 nm). Liquid species diffuse to the ion-exchange membrane through either a bulk flowing electrolyte or a solid-supported electrolyte layer.

126 In each of the described configurations CO_2 is supplied to a catalyst layer that is fully or 127 partially immersed in a conductive electrolyte. This CO₂ can diffuse through the 128 hydrodynamic boundary layer of a saturated bulk electrolyte as in a standard H-cell configuration (Fig. 2a and d),^{45,46,57} or from a nearby gas-phase with a much shorter diffusion 129 pathway (Fig. 2b, c and e).^{58–61} Configurations where CO_2 is provided from the gas-phase use 130 131 a gas-diffusion layer to form a gas-liquid interface adjacent to the catalyst layer. 132 Electrochemical CO₂ reactors using gas-diffusion layers have historically been used in diverse configurations,^{13,62–64} but range primarily from a Kenis-type reactor with a flowing 133 catholyte^{58,65-73} (Fig. 2b), to membrane electrode assemblies^{2,5,12,74,75} which directly combine 134 135 a gas-diffusion layer, catalyst and ion exchange membrane into one unit (Fig. 2c). These latter configurations are occasionally denoted as 'catholyte-free' or gas-phase electrolysis due to the 136 137 lack of a flowing electrolyte between the catalyst layer and ion-exchange membrane. Liquid 138 water, however, is reported to be present in the porous catalyst layer in the majority of cases. 139 Further, research has shown that without the direct presence of a solid-supported electrolyte, CO₂ reduction selectivity can be heavily penalized.^{2,5,64} The two cathode variations shown in 140 141 Fig. 2b and c then similarly involve the diffusion of CO₂ across a gas-liquid interface and 142 through a thin electrolyte to a porous catalyst layer (Fig. 2e), where evidence suggests that the 143 reaction occurs primarily in the aqueous phase rather than at a three-phase solid-liquid-gas 144 interface. Water management is essential to maintain a stable gas-liquid equilibrium as both 145 flooding of the gas-diffusion layer and evaporation of the catholyte will impact CO₂ transport to the catalyst laver.^{5,70,76} A catalyst can be applied to the gas-diffusion laver via drop-casting, 146 147 airbrushing, electrodeposition, compression, or incorporation into the porous layer itself.

148 The primary difference between these architectures is a roughly 3-order of magnitude 149 reduction in the CO₂ diffusion pathway to the surface of the catalyst: from \sim 50 µm in an H-150 cell to \sim 50 nm using a gas-diffusion layer (Fig. 2b,c), which allows for the increased 151 maximum current densities reported in literature. Using a simple 1D reaction-diffusion model 152 developed previously,^{45,46,57–59} we can also approximate the similarities and differences in the 153 local catalytic environments as a function of reaction rate for both cases.

154 The first observation from these curves is that the CO₂ concentration and pH in the electrolyte 155 at low current densities is relatively similar for both configurations (Fig. 3). This is to be 156 expected as the decreased CO₂ diffusion pathway does not affect the maximum availability of 157 CO_2 in an electrolyte, and OH^- diffusion is moderated by the catholyte. In each case a sudden 158 increase in local pH is observed for the weakly-buffered electrolytes (1 M KCl, 159 0.1 M KHCO₃) as the hydroxide generated as a by-product of water-splitting cannot diffuse 160 away fast enough or be immediately buffered by the solution (Fig. 3b and d). Shown here, and in recent experimental work by the Koper group,⁴² the electrode pH can in fact shift by as 161 much as 6 units within the first $1 - 2 \text{ mA/cm}^2$. Not only could the reaction itself be altered by 162 163 this shift, but large pH differences between the reference and working electrodes in this 164 current density range complicate determination of the equilibrium potential, and subsequently, 165 product onset potentials and Tafel slopes. Furthermore, for slightly acidic CO₂-saturated 166 electrolytes, the solvent itself can also act as the sole proton source (via H₃O⁺) at current densities <1 mA/cm² until becoming depleted and replaced by water reduction (Fig. 1a). It is 167 168 then entirely possible for a CO_2 reduction catalyst to be effective within the Tafel region but 169 exhibit slower kinetics at higher potentials/current densities if the water reduction step to 170 liberate protons becomes rate-determining. Within this low current density region, where the 171 most important electrochemical characterizations of a material take place, the reaction 172 environment is then extremely sensitive, complicating analysis of intrinsic catalyst behaviour 173 and the reaction mechanisms at play.

174 In our reaction-diffusion model, the maximum predicted CO_2 reduction current densities in 175 the aqueous-fed system are again <35 mA/cm² for two-electron reduction processes (Fig. 3b).

As shown here in Fig. 3d, and in previous gas-diffusion layer modelling work, we can see 176 177 however that the maximum current densities are much higher in the case of a gas-diffusion layer as a result of the reduced CO₂ diffusion distance; here all electrolytes are capable of 178 sustaining current densities over the proposed 200 mA/cm² minimum. This agrees well with 179 180 experimental literature where current densities substantially higher than 200 mA/cm² have 181 been reported, including the first report using gas-diffusion layers for CO₂ reduction from Cook et al. in 1990.⁶² In recent work by Dinh et al., for example, current densities of 1 A/cm² 182 were reached in 1 M KOH at 1 atm with an overall CO₂ reduction selectivity over 90%.⁷⁰ 183 184 While these current densities might not be desired economically due to the corresponding increase in cell potential required,^{1,7} it indicates that substantial CO₂ reduction reaction rates 185 186 are possible even if the CO₂ partial pressure is reduced. This is important for future largescale devices (>100 cm² catalyst areas) where CO₂ partial pressure will decrease as it is 187 converted in the device. It is also worth noting that the proposed 200 mA/cm² minimum 188 189 current density is defined primarily for two-electron reduction products. For multi-carbon 190 products requiring more electrons per CO₂ molecule converted, this current density limit must 191 be higher to have the same molecular yield per unit area.

192 A final extremely important takeaway from Fig. 3 is that the pH near the electrode will be 193 inevitably high at commercially-viable current densities (>200 mA/cm²) in all of the most 194 commonly-used electrolytes, regardless of the choice of catalyst or electrolyte (Fig. 3d). Due 195 to the extremely large quantity of hydroxide generated as a by-product of water reduction and 196 limitations in transporting hydroxide away from the electrode, we predict the pH within the 197 catalyst layer will greater than 12, even for a 1 M KHCO₃ buffered electrolyte. While the use 198 of a 0.1 M KHCO₃ electrolyte can, and has, been used in an H-cell to approach the local pH 199 values reached at high current densities (Fig. 2b), these conditions are reached only when CO₂ 200 is largely depleted and over a small current density/potential range. It is worth noting that the



Fig. 3: Simplified predictions of the electrode concentration of CO_2 and pH for commonly-used electrolytes as a function of current density in an (a,b) H-cell with a 50 μ m CO₂ diffusion thickness and, (c,d) a gas-diffusion layer with a 50 nm CO₂ diffusion thickness and liquid diffusion layer of 200 μ m. A Faradaic efficiency of CO₂-to-CO of 90% is assumed.

201 locally alkaline conditions could potentially be avoided by using an acidic electrolyte, but the 202 reaction kinetics for CO_2 would have to outweigh the heavily-favoured hydrogen evolution 203 rate in acidic media. In any of these cases all changes in local pH will also ultimately have to 204 be paid for in the overall cell potential, regardless of the locally corrected cathode potential. In 205 brief, the results presented in Fig. 3d show a convergence towards local conditions that have 206 far-reaching implications for not only catalytic activity, but the stability and maximum 207 efficiency of an entire CO_2 reduction system, as discussed in later sections.

From existing knowledge about CO_2 reduction, we can infer that the thermodynamics and kinetics of reactions on a catalytic surface will be impacted by testing under these elevated reaction conditions. Further modelling and direct-measurement experimental studies of the local electrolyte environment are of course warranted, however, to even better understand

how various factors may influence the reaction (e.g. 2D/3D effects, morphology, partial 212 213 pressure of CO₂ in the gas-diffusion layer, etc.). A more detailed representation of CO₂ 214 diffusion through a porous electrode structure, for instance, may provide further insight but requires consideration of pore sizes, structures and additives,⁷⁷ which are catalyst-specific and 215 216 beyond the scope of this article. These studies are particularly needed for zero-gap membrane 217 electrode assemblies where the extremely-low catholyte volume is expected to make the local 218 reaction conditions more sensitive to the specific device configuration and the properties of 219 the ion-exchange membrane.

220 Impact of high current densities on CO₂ reduction catalyst testing

In the previous section we discussed the impact that both hydrogen evolution and CO_2 reduction have on the local environment up to commercially-relevant current densities. This section discusses the important opposite side of the equation, how does access to surplus CO_2 and the predicted local environment at higher current densities impact the reactions occurring on the surface of the catalyst. More importantly, can we use this understanding to design even better catalysts or conditions that may advance CO_2 electroreduction performance further.

227 In catalyst design the surface of a material is altered as a means of modifying catalytic 228 behaviour. By changing a surface's composition, nanostructure or even substrate, the binding 229 energies of molecules to the surface and the reaction rate of different pathways can be tuned 230 to promote certain reactions, and hopefully, suppress unwanted ones. In electrochemical CO₂ 231 reduction, the local environment can provide a similar function. Numerous experimental 232 studies have particularly noted the tendency for higher local pH conditions to favour CO and multi-carbon products while suppressing H₂ and CH₄ on metals such as Ag and Cu.^{32,36} As 233 234 shown in Fig. 3d, when operating at higher current densities this effect is pushed to the 235 extreme, even in highly buffered solutions. An important place to start is then to discuss the 236 effect of pH on the selectivity of both CO₂ reduction products and hydrogen evolution.

237 Due to its role as the primary competing reaction to CO₂ reduction, H₂ evolution is one of the 238 most important products to consider. Under basic conditions the H₂ evolution reaction 239 proceeds through direct water reduction and the Volmer-Tafel or Volmer-Heyrovsky steps 240 (see EIS Fig. S2). For commonly-used metals such as Cu, Au and Ag, the Volmer step is 241 particularly sluggish in basic conditions due to both poor water dissociation properties and 242 weak *H binding energies, which is pushed even further to the right and away from the peak of the classical volcano plot under higher pH conditions.^{78,79} Simultaneous CO₂ reduction 243 244 occurring on a catalyst's surface also tends to further suppress H₂ activity by weakening hydrogen binding, occupying surface sites and consuming protons.^{25,80} For catalysts on the 245 246 left side of the hydrogen binding energy volcano curve, however, hydrogen evolution under 247 locally basic conditions may increase for the same fundamental reasons.

For the most commonly-used set of materials, access to >200 mA/cm² current densities can 248 249 then provide a secondary means of suppressing hydrogen evolution by weakening hydrogen 250 binding energies under higher local pH conditions. A secondary, non-material approach for 251 suppressing hydrogen is particularly important for multi-carbon product formation where, 252 despite achieving 100-fold C2:C1 ratios, many of the best catalysts when operated in an Hcell are constantly dogged by a persistent 20-30% H₂ selectivity.^{62,63,68,69} When these same 253 254 catalyst are operated under elevated current densities in the configurations and electrolytes 255 described here (Fig. 2 and 3), the selectivity towards target products could be increased purely 256 by penalizing hydrogen evolution, rather than necessarily promoting CO₂ reduction activity. 257 From Fig. 3 one can expect that any pH-dependent suppression of H₂ would be a function of 258 current density and buffering strength, with the simultaneous requirement that the 259 overpotentials needed for CO₂ reduction are also competitive with H₂ evolution.

The local pH environment can also separately influence the energetics of different CO₂
reduction products. For catalysts capable of producing only CO and H₂, the suppression of H₂

262 can lead to high CO selectivities. On a Ag catalyst CO formation under alkaline conditions 263 has been also been observed to be produced almost immediately following the equilibrium potential of -0.11 V vs RHE^{58,67}, indicating that the reaction itself is improved. The behaviour 264 265 of CO formation on Cu also differs from that of a more neutral H-cell environment. In H-cell 266 tests CO selectivities of >20% are observed on Cu and Cu-derivatives only at very low 267 current densities (<5 mA/cm²) before being supplanted by CO₂ reduction to methane, 268 ethylene and ethanol. Under alkaline conditions performed in a gas-diffusion layer, high CO 269 selectivities appear over a much broader range (0-200 mA/cm²)^{70,73}. This suggests that the 270 binding energy of CO on Cu may be weakened under alkaline conditions, promoting faster desorption of the formed *CO intermediate more than under neutral conditions.⁷⁰ The 271 selectivity towards CO does eventually decrease in favour of higher order products similar to 272 273 what is observed in an H-cell, but at much higher overall current densities.

274 Similar to H₂ evolution, methane formation on Cu has been shown to be suppressed by 275 increased local pH on oxide-derived samples. If locally alkaline (pH>12) conditions are 276 indeed unavoidable with the currently-used electrolytes, then these results suggest that an alternate reaction mechanism or catalyst may be needed to realize selective methane 277 278 formation at elevated current densities. An interesting fundamental result would then be the 279 demonstration of a catalyst capable of selective methane formation under alkaline or locally 280 alkaline conditions. Inversely, for multi-carbon product formation on Cu, higher local pH conditions have been experimentally demonstrated^{31,73,83} to be an important factor for 281 282 promoting carbon-carbon coupling. The higher observed activity toward multi-carbon species 283 at lower potentials could be due to the imporved CO onset potentials, changes to the binding 284 energy of *CO, a direct effect of the local conditions on the energetics of the coupling step itself, or a cumulative effect of multiple factors. There does not appear to be any strong 285

correlations between pH and product distribution after C-C coupling, however, as most
studies report similar alkane to alkene ratios as in lower current density H-cell experiments.

288 While several studies have operated at elevated current densities using membrane electrode assemblies or neutral-pH catholytes such as KCl and bicarbonate-based salts, 2,5,12,13,73,84 a 289 290 larger number of gas-diffusion layer experiments have used KOH directly as a bulk catholyte, 58,65-68,70,71,85 with much of the original CO₂ reduction research pioneered by the 291 292 Kenis Group. By using an alkaline catholyte directly, the impact of a higher pH environment on catalyst performance can be probed across both low and high current densities.^{65–68,85} In a 293 294 1 M KOH environment, CO₂ reduction products have been observed on Cu, Au and Ag 295 catalysts at earlier overall onset potentials than in neutral conditions, with current densities of 296 >100 mA/cm² having been reached for CO, C₂H₄ and ethanol at more anodic potentials than -0.6 V vs. RHE and with <10% H₂ selectivities.^{61,65,67,70,86} These experiments, however, 297 298 do not pay the same overpotential price associated with the large local pH swing from neutral 299 to alkaline conditions, which are not taken into account when cathode potential are reported 300 versus a reversible hydrogen electrode (RHE). Additionally, the interaction between 301 unreacted CO₂ and hydroxide is problematic for overall stability, as described in the following 302 section. Using an alkaline electrolyte for testing and characterizing catalyst performance is 303 however a promising means of mimicking the local environment of high current densities 304 while being able to measure catalytic activity even at lower current densities.

A final consideration for our prediction that many electrolytes will be forced towards high local pH conditions pertains to catalyst stability. Depending on the properties and composition of a given catalyst, such conditions may result in the dissolution of metals into solution or the removal of some species from the surface. While this has not been observed for many of the Cu and Ag catalysts tested in gas-diffusion layer configurations to date, it should be a consideration in the design of new catalysts. 311 A second important property of the local reaction environment at commercial-relevant current densities is access to excess CO₂. While we have imposed a current density of 200 mA/cm² as 312 313 a threshold to reach, from Fig. 3c we can see that additional unreacted CO₂ surrounding the catalyst provides the capacity for even higher current densities. An increased CO₂ 314 315 concentration, even at elevated current densities, helps to kinetically ensure that CO₂ rather 316 than protons are able to populate the reaction surface. More importantly, the reaction will not 317 be hindered by a deficit of CO₂, even at higher local pH conditions. While single-carbon CO₂ reduction products such as CO,73 HCOOH88,89 and CH490 can reach relatively high 318 319 selectivities even at lower current densities in an H-cell configuration, the highest Faradaic 320 efficiencies reported for multi-carbon products typically appear at current densities where 321 CO₂ is almost depleted. This is in part due to the necessity for multi-carbon products to follow 322 from *CO (Fig. S2) and C-C coupling which requires both sufficient potentials and current densities.^{48,86,91} Testing novel catalysts at elevated current densities with less CO₂ limitations 323 324 would allow the surface coverage of the *CO reaction intermediate to be maximized over a 325 wider current and potential range without being kinetically-limited by CO₂ availability. This 326 is in contrast to current H-cell environments where peak C2 selectivities are often observed 327 only at singular operating conditions (i.e. at a specific potential, current density and pH). 328 Access to a larger operating window then allows more attention to be placed on modifying 329 catalysts to specifically alter CO₂ reduction product selectivity between higher-order products 330 such as alkenes vs. alcohols and C2 vs C3 products. Finally, operating under an excess CO₂ 331 environment reduces the overpotential losses associated with transport limitations (sometimes 332 called concentration polarizations). As a result, plots of voltage versus log(j) have been 333 observed to remain linear even up to 300 mA/cm², helping to remove one of the barriers to 334 gauging intrinsic catalyst activity.¹⁷

335 While the exact implications of high current density catalyst testing will vary slightly with 336 materials, we can assert that the local environment will differ greatly from the bulk electrolyte 337 with a substantial chance of changing important surface kinetics and the observed catalytic 338 activity. Tuning catalysts to optimize morphology or surface binding energies for low current 339 density characterization may then risk optimizing the catalyst for the wrong environment 340 unless higher current conditions can be appropriately mimicked. Performing such 341 experiments adds an additional degree of complexity due to the need for researchers to adopt 342 either a pressurized system or a gas-diffusion layer to supply additional CO₂ (Fig. 2), in 343 addition to developing new catalysts. We believe, however, that this to be an essential step to 344 make the best (highest activity, selectivity and stability) CO₂ reduction catalyst possible. 345 Fortunately, the range of experimental reports already performed at higher current densities 346 indicate that CO₂ reduction is typically improved versus operating in the same electrolyte at 347 lower current densities, at least in part due to increased CO₂ availability and suppression of pH-independent products. 348

349 Impact of high current densities on system design

Up to this point we have discussed the impacts of configuration and reaction conditions on the CO₂ reduction reaction and vice versa. While understanding the CO₂ reduction reaction and catalyst over a range of conditions is important, our preferred choice of catalyst and catholyte will have implications and constraints for the system as a whole. Further catalyst testing in a more commercial-type reactor will help to bring operational issues to the forefront of the field and may result in new ingenious scientific and engineering solutions to these issues.

356 One such issue pertains to the twist of fate that the most efficient CO_2 reduction conditions 357 appear to occur when a highly-alkaline electrolyte is used as a catholyte. While an alkaline 358 catholyte may provide optimal cathode performance, it comes at the cost of system stability 359 due to the interaction between unreacted CO_2 and hydroxide in the electrolyte, particularly at 360 current densities less than the CO₂ limiting case where higher concentrations of CO₂ exist in 361 solution. Our reaction-diffusion model shows that this interaction can decrease the pH within 362 the porous catalyst layer by 1-2 units at lower current densities depending on the replenishment rate from a bulk liquid phase (Fig. 3d).¹⁷ While this pH change can be 363 364 accounted for when trying to ascertain the intrinsic activity of the catalyst, a portion of the 365 CO₂ crossing the gas-liquid interface will be converted to bicarbonate upon interacting with hydroxide and then carbonate.⁶¹ Not only does this decrease CO₂ utilization, but over a long 366 367 enough operating time it will destroy the expensive KOH catholyte, itself energy-intensively 368 produced through electrochemical reactions. At the moment there is no engineering solution to completely mitigate this effect even at small scales, let alone a more complex $>100 \text{ cm}^2$ 369 370 reactor design. We may then be resigned to the use of neutral-pH catholytes which to date 371 would represent an increase in expected cathode overpotentials. Further, overall cell potentials 372 will be higher due to the need for the oxygen evolution reaction to occur in a similar pH 373 electrolyte, or by using a bipolar membrane to maintain an alkaline anolyte. While CO₂-374 hydroxide interactions are typically only considered as a critical issue for alkaline catholytes 375 such as KOH, systems using neutral electrolytes should also aim to balance the generated hydroxide ions with protons generated by the anode reaction.⁹² Even in a neutral-pH medium 376



Fig. 4: Expected ohmic losses as a function of current density for commonly-used electrolytes in an electrochemical cell with a combined 3 mm catholyte and anolyte thickness at 25 °C.

377 the system's electrolyte balance would similarly be steadily shifted away from the initial 378 condition due our CO_2 reagent that can influence pH; in this case, however, the electrolyte 379 could be externally regenerated without additional energy input.

380 Another cell design issue with using alkaline electrolytes is the need for anion exchange 381 membranes, which have comparatively slower ion transport than proton exchange membranes 382 and overall limited mobility for both bicarbonate and carbonate anions.^{11,81} For these reasons a large amount of research is being undertaken to improve OH^{-} , HCO_{3}^{-} and CO_{3}^{2-} transport 383 through anion exchange membranes, with a fair amount of work done by Dioxide Materials' 384 and their Sustainion[©] membrane which has shown 1000's of hours of stability, albeit under 385 specific operating conditions.^{25,82} Without sufficient bicarbonate/carbonate transport through 386 387 the membrane, the concentration of buffering ions will increase over time, forcing co-ion transport through the membrane and resulting in electrolyte precipitation, destroying the 388 389 membrane and/or the gas-diffusion layer. Without solutions to these issues it will be difficult 390 for either membrane electrode assemblies or alkaline catholytes to be paired with anion 391 exchange membranes in a practical CO₂ reduction device.

392 An additional reaction constraint brought on by the need for >200 mA/cm² operation pertains 393 to the practical choice of electrolytes, independent of their impact on catalytic activity. Using 394 this minimum current density as a target threshold we can approximate the expected ohmic 395 losses of commonly-used electrolytes at 25°C, regardless of the catalyst or substrate used. 396 Assuming a combined catholyte and anolyte thickness of 3 mm, for example, it is clear that 397 certain electrolytes will cause prohibitive ohmic losses (Fig. 4). The 0.1 M KHCO₃ electrolyte 398 used in the majority of the highest selectivity C₂H₄ studies, for instance, results in heating 399 losses of 6 V at 200 mA/cm², five-fold larger than the thermodynamic cell potential when 400 using an oxygen-evolving anode (Fig. S3). Such a low conductivity electrolyte can then never 401 be used in a functioning system unless the electrolyte pathway between the anode and cathode

is eliminated or greatly reduced, as in the case of membrane electrode assemblies (Fig. 2c).^{2,5} 402 403 These ohmic drops also put into perspective how other cell losses may be more influential 404 than further decreases to cathode overpotentials. It is worth noting that the result in Fig. 4 405 becomes even more pronounced when the presumed even higher current densities needed for 406 multi-carbon products such as C₂H₄ are considered. Finally, separate from our discussion 407 motivating the testing of catalysts at elevated current densities, this result highlights the need 408 to test catalysts in higher conductivity electrolytes to see the effect that a higher concentration 409 of supporting ions may or may not impact a catalyst's activity.

410 A final notable difference to performing CO₂ electroreduction in an H-cell versus a gas-411 diffusion layer configuration is subtler. As has been recently demonstrated, under high current 412 density operation the CO₂ reduction reaction is confined to a relatively small portion of a porous catalyst layer and takes place on the backside of the material (Fig. 5a).⁷⁰ This is in 413 414 contrast to an H-cell where CO₂ diffuses to the catalyst layer from the front-side bulk 415 electrolyte (Fig. 5a). Much like the effects of varying morphology and porosity in H-cell 416 catalyst studies allowed for performance to be improved and varied, the reversed flow 417 direction of CO₂ transport allows for unique gas-diffusion and catalyst layer engineering to 418 take place. One recent example is placing an inactive material on top of the catalyst layer 419 (Fig. 5a) to provide an additionally conductive layer. While this layer is used as a current 420 collector, it may also help to prevent both catalyst restructuring that can change catalytic 421 behaviour as well as the deposition of contaminants on the active catalyst surface. 422 Contaminants are a problem largely unique to CO₂ reduction due to the tendency for most 423 electrolytes to contain minute concentrations of Ni, Fe or Co, metals capable of preferentially 424 promoting hydrogen evolution even at low potentials and are a primary source of catalyst deactivation.^{2,95,96} One could further imagine layering catalyst structures on gas-diffusion 425 426 layers for either unique catalyst designs or supportive layers that provide new functionalities.



Fig. 5: (a) Schematic of the directional change in CO_2 transport for fully-aqueous and gas-diffusion layer CO_2 reduction catalysts. (b) Potential advantages of a change in the CO_2 transport and reaction direction inside a catalyst layer. A buried catalyst layer may be inherently more stable and protected from both contaminants and restructuring while still having access to CO_2 .

427 While many possibilities have yet to be explored for CO₂ reduction, a gas-diffusion layer 428 provides a porous electrode structure which fundamentally changes both reagent and product 429 transport pathways compared to the impermeable supports traditionally used in fully-aqueous 430 reactors. As adoption increases substantial opportunity then exists for further innovative 431 catalyst-support integrations to improve either stability or performance. The subtle operational 432 difference also means the traditionally described benefits of catalyst nanostructuring (for 433 increased surface area, mass transport, facet exposure, etc.) have to be somewhat reassessed, 434 which may be difficult as the primary active surface is no longer easily accessible to surface 435 characterization techniques.

436 <u>Conclusion</u>

437 In summary, in this article we have shown that the minimum current density requirements for 438 future commercial systems will ultimately drive CO_2 reduction away from the operating 439 conditions where much of the cutting-edge catalyst research has been performed. 440 Acknowledging these realities and testing state-of-the-art catalysts under these more realistic 441 operating conditions will be important not only for further improving performance metrics 442 such as selectivity, activity and stability, but to accelerate research towards commercial 443 applications that are exceedingly needed sooner rather than later. It is encouraging that there 444 has been a recent noticeable shift in literature towards more system-integrated testing 445 platforms for electrochemical CO_2 reduction, and we hope that this new perspective further 446 motivates adoption and helps incite new discoveries.

447 **Conflicts of Interest**

448 There are no conflicts of interest to declare.

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